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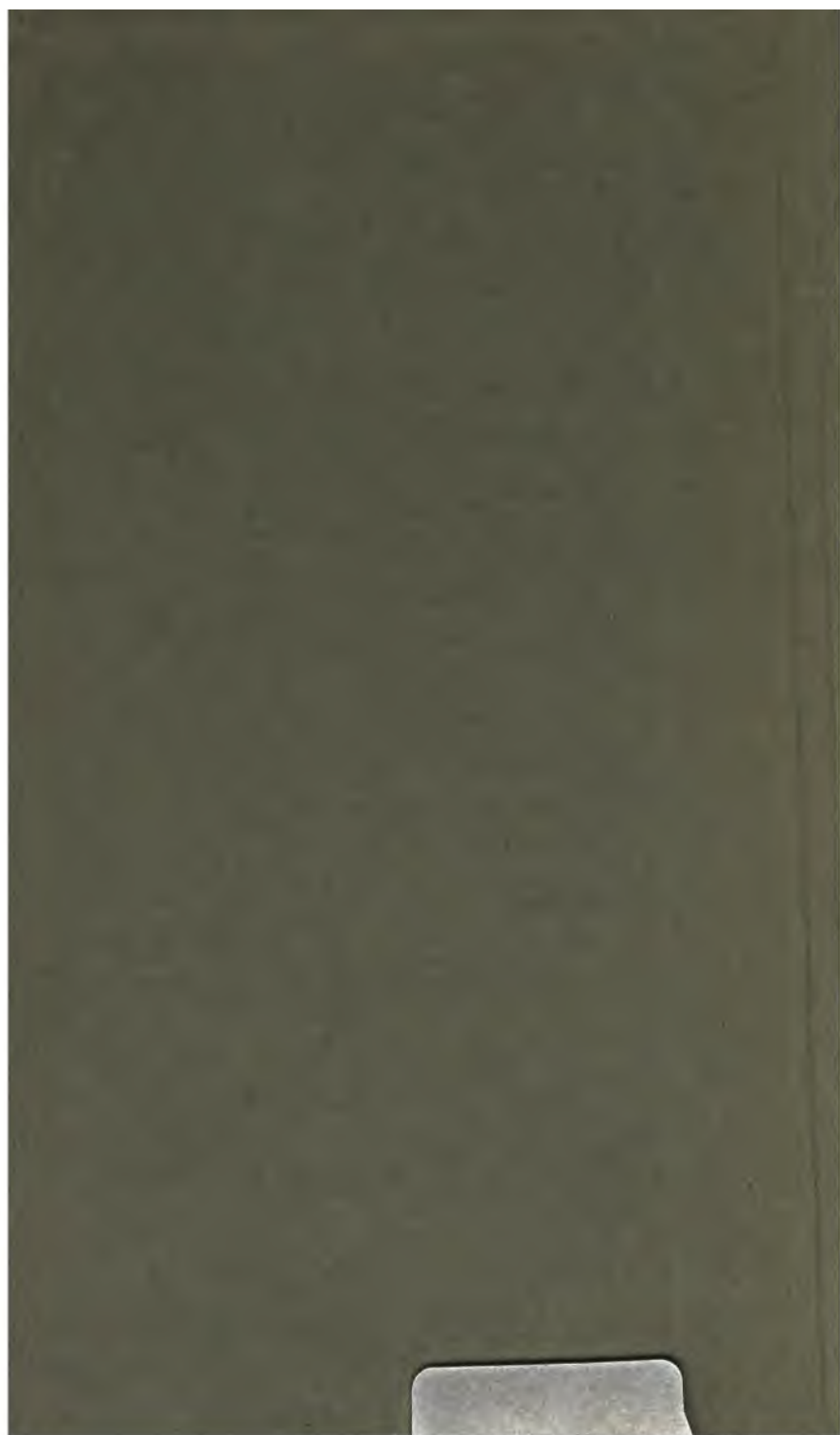
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PREPARED FOR STUDENTS OF THE
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SCRANTON, PA.

Volume V

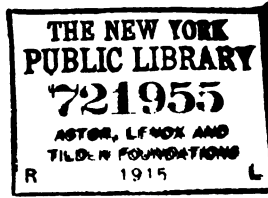
TABLES AND FORMULAS

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JULY
1897

TABLES AND FORMULAS.

This volume contains all the principal Tables and Formulas which are likely to be used by the student in practice. They have been collected and placed in this volume in order to make them convenient for ready reference, so that the student will not be obliged to hunt them out in the preceding volumes. The number after each formula is the same as the number following the same formula in the text.

NEW YORK
PUBLISHED BY
JOHN WILEY & SONS

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VIA AIR

TABLE

OF

COMMON LOGARITHMS

OF NUMBERS

From 1 to 10,000.

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LOGARITHMS.

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LOGARITHMS.

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300	47	712	727	741	756	770	784	799	813	828	842	
301		857	871	885	900	914	929	943	958	972	986	
302	48	001	015	029	044	058	073	087	101	116	130	
303		144	159	173	187	202	216	230	244	259	273	
304		287	302	316	330	344	359	373	387	401	416	
305		430	444	458	473	487	501	515	530	544	558	
306		572	586	601	615	629	643	657	671	686	700	
307		714	728	742	756	770	785	799	813	827	841	
308		855	869	883	897	911	926	940	954	968	982	
309		996	*010	*024	*038	*052	*066	*080	*094	*108	*122	
310	49	136	150	164	178	192	206	220	234	248	262	
311		276	290	304	318	332	346	360	374	388	402	
312		415	429	443	457	471	485	499	513	527	541	
313		554	568	582	596	610	624	638	651	665	679	
314		693	707	721	734	748	762	776	790	803	817	
315		831	845	859	872	886	900	914	927	941	955	
316		969	982	996	*010	*024	*037	*051	*065	*079	*092	
317	50	106	120	133	147	161	174	188	202	215	229	
318		243	256	270	284	297	311	325	338	352	365	
319		379	393	406	420	433	447	461	474	488	501	
320		515	529	542	556	569	583	596	610	623	637	
321		651	664	678	691	705	718	732	745	759	772	
322		786	799	813	826	840	853	866	880	893	907	
323		920	934	947	961	974	987	*001	*014	*028	*041	
324	51	055	068	081	095	108	121	135	148	162	175	
325		188	202	215	228	242	255	268	282	295	308	
326		322	335	348	362	375	388	402	415	428	441	
327		455	468	481	495	508	521	534	548	561	574	
328		587	601	614	627	640	654	667	680	693	706	
329		720	733	746	759	772	786	799	812	825	838	
330		851	865	878	891	904	917	930	943	957	970	
331		983	996	*009	*022	*035	*048	*061	*075	*088	*101	
332	52	114	127	140	153	166	179	192	205	218	231	
333		244	257	270	284	297	310	323	336	349	362	
334		375	388	401	414	427	440	453	466	479	492	
335		504	517	530	543	556	569	582	595	608	621	
336		634	647	660	673	686	699	711	724	737	750	
337		763	776	789	802	815	827	840	853	866	879	
338		892	905	917	930	943	956	969	982	994	*007	
339	53	020	033	046	058	071	084	097	110	122	135	
340		148	161	173	186	199	212	224	237	250	263	
341		275	288	301	314	326	339	352	364	377	390	
342		403	415	428	441	453	466	479	491	504	517	
343		529	542	555	567	580	593	605	618	631	643	
344		656	668	681	694	706	719	732	744	757	769	
345		782	794	807	820	832	845	857	870	882	895	
346		908	920	933	945	958	970	983	995	*008	*020	
347	54	033	045	058	070	083	095	108	120	133	145	
348		158	170	183	195	208	220	233	245	258	270	
349		283	295	307	320	332	345	357	370	382	394	
350		407	419	432	444	456	469	481	494	506	518	
N.	L.	0	1	2	3	4	5	6	7	8	9	P. P.

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350	54 407	419	432	444	456	469	481	494	506	518	13 1 1.3 2 2.6 3 3.9 4 5.2 5 6.5 6 7.8 7 9.1 8 10.4 9 11.7
351	531	543	555	568	580	593	605	617	630	642	
352	654	667	679	691	704	716	728	741	753	765	
353	777	790	802	814	827	839	851	864	876	888	
354	900	913	925	937	949	962	974	986	998	*011	
355	55 023	035	047	060	072	084	096	108	121	133	
356	145	157	169	182	194	206	218	230	242	255	
357	267	279	291	303	315	328	340	352	364	376	
358	388	400	413	425	437	449	461	473	485	497	
359	509	522	534	546	558	570	582	594	606	618	
360	630	642	654	666	678	691	703	715	727	739	12 1 1.2 2 2.4 3 3.6 4 4.8 5 6.0 6 7.2 7 8.4 8 9.6 9 10.8
361	751	763	775	787	799	811	823	835	847	859	
362	871	883	895	907	919	931	943	955	967	979	
363	991	*003	*015	*027	*038	*050	*062	*074	*086	*098	
364	56 110	122	134	146	158	170	182	194	205	217	
365	229	241	253	265	277	289	301	312	324	336	
366	348	360	372	384	396	407	419	431	443	455	
367	467	478	490	502	514	526	538	549	561	573	
368	585	597	608	620	632	644	656	667	679	691	
369	703	714	726	738	750	761	773	785	797	808	
370	820	832	844	855	867	879	891	902	914	926	11 1 1.1 2 2.2 3 3.3 4 4.4 5 5.5 6 6.6 7 7.7 8 8.8 9 9.9
371	937	949	961	972	984	996	*008	*019	*031	*043	
372	57 054	066	078	089	101	113	124	136	148	159	
373	171	183	194	206	217	229	241	252	264	276	
374	287	299	310	322	334	345	357	368	380	392	
375	403	415	426	438	449	461	473	484	496	507	
376	519	530	542	553	565	576	588	600	611	623	
377	634	646	657	669	680	692	703	715	726	738	
378	749	761	772	784	795	807	818	830	841	852	
379	864	875	887	898	910	921	933	944	955	967	
380	978	990	*001	*013	*024	*035	*047	*058	*070	*081	10 1 1.0 2 2.0 3 3.0 4 4.0 5 5.0 6 6.0 7 7.0 8 8.0 9 9.0
381	58 092	104	115	127	138	149	161	172	184	195	
382	206	218	229	240	252	263	274	286	297	309	
383	320	331	343	354	365	377	388	399	410	422	
384	433	444	456	467	478	490	501	512	524	535	
385	546	557	569	580	591	602	614	625	636	647	
386	659	670	681	692	704	715	726	737	749	760	
387	771	782	794	805	816	827	838	850	861	872	
388	883	894	906	917	928	939	950	961	973	984	
389	995	*006	*017	*028	*040	*051	*062	*073	*084	*095	
390	59 106	118	129	140	151	162	173	184	195	207	9 1 1.0 2 2.0 3 3.0 4 4.0 5 5.0 6 6.0 7 7.0 8 8.0 9 9.0
391	218	229	240	251	262	273	284	295	306	318	
392	329	340	351	362	373	384	395	406	417	428	
393	439	450	461	472	483	494	506	517	528	539	
394	550	561	572	583	594	605	616	627	638	649	
395	660	671	682	693	704	715	726	737	748	759	
396	770	780	791	802	813	824	835	846	857	868	
397	879	890	901	912	923	934	945	956	966	977	
398	988	999	*010	*021	*032	*043	*054	*065	*076	*086	
399	60 097	108	119	130	141	152	163	173	184	195	
400	206	217	228	239	249	260	271	282	293	304	P. P.
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400	60 206	217	228	239	249	260	271	282	293	304	
401	314	325	336	347	358	369	379	390	401	412	
402	423	433	444	455	466	477	487	498	509	520	
403	531	541	552	563	574	584	595	606	617	627	
404	638	649	660	670	681	692	703	713	724	735	
405	746	756	767	778	788	799	810	821	831	842	
406	853	863	874	885	895	906	917	927	938	949	
407	959	970	981	991	*002	*013	*023	*034	*045	*055	11
408	61 066	077	087	098	109	119	130	140	151	162	1 1.1
409	172	183	194	204	215	225	236	247	257	268	2 2.2
410	278	289	300	310	321	331	342	352	363	374	3 3.3
411	384	395	405	416	426	437	448	458	469	479	4 4.4
412	490	500	511	521	532	542	553	563	574	584	5 5.5
413	595	606	616	627	637	648	658	669	679	690	6 6.6
414	700	711	721	731	742	752	763	773	784	794	7 7.7
415	805	815	826	836	847	857	868	878	888	899	8 8.8
416	909	920	930	941	951	962	972	982	993	*003	9 9.9
417	62 014	024	034	045	055	066	076	086	097	107	
418	118	128	138	149	159	170	180	190	201	211	
419	221	232	242	252	263	273	284	294	304	315	
420	325	335	346	356	366	377	387	397	408	418	
421	428	439	449	459	469	480	490	500	511	521	10
422	531	542	552	562	572	583	593	603	613	624	1 1.0
423	634	644	655	665	675	685	696	706	716	726	2 2.0
424	737	747	757	767	778	788	798	808	818	829	3 3.0
425	839	849	859	870	880	890	900	910	921	931	4 4.0
426	941	951	961	972	982	992	*002	*012	*022	*033	5 5.0
427	63 043	053	063	073	083	094	104	114	124	134	6 6.0
428	144	155	165	175	185	195	205	215	225	236	7 7.0
429	246	256	266	276	286	296	306	317	327	337	8 8.0
430	347	357	367	377	387	397	407	417	428	438	9 9.0
431	448	458	468	478	488	498	508	518	528	538	
432	548	558	568	579	589	599	609	619	629	639	
433	649	659	669	679	689	699	709	719	729	739	
434	749	759	769	779	789	799	809	819	829	839	
435	849	859	869	879	889	899	909	919	929	959	
436	949	959	969	979	988	998	*008	*018	*028	*038	
437	64 048	058	068	078	088	098	108	118	128	137	9
438	147	157	167	177	187	197	207	217	227	237	1 0.9
439	246	256	266	276	286	296	306	316	326	335	2 1.8
440	345	355	365	375	385	395	404	414	424	434	3 2.7
441	444	454	464	473	483	493	503	513	523	532	4 3.6
442	542	552	562	572	582	591	601	611	621	631	5 4.5
443	640	650	660	670	680	689	699	709	719	729	6 5.4
444	738	748	758	768	777	787	797	807	816	826	7 6.3
445	836	846	856	865	875	885	895	904	914	924	8 7.2
446	933	943	953	963	972	982	992	*002	*011	*021	9 8.1
447	65 031	040	050	060	070	079	089	099	108	118	
448	128	137	147	157	167	176	186	196	205	215	
449	225	234	244	254	263	273	283	292	302	312	
450	321	331	341	350	360	369	379	389	398	408	
N.	L. o	1	2	3	4	5	6	7	8	9	P. P.

LOGARITHMS.

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N.	L. o	1	2	3	4	5	6	7	8	9	P. P.
450	65 321	331	341	350	360	369	379	389	398	408	10 1 1.0 2 2.0 3 3.0 4 4.0 5 5.0 6 6.0 7 7.0 8 8.0 9 9.0
451	418	427	437	447	456	466	475	485	495	504	
452	514	523	533	543	552	562	571	581	591	600	
453	610	619	629	639	648	658	667	677	686	696	
454	706	715	725	734	744	753	763	772	782	792	
455	801	811	820	830	839	849	858	868	877	887	
456	896	906	916	925	935	944	954	963	973	982	
457	992	*001	*011	*020	*030	*039	*049	*058	*068	*077	
458	66 087	096	106	115	124	134	143	153	162	172	
459	181	191	200	210	219	229	238	247	257	266	
460	276	285	295	304	314	323	332	342	351	361	9 1 0.9 2 1.8 3 2.7 4 3.6 5 4.5 6 5.4 7 6.3 8 7.2 9 8.1
461	370	380	389	398	408	417	427	436	445	455	
462	464	474	483	492	502	511	521	530	539	549	
463	558	567	577	586	596	605	614	624	633	642	
464	652	661	671	680	689	699	708	717	727	736	
465	745	755	764	773	783	792	801	811	820	829	
466	839	848	857	867	876	885	894	904	913	922	
467	932	941	950	960	969	978	987	997	*006	*015	
468	67 025	034	043	052	062	071	080	089	099	108	
469	117	127	136	145	154	164	173	182	191	201	
470	210	219	228	237	247	256	265	274	284	293	8 1 0.8 2 1.6 3 2.4 4 3.2 5 4.0 6 4.8 7 5.6 8 6.4 9 7.2
471	302	311	321	330	339	348	357	367	376	385	
472	394	403	413	422	431	440	449	459	468	477	
473	486	495	504	514	523	532	541	550	560	569	
474	578	587	596	605	614	624	633	642	651	660	
475	669	679	688	697	706	715	724	733	742	752	
476	761	770	779	788	797	806	815	825	834	843	
477	852	861	870	879	888	897	906	916	925	934	
478	943	952	961	970	979	988	997	*006	*015	*024	
479	68 034	043	052	061	070	079	088	097	106	115	
480	124	133	142	151	160	169	178	187	196	205	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
481	215	224	233	242	251	260	269	278	287	296	
482	305	314	323	332	341	350	359	368	377	386	
483	395	404	413	422	431	440	449	458	467	476	
484	485	494	502	511	520	529	538	547	556	565	
485	574	583	592	601	610	619	628	637	646	655	
486	664	673	681	690	699	708	717	726	735	744	
487	753	762	771	780	789	797	806	815	824	833	
488	842	851	860	869	878	886	895	904	913	922	
489	931	940	949	958	966	975	984	993	*002	*011	
490	69 020	028	037	046	055	064	073	082	090	099	6 1 0.6 2 1.2 3 1.8 4 2.4 5 3.0 6 3.6 7 4.2 8 4.8 9 5.4
491	108	117	126	135	144	152	161	170	179	188	
492	197	205	214	223	232	241	249	258	267	276	
493	285	294	302	311	320	329	338	346	355	364	
494	373	381	390	399	408	417	425	434	443	452	
495	461	469	478	487	496	504	513	522	531	539	
496	548	557	566	574	583	592	601	609	618	627	
497	636	644	653	662	671	679	688	697	705	714	
498	723	732	740	749	758	767	775	784	793	801	
499	810	819	827	836	845	854	862	871	880	888	
500	897	906	914	923	932	940	949	958	966	975	P. P.
N.	L. o	1	2	3	4	5	6	7	8	9	P. P.

LOGARITHMS.

N.	L. o	1	2	3	4	5	6	7	8	9	P. P.
500	69 897	906	914	923	932	940	949	958	966	975	
501	984	992	*001	*010	*018	*027	*036	*044	*053	*062	
502	70 070	079	088	096	105	114	122	131	140	148	
503	157	165	174	183	191	200	209	217	226	234	
504	243	252	260	269	278	286	295	303	312	321	
505	329	338	346	355	364	372	381	389	398	406	
506	415	424	432	441	449	458	467	475	484	492	
507	501	509	518	526	535	544	552	561	569	578	
508	586	595	603	612	621	629	638	646	655	663	
509	672	680	689	697	706	714	723	731	740	749	
510	757	766	774	783	791	800	808	817	825	834	
511	842	851	859	868	876	885	893	902	910	919	
512	927	935	944	952	961	969	978	986	995	*003	
513	71 012	020	029	037	046	054	063	071	079	088	
514	096	105	113	122	130	139	147	155	164	172	
515	181	189	198	206	214	223	231	240	248	257	
516	265	273	282	290	299	307	315	324	332	341	
517	349	357	366	374	383	391	399	408	416	425	
518	433	441	450	458	466	475	483	492	500	508	
519	517	525	533	542	550	559	567	575	584	592	
520	600	609	617	625	634	642	650	659	667	675	
521	684	692	700	709	717	725	734	742	750	759	
522	767	775	784	792	800	809	817	825	834	842	
523	850	858	867	875	883	892	900	908	917	925	
524	933	941	950	958	966	975	983	991	999	*008	
525	72 016	024	032	041	049	057	066	074	082	090	
526	099	107	115	123	132	140	148	156	165	173	
527	181	189	198	206	214	222	230	239	247	255	
528	263	272	280	288	296	304	313	321	329	337	
529	346	354	362	370	378	387	395	403	411	419	
530	428	436	444	452	460	469	477	485	493	501	
531	509	518	526	534	542	550	558	567	575	583	
532	591	599	607	616	624	632	640	648	656	665	
533	673	681	689	697	705	713	722	730	738	746	
534	754	762	770	779	787	795	803	811	819	827	
535	835	843	852	860	868	876	884	892	900	908	
536	916	925	933	941	949	957	965	973	981	989	
537	997	*006	*014	*022	*030	*038	*046	*054	*062	*070	
538	73 078	086	094	102	111	119	127	135	143	151	
539	159	167	175	183	191	199	207	215	223	231	
540	239	247	255	263	272	280	288	296	304	312	
541	320	328	336	344	352	360	368	376	384	392	
542	400	408	416	424	432	440	448	456	464	472	
543	480	488	496	504	512	520	528	536	544	552	
544	560	568	576	584	592	600	608	616	624	632	
545	640	648	656	664	672	679	687	695	703	711	
546	719	727	735	743	751	759	767	775	783	791	
547	799	807	815	823	830	838	846	854	862	870	
548	878	886	894	902	910	918	926	933	941	949	
549	957	965	973	981	989	997	*005	*013	*020	*028	
550	74 036	044	052	060	068	076	084	092	099	107	
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LOGARITHMS.

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550	74 036	044	052	060	068	076	084	092	099	107	8 1 0.8 2 1.6 3 2.4 4 3.2 5 4.0 6 4.8 7 5.6 8 6.4 9 7.2
551	115	123	131	139	147	155	162	170	178	186	
552	194	202	210	218	225	233	241	249	257	265	
553	273	280	288	296	304	312	320	327	335	343	
554	351	359	367	374	382	390	398	406	414	421	
555	429	437	445	453	461	468	476	484	492	500	
556	507	515	523	531	539	547	554	562	570	578	
557	586	593	601	609	617	624	632	640	648	656	
558	663	671	679	687	695	702	710	718	726	733	
559	741	749	757	764	772	780	788	796	803	811	
560	819	827	834	842	850	858	865	873	881	889	8 1 0.8 2 1.6 3 2.4 4 3.2 5 4.0 6 4.8 7 5.6 8 6.4 9 7.2
561	896	904	912	920	927	935	943	950	958	966	
562	974	981	989	997	*005	*012	*020	*028	*035	*043	
563	75 051	059	066	074	082	089	097	105	113	120	
564	128	136	143	151	159	166	174	182	189	197	
565	205	213	220	228	236	243	251	259	266	274	
566	282	289	297	305	312	320	328	335	343	351	
567	358	366	374	381	389	397	404	412	420	427	
568	435	442	450	458	465	473	481	488	496	504	
569	511	519	526	534	542	549	557	565	572	580	
570	587	595	603	610	618	626	633	641	648	656	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
571	664	671	679	686	694	702	709	717	724	732	
572	740	747	755	762	770	778	785	793	800	808	
573	815	823	831	838	846	853	861	868	876	884	
574	891	899	906	914	921	929	937	944	952	959	
575	967	974	982	989	997	*005	*012	*020	*027	*035	
576	76 042	050	057	065	072	080	087	095	103	110	
577	118	125	133	140	148	155	163	170	178	185	
578	193	200	208	215	223	230	238	245	253	260	
579	268	275	283	290	298	305	313	320	328	335	
580	343	350	358	365	373	380	388	395	403	410	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
581	418	425	433	440	448	455	462	470	477	485	
582	492	500	507	515	522	530	537	545	552	559	
583	567	574	582	589	597	604	612	619	626	634	
584	641	649	656	664	671	678	686	693	701	708	
585	716	723	730	738	745	753	760	768	775	782	
586	790	797	805	812	819	827	834	842	849	856	
587	864	871	879	886	893	901	908	916	923	930	
588	938	945	953	960	967	975	982	989	997	*004	
589	77 012	019	026	034	041	048	056	063	070	078	
590	085	093	100	107	115	122	129	137	144	151	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
591	159	166	173	181	188	195	203	210	217	225	
592	232	240	247	254	262	269	276	283	291	298	
593	305	313	320	327	335	342	349	357	364	371	
594	379	386	393	401	408	415	422	430	437	444	
595	452	459	466	474	481	488	495	503	510	517	
596	525	532	539	546	554	561	568	576	583	590	
597	597	605	612	619	627	634	641	648	656	663	
598	670	677	685	692	699	706	714	721	728	735	
599	743	750	757	764	772	779	786	793	801	808	
600	815	822	830	837	844	851	859	866	873	880	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
N.	L. o	1	2	3	4	5	6	7	8	9	
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600	77 815	822	830	837	844	851	859	866	873	880	
601	887	895	902	909	916	924	931	938	945	952	
602	960	967	974	981	988	996	*003	*010	*017	*025	
603	78 032	039	046	053	061	068	075	082	089	097	
604	104	111	118	125	132	140	147	154	161	168	
605	176	183	190	197	204	211	219	226	233	240	
606	247	254	262	269	276	283	290	297	305	312	
607	319	326	333	340	347	355	362	369	376	383	
608	390	398	405	412	419	426	433	440	447	455	
609	462	469	476	483	490	497	504	512	519	526	
610	533	540	547	554	561	569	576	583	590	597	
611	604	611	618	625	633	640	647	654	661	668	
612	675	682	689	696	704	711	718	725	732	739	
613	746	753	760	767	774	781	789	796	803	810	
614	817	824	831	838	845	852	859	866	873	880	
615	888	895	902	909	916	923	930	937	944	951	
616	958	965	972	979	986	993	*000	*007	*014	*021	
617	79 029	036	043	050	057	064	071	078	085	092	
618	099	106	113	120	127	134	141	148	155	162	
619	169	176	183	190	197	204	211	218	225	232	
620	239	246	253	260	267	274	281	288	295	302	
621	309	316	323	330	337	344	351	358	365	372	
622	379	386	393	400	407	414	421	428	435	442	
623	449	456	463	470	477	484	491	498	505	511	
624	518	525	532	539	546	553	560	567	574	581	
625	588	595	602	609	616	623	630	637	644	650	
626	657	664	671	678	685	692	699	706	713	720	
627	727	734	741	748	754	761	768	775	782	789	
628	796	803	810	817	824	831	837	844	851	858	
629	865	872	879	886	893	900	906	913	920	927	
630	934	941	948	955	962	969	975	982	989	996	
631	80 003	010	017	024	030	037	044	051	058	065	
632	072	079	085	092	099	106	113	120	127	134	
633	140	147	154	161	168	175	182	188	195	202	
634	209	216	223	229	236	243	250	257	264	271	
635	277	284	291	298	305	312	318	325	332	339	
636	346	353	359	366	373	380	387	393	400	407	
637	414	421	428	434	441	448	455	462	468	475	
638	482	489	496	502	509	516	523	530	536	543	
639	550	557	564	570	577	584	591	598	604	611	
640	618	625	632	638	645	652	659	665	672	679	
641	686	693	699	706	713	720	726	733	740	747	
642	754	760	767	774	781	787	794	801	808	814	
643	821	828	835	841	848	855	862	868	875	882	
644	889	895	902	909	916	922	929	936	943	949	
645	956	963	969	976	983	990	996	*003	*010	*017	
646	81 023	030	037	043	050	057	064	070	077	084	
647	090	097	104	111	117	124	131	137	144	151	
648	158	164	171	178	184	191	198	204	211	218	
649	224	231	238	245	251	258	265	271	278	285	
650	291	298	305	311	318	325	331	338	345	351	
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81 291	298	305	311	318	325	331	338	345	351	
358	365	371	378	385	391	398	405	411	418	
425	431	438	445	451	458	465	471	478	485	
491	498	505	511	518	525	531	538	544	551	
558	564	571	578	584	591	598	604	611	617	
624	631	637	644	651	657	664	671	677	684	
690	697	704	710	717	723	730	737	743	750	
757	763	770	776	783	790	796	803	809	816	
823	829	836	842	849	856	862	869	875	882	
889	895	902	908	915	921	928	935	941	948	
954	961	968	974	981	987	994	*000	*007	*014	
82 020	027	033	040	046	053	060	066	073	079	
086	092	099	105	112	119	125	132	138	145	
151	158	164	171	178	184	191	197	204	210	
217	223	230	236	243	249	256	263	269	276	
282	289	295	302	308	315	321	328	334	341	
347	354	360	367	373	380	387	393	400	406	
413	419	426	432	439	445	452	458	465	471	
478	484	491	497	504	510	517	523	530	536	
543	549	556	562	569	575	582	588	595	601	
607	614	620	627	633	640	646	653	659	666	
672	679	685	692	698	705	711	718	724	730	
737	743	750	756	763	769	776	782	789	795	
802	808	814	821	827	834	840	847	853	860	
866	872	879	885	892	898	905	911	918	924	
930	937	943	950	956	963	969	975	982	988	
995	*001	*008	*014	*020	*027	*033	*040	*046	*052	
83 059	065	072	078	085	091	097	104	110	117	
123	129	136	142	149	155	161	168	174	181	
187	193	200	206	213	219	225	232	238	245	
251	257	264	270	276	283	289	296	302	308	
315	321	327	334	340	347	353	359	366	372	
378	385	391	398	404	410	417	423	429	436	
442	448	455	461	467	474	480	487	493	499	
506	512	518	525	531	537	544	550	556	563	
569	575	582	588	594	601	607	613	620	626	
632	639	645	651	658	664	670	677	683	689	
696	702	708	715	721	727	734	740	746	753	
759	765	771	778	784	790	797	803	809	816	
822	828	835	841	847	853	860	866	872	879	
885	891	897	904	910	916	923	929	935	942	
948	954	960	967	973	979	985	992	998	*004	
84 011	017	023	029	036	042	048	055	061	067	
073	080	086	092	098	105	111	117	123	130	
136	142	148	155	161	167	173	180	186	192	
198	205	211	217	223	230	236	242	248	255	
261	267	273	280	286	292	298	305	311	317	
323	330	336	342	348	354	361	367	373	379	
386	392	398	404	410	417	423	429	435	442	
448	454	460	466	473	479	485	491	497	504	
510	516	522	528	535	541	547	553	559	566	
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700	84 510	516	522	528	535	541	547	553	559	566	7 1 0.7 2 1.4 3 2.1 4 2.8 5 3.5 6 4.2 7 4.9 8 5.6 9 6.3
701	572	578	584	590	597	603	609	615	621	628	
702	634	640	646	652	658	665	671	677	683	689	
703	696	702	708	714	720	726	733	739	745	751	
704	757	763	770	776	782	788	794	800	807	813	
705	819	825	831	837	844	850	856	862	868	874	
706	880	887	893	899	905	911	917	924	930	936	
707	942	948	954	960	967	973	979	985	991	997	
708	85 003	009	016	022	028	034	040	046	052	058	
709	065	071	077	083	089	095	101	107	114	120	
710	126	132	138	144	150	156	163	169	175	181	6 1 0.6 2 1.2 3 1.8 4 2.4 5 3.0 6 3.6 7 4.2 8 4.8 9 5.4
711	187	193	199	205	211	217	224	230	236	242	
712	248	254	260	266	272	278	285	291	297	303	
713	309	315	321	327	333	339	345	352	358	364	
714	370	376	382	388	394	400	406	412	418	425	
715	431	437	443	449	455	461	467	473	479	485	
716	491	497	503	509	516	522	528	534	540	546	
717	552	558	564	570	576	582	588	594	600	606	
718	612	618	625	631	637	643	649	655	661	667	
719	673	679	685	691	697	703	709	715	721	727	
720	733	739	745	751	757	763	769	775	781	788	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
721	794	800	806	812	818	824	830	836	842	848	
722	854	860	866	872	878	884	890	896	902	908	
723	914	920	926	932	938	944	950	956	962	968	
724	974	980	986	992	998	*004	*010	*016	*022	*028	
725	86 034	040	046	052	058	064	070	076	082	088	
726	094	100	106	112	118	124	130	136	141	147	
727	153	159	165	171	177	183	189	195	201	207	
728	213	219	225	231	237	243	249	255	261	267	
729	273	279	285	291	297	303	308	314	320	326	
730	332	338	344	350	356	362	368	374	380	386	4 1 0.4 2 0.8 3 1.2 4 1.6 5 2.0 6 2.4 7 2.8 8 3.2 9 3.6
731	392	398	404	410	415	421	427	433	439	445	
732	451	457	463	469	475	481	487	493	499	504	
733	510	516	522	528	534	540	546	552	558	564	
734	570	576	581	587	593	599	605	611	617	623	
735	629	635	641	646	652	658	664	670	676	682	
736	688	694	700	705	711	717	723	729	735	741	
737	747	753	759	764	770	776	782	788	794	800	
738	806	812	817	823	829	835	841	847	853	859	
739	864	870	876	882	888	894	900	906	911	917	
740	923	929	935	941	947	953	958	964	970	976	3 1 0.3 2 0.6 3 0.9 4 1.2 5 1.5 6 1.8 7 2.1 8 2.4 9 2.7
741	982	988	994	999	*005	*011	*017	*023	*029	*035	
742	87 040	046	052	058	064	070	075	081	087	093	
743	099	105	111	116	122	128	134	140	146	151	
744	157	163	169	175	181	186	192	198	204	210	
745	216	221	227	233	239	245	251	256	262	268	
746	274	280	286	291	297	303	309	315	320	326	
747	332	338	344	349	355	361	367	373	379	384	
748	390	396	402	408	413	419	425	431	437	442	
749	448	454	460	466	471	477	483	489	495	500	
750	506	512	518	523	529	535	541	547	552	558	2 1 0.2 2 0.4 3 0.6 4 0.8 5 1.0 6 1.2 7 1.4 8 1.6 9 1.8
N.	L. o	1	2	3	4	5	6	7	8	9	P. P.

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87 506	512	518	523	529	535	541	547	552	558	6 1 0.6 2 1.2 3 1.8 4 2.4 5 3.0 6 3.6 7 4.2 8 4.8 9 5.4
564	570	576	581	587	593	599	604	610	616	
622	628	633	639	645	651	656	662	668	674	
679	685	691	697	703	708	714	720	726	731	
737	743	749	754	760	766	772	777	783	789	
795	800	806	812	818	823	829	835	841	846	
852	858	864	869	875	881	887	892	898	904	
910	915	921	927	933	938	944	950	955	961	
967	973	978	984	990	996	*001	*007	*013	*018	
88 024	030	036	041	047	053	058	064	070	076	
081	087	093	098	104	110	116	121	127	133	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
138	144	150	156	161	167	173	178	184	190	
195	201	207	213	218	224	230	235	241	247	
252	258	264	270	275	281	287	292	298	304	
309	315	321	326	332	338	343	349	355	360	
366	372	377	383	389	395	400	406	412	417	
423	429	434	440	446	451	457	463	468	474	
480	485	491	497	502	508	513	519	525	530	
536	542	547	553	559	564	570	576	581	587	
593	598	604	610	615	621	627	632	638	643	
649	655	660	666	672	677	683	689	694	700	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
705	711	717	722	728	734	739	745	750	756	
762	767	773	779	784	790	795	801	807	812	
818	824	829	835	840	846	852	857	863	868	
874	880	885	891	897	902	908	913	919	925	
930	936	941	947	953	958	964	969	975	981	
986	992	997	*003	*009	*014	*020	*025	*031	*037	
89 042	048	053	059	064	070	076	081	087	092	
098	104	109	115	120	126	131	137	143	148	
154	159	165	170	176	182	187	193	198	204	
209	215	221	226	232	237	243	248	254	260	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
265	271	276	282	287	293	298	304	310	315	
321	326	332	337	343	348	354	360	365	371	
376	382	387	393	398	404	409	415	421	426	
432	437	443	448	454	459	465	470	476	481	
487	492	498	504	509	515	520	526	531	537	
542	548	553	559	564	570	575	581	586	592	
597	603	609	614	620	625	631	636	642	647	
653	658	664	669	675	680	686	691	697	702	
708	713	719	724	730	735	741	746	752	757	
763	768	774	779	785	790	796	801	807	812	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
818	823	829	834	840	845	851	856	862	867	
873	878	883	889	894	900	905	911	916	922	
927	933	938	944	949	955	960	966	971	977	
982	988	993	998	*004	*009	*015	*020	*026	*031	
90 037	042	048	053	059	064	069	075	080	086	
091	097	102	108	113	119	124	129	135	140	
146	151	157	162	168	173	179	184	189	195	
200	206	211	217	222	227	233	238	244	249	
255	260	266	271	276	282	287	293	298	304	
309	314	320	325	331	336	342	347	352	358	5 1 0.5 2 1.0 3 1.5 4 2.0 5 2.5 6 3.0 7 3.5 8 4.0 9 4.5
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800	90	309	314	320	325	331	336	342	347	352	358	
801		363	369	374	380	385	390	396	401	407	412	
802		417	423	428	434	439	445	450	455	461	466	
803		472	477	482	488	493	499	504	509	515	520	
804		526	531	536	542	547	553	558	563	569	574	
805		580	585	590	596	601	607	612	617	623	628	
806		634	639	644	650	655	660	666	671	677	682	
807		687	693	698	703	709	714	720	725	730	736	
808		741	747	752	757	763	768	773	779	784	789	
809		795	800	806	811	816	822	827	832	838	843	
810		849	854	859	865	870	875	881	886	891	897	
811		902	907	913	918	924	929	934	940	945	950	
812		956	961	966	972	977	982	988	993	998	*004	
813	91	009	014	020	025	030	036	041	046	052	057	
814		062	068	073	078	084	089	094	100	105	110	
815		116	121	126	132	137	142	148	153	158	164	
816		169	174	180	185	190	196	201	206	212	217	
817		222	228	233	238	243	249	254	259	265	270	
818		275	281	286	291	297	302	307	312	318	323	
819		328	334	339	344	350	355	360	365	371	376	
820		381	387	392	397	403	408	413	418	424	429	
821		434	440	445	450	455	461	466	471	477	482	
822		487	492	498	503	508	514	519	524	529	535	
823		540	545	551	556	561	566	572	577	582	587	
824		593	598	603	609	614	619	624	630	635	640	
825		645	651	656	661	666	672	677	682	687	693	
826		698	703	709	714	719	724	730	735	740	745	
827		751	756	761	766	772	777	782	787	793	798	
828		803	808	814	819	824	829	834	840	845	850	
829		855	861	866	871	876	882	887	892	897	903	
830		908	913	918	924	929	934	939	944	950	955	
831		960	965	971	976	981	986	991	997	*002	*007	
832	92	012	018	023	028	033	038	044	049	054	059	
833		065	070	075	080	085	091	096	101	106	111	
834		117	122	127	132	137	143	148	153	158	163	
835		169	174	179	184	189	195	200	205	210	215	
836		221	226	231	236	241	247	252	257	262	267	
837		273	278	283	288	293	298	304	309	314	319	
838		324	330	335	340	345	350	355	361	366	371	
839		376	381	387	392	397	402	407	412	418	423	
840		428	433	438	443	449	454	459	464	469	474	
841		480	485	490	495	500	505	511	516	521	526	
842		531	536	542	547	552	557	562	567	572	578	
843		583	588	593	598	603	609	614	619	624	629	
844		634	639	645	650	655	660	665	670	675	681	
845		686	691	696	701	706	711	716	722	727	732	
846		737	742	747	752	758	763	768	773	778	783	
847		788	793	799	804	809	814	819	824	829	834	
848		840	845	850	855	860	865	870	875	881	886	
849		891	896	901	906	911	916	921	927	932	937	
850		942	947	952	957	962	967	973	978	983	988	
N.	L.	o	1	2	3	4	5	6	7	8	9	P. P.

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1 0.6
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L. o	1	2	3	4	5	6	7	8	9	P. P.
92 942	947	952	957	962	967	973	978	983	988	
93 993	998	*003	*008	*013	*018	*024	*029	*034	*039	
044	049	054	059	064	069	075	080	085	090	
095	100	105	110	115	120	125	131	136	141	
146	151	156	161	166	171	176	181	186	192	
197	202	207	212	217	222	227	232	237	242	
247	252	258	263	268	273	278	283	288	293	
298	303	308	313	318	323	328	334	339	344	
349	354	359	364	369	374	379	384	389	394	
399	404	409	414	420	425	430	435	440	445	
450	455	460	465	470	475	480	485	490	495	
500	505	510	515	520	526	531	536	541	546	
551	556	561	566	571	576	581	586	591	596	
601	606	611	616	621	626	631	636	641	646	
651	656	661	666	671	676	682	687	692	697	
702	707	712	717	722	727	732	737	742	747	
752	757	762	767	772	777	782	787	792	797	
802	807	812	817	822	827	832	837	842	847	
852	857	862	867	872	877	882	887	892	897	
902	907	912	917	922	927	932	937	942	947	
952	957	962	967	972	977	982	987	992	997	
94 002	007	012	017	022	027	032	037	042	047	
052	057	062	067	072	077	082	086	091	096	
101	106	111	116	121	126	131	136	141	146	
151	156	161	166	171	176	181	186	191	196	
201	206	211	216	221	226	231	236	240	245	
250	255	260	265	270	275	280	285	290	295	
300	305	310	315	320	325	330	335	340	345	
349	354	359	364	369	374	379	384	389	394	
399	404	409	414	419	424	429	433	438	443	
448	453	458	463	468	473	478	483	488	493	
498	503	507	512	517	522	527	532	537	542	
547	552	557	562	567	571	576	581	586	591	
596	601	606	611	616	621	626	630	635	640	
645	650	655	660	665	670	675	680	685	689	
694	699	704	709	714	719	724	729	734	738	
743	748	753	758	763	768	773	778	783	787	
792	797	802	807	812	817	822	827	832	836	
841	846	851	856	861	866	871	876	880	885	
890	895	900	905	910	915	919	924	929	934	
939	944	949	954	959	963	968	973	978	983	
95 988	993	998	*002	*007	*012	*017	*022	*027	*032	
036	041	046	051	056	061	066	071	075	080	
085	090	095	100	105	109	114	119	124	129	
134	139	143	148	153	158	163	168	173	177	
182	187	192	197	202	207	211	216	221	226	
231	236	240	245	250	255	260	265	270	274	
279	284	289	294	299	303	308	313	318	323	
328	332	337	342	347	352	357	361	366	371	
376	381	386	390	395	400	405	410	415	419	
424	429	434	439	444	448	453	458	463	468	
L. o	1	2	3	4	5	6	7	8	9	F. P.

6	0.6
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N.	L. o	1	2	3	4	5	6	7	8	9	P. P.
900	95 424	429	434	439	444	448	453	458	463	468	
901	472	477	482	487	492	497	501	506	511	516	
902	521	525	530	535	540	545	550	554	559	564	
903	569	574	578	583	588	593	598	602	607	612	
904	617	622	626	631	636	641	646	650	655	660	
905	665	670	674	679	684	689	694	698	703	708	
906	713	718	722	727	732	737	742	746	751	756	
907	761	766	770	775	780	785	789	794	799	804	
908	809	813	818	823	828	832	837	842	847	852	
909	856	861	866	871	875	880	885	890	895	899	
910	904	909	914	918	923	928	933	938	942	947	
911	952	957	961	966	971	976	980	985	990	995	
912	999	*004	*009	*014	*019	*023	*028	*033	*038	*042	
913	96 047	052	057	061	066	071	076	080	085	090	
914	095	099	104	109	114	118	123	128	133	137	
915	142	147	152	156	161	166	171	175	180	185	
916	190	194	199	204	209	213	218	223	227	232	
917	237	242	246	251	256	261	265	270	275	280	
918	284	289	294	298	303	308	313	317	322	327	
919	332	336	341	346	350	355	360	365	369	374	
920	379	384	388	393	398	402	407	412	417	421	
921	426	431	435	440	445	450	454	459	464	468	
922	473	478	483	487	492	497	501	506	511	515	
923	520	525	530	534	539	544	548	553	558	562	
924	567	572	577	581	586	591	595	600	605	609	
925	614	619	624	628	633	638	642	647	652	656	
926	661	666	670	675	680	685	689	694	699	703	
927	708	713	717	722	727	731	736	741	745	750	
928	755	759	764	769	774	778	783	788	792	797	
929	802	806	811	816	820	825	830	834	839	844	
930	848	853	858	862	867	872	876	881	886	890	
931	895	900	904	909	914	918	923	928	932	937	
932	942	946	951	956	960	965	970	974	979	984	
933	988	993	997	*002	*007	*011	*016	*021	*025	*030	
934	97 035	039	044	049	053	058	063	067	072	077	
935	081	086	090	095	100	104	109	114	118	123	
936	128	132	137	142	146	151	155	160	165	169	
937	174	179	183	188	192	197	202	206	211	216	
938	220	225	230	234	239	243	248	253	257	262	
939	267	271	276	280	285	290	294	299	304	308	
940	313	317	322	327	331	336	340	345	350	354	
941	359	364	368	373	377	382	387	391	396	400	
942	405	410	414	419	424	428	433	437	442	447	
943	451	456	460	465	470	474	479	483	488	493	
944	497	502	506	511	516	520	525	529	534	539	
945	543	548	552	557	562	566	571	575	580	585	
946	589	594	598	603	607	612	617	621	626	630	
947	635	640	644	649	653	658	663	667	672	676	
948	681	685	690	695	699	704	708	713	717	722	
949	727	731	736	740	745	749	754	759	763	768	
950	772	777	782	786	791	795	800	804	809	813	
N.	L. o	1	2	3	4	5	6	7	8	9	P. P.

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LOGARITHMS.

19

N.	L.	o	1	2	3	4	5	6	7	8	9	P. P.
950	97	772	777	782	786	791	795	800	804	809	813	5 1 0.5 2 1.0 3 1.5

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1000

TABLES
OF
NATURAL SINES, COSINES
TANGENTS,
AND COTANGENTS

GIVING THE VALUES OF THE FUNCTIONS FOR
ALL DEGREES AND MINUTES FROM
0° TO 90°

°	0°		1°		2°		3°		4°		°
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.00000	1.	.01745	.99985	.03490	.99939	.05234	.99863	.06976	.99756	60
1	.00029	1.	.01774	.99984	.03519	.99938	.05263	.99861	.07005	.99754	59
2	.00058	1.	.01803	.99983	.03548	.99937	.05292	.99859	.07034	.99752	58
3	.00087	1.	.01832	.99982	.03577	.99936	.05321	.99858	.07063	.99750	57
4	.00116	1.	.01862	.99981	.03606	.99935	.05350	.99857	.07092	.99748	56
5	.00145	1.	.01891	.99980	.03635	.99934	.05379	.99855	.07121	.99746	55
6	.00175	1.	.01920	.99979	.03664	.99933	.05408	.99854	.07150	.99744	54
7	.00204	1.	.01949	.99978	.03693	.99932	.05437	.99852	.07179	.99742	53
8	.00233	1.	.01978	.99977	.03723	.99931	.05466	.99851	.07208	.99740	52
9	.00262	1.	.02007	.99976	.03752	.99930	.05495	.99849	.07237	.99738	51
10	.00291	1.	.02036	.99975	.03781	.99929	.05524	.99847	.07266	.99736	50
11	.00320	.99999	.02065	.99974	.03810	.99927	.05553	.99846	.07295	.99734	49
12	.00349	.99999	.02094	.99973	.03839	.99926	.05582	.99844	.07324	.99732	48
13	.00378	.99999	.02123	.99972	.03868	.99925	.05611	.99842	.07353	.99730	47
14	.00407	.99999	.02152	.99971	.03897	.99924	.05640	.99841	.07382	.99728	46
15	.00436	.99999	.02181	.99970	.03926	.99923	.05669	.99839	.07411	.99726	45
16	.00465	.99999	.02211	.99969	.03955	.99922	.05698	.99838	.07440	.99724	44
17	.00495	.99999	.02240	.99968	.03984	.99921	.05727	.99836	.07469	.99722	43
18	.00524	.99999	.02269	.99967	.04013	.99919	.05756	.99834	.07498	.99720	42
19	.00553	.99998	.02298	.99966	.04042	.99918	.05785	.99833	.07527	.99718	41
20	.00582	.99998	.02327	.99965	.04071	.99917	.05814	.99831	.07556	.99716	40
21	.00611	.99998	.02356	.99964	.04100	.99916	.05844	.99829	.07585	.99714	39
22	.00640	.99998	.02385	.99963	.04129	.99915	.05873	.99827	.07614	.99712	38
23	.00669	.99998	.02414	.99962	.04158	.99913	.05902	.99826	.07643	.99710	37
24	.00698	.99997	.02443	.99961	.04188	.99912	.05931	.99824	.07672	.99708	36
25	.00727	.99997	.02472	.99960	.04217	.99911	.05960	.99822	.07701	.99706	35
26	.00756	.99997	.02501	.99959	.04246	.99910	.05989	.99821	.07730	.99704	34
27	.00785	.99997	.02530	.99958	.04275	.99909	.06018	.99819	.07759	.99702	33
28	.00814	.99997	.02559	.99957	.04304	.99907	.06047	.99817	.07788	.99700	32
29	.00844	.99996	.02588	.99956	.04333	.99906	.06076	.99815	.07817	.99698	31
30	.00873	.99996	.02618	.99955	.04362	.99905	.06105	.99813	.07846	.99696	30
31	.00902	.99996	.02647	.99954	.04391	.99904	.06134	.99812	.07875	.99694	29
32	.00931	.99996	.02676	.99953	.04420	.99903	.06163	.99810	.07904	.99692	28
33	.00960	.99995	.02705	.99952	.04449	.99901	.06192	.99808	.07933	.99690	27
34	.00989	.99995	.02734	.99951	.04478	.99900	.06221	.99806	.07962	.99688	26
35	.01018	.99995	.02763	.99950	.04507	.99898	.06250	.99804	.07991	.99686	25
36	.01047	.99995	.02792	.99949	.04536	.99897	.06279	.99803	.08020	.99684	24
37	.01076	.99994	.02821	.99948	.04565	.99896	.06308	.99801	.08049	.99682	23
38	.01105	.99994	.02850	.99947	.04594	.99894	.06337	.99799	.08078	.99680	22
39	.01134	.99994	.02879	.99946	.04623	.99893	.06366	.99797	.08107	.99678	21
40	.01164	.99993	.02908	.99945	.04653	.99892	.06395	.99795	.08136	.99676	20
41	.01193	.99993	.02938	.99944	.04682	.99890	.06424	.99793	.08165	.99674	19
42	.01222	.99993	.02967	.99943	.04711	.99889	.06453	.99792	.08194	.99672	18
43	.01251	.99992	.02996	.99942	.04740	.99888	.06482	.99790	.08223	.99670	17
44	.01280	.99992	.03025	.99941	.04769	.99886	.06511	.99788	.08252	.99668	16
45	.01309	.99991	.03054	.99940	.04798	.99885	.06540	.99786	.08281	.99666	15
46	.01338	.99991	.03083	.99939	.04827	.99883	.06569	.99784	.08310	.99664	14
47	.01367	.99991	.03112	.99938	.04856	.99882	.06598	.99782	.08339	.99662	13
48	.01396	.99990	.03141	.99937	.04885	.99881	.06627	.99780	.08368	.99660	12
49	.01425	.99990	.03170	.99936	.04914	.99879	.06656	.99778	.08397	.99658	11
50	.01454	.99989	.03199	.99935	.04943	.99878	.06685	.99776	.08426	.99656	10
51	.01483	.99989	.03228	.99934	.04972	.99876	.06714	.99774	.08455	.99654	9
52	.01513	.99988	.03257	.99933	.05001	.99875	.06743	.99772	.08484	.99652	8
53	.01542	.99988	.03286	.99932	.05030	.99873	.06772	.99770	.08513	.99650	7
54	.01571	.99988	.03316	.99931	.05059	.99872	.06802	.99768	.08542	.99648	6
55	.01600	.99987	.03345	.99930	.05088	.99870	.06831	.99766	.08571	.99646	5
56	.01629	.99987	.03374	.99929	.05117	.99869	.06860	.99764	.08600	.99644	4
57	.01658	.99986	.03403	.99928	.05146	.99867	.06889	.99762	.08629	.99642	3
58	.01687	.99986	.03432	.99927	.05175	.99866	.06918	.99760	.08658	.99640	2
59	.01716	.99985	.03461	.99926	.05204	.99864	.06947	.99758	.08687	.99638	1
60	.01745	.99985	.03490	.99925	.05234	.99863	.06976	.99756	.08716	.99636	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	89°		88°		87°		86°		85°		

	5°		6°		7°		8°		9°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.08716	.99619	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	60
1	.08745	.99617	.10482	.99449	.12216	.99251	.13946	.99023	.15672	.98764	59
2	.08774	.99614	.10511	.99446	.12245	.99248	.13975	.99019	.15701	.98760	58
3	.08803	.99612	.10540	.99443	.12274	.99244	.14004	.99015	.15730	.98755	57
4	.08831	.99609	.10569	.99440	.12302	.99240	.14033	.99011	.15758	.98751	56
5	.08860	.99607	.10597	.99437	.12331	.99237	.14061	.99006	.15787	.98746	55
6	.08889	.99604	.10626	.99434	.12360	.99233	.14090	.99002	.15816	.98741	54
7	.08918	.99602	.10655	.99431	.12389	.99230	.14119	.98998	.15845	.98737	53
8	.08947	.99599	.10684	.99428	.12418	.99226	.14148	.98994	.15873	.98732	52
9	.08976	.99596	.10713	.99424	.12447	.99222	.14177	.98990	.15902	.98728	51
10	.09005	.99594	.10742	.99421	.12476	.99219	.14205	.98986	.15931	.98723	50
11	.09034	.99591	.10771	.99418	.12504	.99215	.14234	.98982	.15959	.98718	49
12	.09063	.99588	.10800	.99415	.12533	.99211	.14263	.98978	.15988	.98714	48
13	.09092	.99586	.10829	.99412	.12562	.99208	.14292	.98973	.16017	.98709	47
14	.09121	.99583	.10858	.99409	.12591	.99204	.14320	.98969	.16046	.98704	46
15	.09150	.99580	.10887	.99406	.12620	.99200	.14349	.98965	.16074	.98700	45
16	.09179	.99578	.10916	.99402	.12649	.99197	.14378	.98961	.16103	.98695	44
17	.09208	.99575	.10945	.99399	.12678	.99193	.14407	.98957	.16132	.98690	43
18	.09237	.99572	.10973	.99396	.12706	.99189	.14436	.98953	.16160	.98686	42
19	.09266	.99570	.11002	.99393	.12735	.99186	.14464	.98948	.16189	.98681	41
20	.09295	.99567	.11031	.99390	.12764	.99182	.14493	.98944	.16218	.98676	40
21	.09324	.99564	.11060	.99386	.12793	.99178	.14522	.98940	.16246	.98671	39
22	.09353	.99562	.11089	.99383	.12822	.99175	.14551	.98936	.16275	.98667	38
23	.09382	.99559	.11118	.99380	.12851	.99171	.14580	.98931	.16304	.98662	37
24	.09411	.99556	.11147	.99377	.12880	.99167	.14608	.98927	.16333	.98657	36
25	.09440	.99553	.11176	.99374	.12909	.99163	.14637	.98923	.16361	.98652	35
26	.09469	.99551	.11205	.99370	.12937	.99160	.14666	.98919	.16390	.98648	34
27	.09498	.99548	.11234	.99367	.12966	.99156	.14695	.98914	.16419	.98643	33
28	.09527	.99545	.11263	.99364	.12995	.99152	.14723	.98910	.16447	.98638	32
29	.09556	.99542	.11291	.99360	.13024	.99148	.14752	.98906	.16476	.98633	31
30	.09585	.99540	.11320	.99357	.13053	.99144	.14781	.98902	.16505	.98629	30
31	.09614	.99537	.11349	.99354	.13081	.99141	.14810	.98897	.16533	.98624	29
32	.09642	.99534	.11378	.99351	.13110	.99137	.14838	.98893	.16562	.98619	28
33	.09671	.99531	.11407	.99347	.13139	.99133	.14867	.98889	.16591	.98614	27
34	.09700	.99528	.11436	.99344	.13168	.99129	.14896	.98884	.16620	.98609	26
35	.09729	.99526	.11465	.99341	.13197	.99125	.14925	.98880	.16648	.98604	25
36	.09758	.99523	.11494	.99337	.13226	.99122	.14954	.98876	.16677	.98600	24
37	.09787	.99520	.11523	.99334	.13254	.99118	.14982	.98871	.16706	.98595	23
38	.09816	.99517	.11552	.99331	.13283	.99114	.15011	.98867	.16734	.98590	22
39	.09845	.99514	.11580	.99327	.13312	.99110	.15040	.98863	.16763	.98585	21
40	.09874	.99511	.11609	.99324	.13341	.99106	.15069	.98858	.16792	.98580	20
41	.09903	.99508	.11638	.99320	.13370	.99102	.15097	.98854	.16820	.98575	19
42	.09932	.99506	.11667	.99317	.13399	.99098	.15126	.98849	.16849	.98570	18
43	.09961	.99503	.11696	.99314	.13427	.99094	.15155	.98845	.16878	.98565	17
44	.09990	.99500	.11725	.99310	.13456	.99090	.15184	.98841	.16906	.98561	16
45	.10019	.99497	.11754	.99307	.13485	.99087	.15213	.98836	.16935	.98556	15
46	.10048	.99494	.11783	.99303	.13514	.99083	.15241	.98832	.16964	.98551	14
47	.10077	.99491	.11812	.99300	.13543	.99079	.15270	.98827	.16992	.98546	13
48	.10106	.99488	.11840	.99297	.13572	.99075	.15299	.98823	.17021	.98541	12
49	.10135	.99485	.11869	.99293	.13600	.99071	.15327	.98818	.17050	.98536	11
50	.10164	.99482	.11898	.99290	.13629	.99067	.15356	.98814	.17078	.98531	10
51	.10192	.99479	.11927	.99286	.13658	.99063	.15385	.98809	.17107	.98526	9
52	.10221	.99476	.11956	.99283	.13687	.99059	.15414	.98805	.17136	.98521	8
53	.10250	.99473	.11985	.99279	.13716	.99055	.15442	.98800	.17164	.98516	7
54	.10279	.99470	.12014	.99276	.13744	.99051	.15471	.98796	.17193	.98511	6
55	.10308	.99467	.12043	.99272	.13773	.99047	.15500	.98791	.17222	.98506	5
56	.10337	.99464	.12071	.99269	.13802	.99043	.15529	.98787	.17250	.98501	4
57	.10366	.99461	.12100	.99265	.13831	.99039	.15557	.98782	.17279	.98496	3
58	.10395	.99458	.12129	.99262	.13860	.99035	.15586	.98778	.17308	.98491	2
59	.10424	.99455	.12158	.99258	.13889	.99031	.15615	.98773	.17336	.98486	1
60	.10453	.99452	.12187	.99255	.13917	.99027	.15643	.98769	.17365	.98481	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	84°		83°		82°		81°		80°		

	10°		11°		12°		13°		14°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.17365	.98481	.19081	.98163	.20791	.97815	.22495	.97437	.24192	.97030	60
1	.17393	.98476	.19109	.98157	.20820	.97809	.22523	.97430	.24220	.97023	59
2	.17422	.98471	.19138	.98152	.20848	.97803	.22552	.97424	.24249	.97015	58
3	.17451	.98466	.19167	.98146	.20877	.97797	.22580	.97417	.24277	.97008	57
4	.17479	.98461	.19195	.98140	.20905	.97791	.22608	.97411	.24305	.97001	56
5	.17508	.98455	.19224	.98135	.20933	.97784	.22637	.97404	.24333	.96994	55
6	.17537	.98450	.19252	.98129	.20962	.97778	.22665	.97398	.24362	.96987	54
7	.17565	.98445	.19281	.98124	.20990	.97772	.22693	.97391	.24390	.96980	53
8	.17594	.98440	.19309	.98118	.21019	.97766	.22722	.97384	.24418	.96973	52
9	.17623	.98435	.19338	.98112	.21047	.97760	.22750	.97378	.24446	.96966	51
10	.17651	.98430	.19366	.98107	.21076	.97754	.22778	.97371	.24474	.96959	50
11	.17680	.98425	.19395	.98101	.21104	.97748	.22807	.97365	.24503	.96952	49
12	.17708	.98420	.19423	.98096	.21132	.97742	.22835	.97358	.24531	.96945	48
13	.17737	.98414	.19452	.98090	.21161	.97735	.22863	.97351	.24559	.96937	47
14	.17766	.98409	.19481	.98084	.21189	.97729	.22892	.97345	.24587	.96930	46
15	.17794	.98404	.19509	.98079	.21218	.97723	.22920	.97338	.24615	.96923	45
16	.17823	.98399	.19538	.98073	.21246	.97717	.22948	.97331	.24644	.96916	44
17	.17852	.98394	.19566	.98067	.21275	.97711	.22977	.97325	.24672	.96909	43
18	.17880	.98389	.19595	.98061	.21303	.97705	.23005	.97318	.24700	.96902	42
19	.17909	.98383	.19623	.98056	.21331	.97699	.23033	.97311	.24728	.96894	41
20	.17937	.98378	.19652	.98050	.21360	.97692	.23062	.97304	.24756	.96887	40
21	.17966	.98373	.19680	.98044	.21388	.97686	.23090	.97298	.24784	.96880	39
22	.17995	.98368	.19709	.98039	.21417	.97680	.23118	.97291	.24813	.96873	38
23	.18023	.98362	.19737	.98033	.21445	.97673	.23146	.97284	.24841	.96866	37
24	.18052	.98357	.19766	.98027	.21474	.97667	.23175	.97278	.24869	.96858	36
25	.18081	.98352	.19794	.98021	.21502	.97661	.23203	.97271	.24897	.96851	35
26	.18109	.98347	.19823	.98016	.21530	.97655	.23231	.97264	.24925	.96844	34
27	.18138	.98341	.19851	.98010	.21559	.97648	.23260	.97257	.24954	.96837	33
28	.18166	.98336	.19880	.98004	.21587	.97642	.23288	.97251	.24982	.96829	32
29	.18195	.98331	.19908	.97998	.21616	.97636	.23316	.97244	.25010	.96822	31
30	.18224	.98325	.19937	.97992	.21644	.97630	.23345	.97237	.25038	.96815	30
31	.18252	.98320	.19965	.97987	.21672	.97623	.23373	.97230	.25066	.96807	29
32	.18281	.98315	.19994	.97981	.21701	.97617	.23401	.97223	.25094	.96800	28
33	.18309	.98310	.20022	.97975	.21729	.97611	.23429	.97217	.25122	.96793	27
34	.18338	.98304	.20051	.97969	.21758	.97604	.23458	.97210	.25151	.96786	26
35	.18367	.98299	.20079	.97963	.21786	.97598	.23486	.97203	.25179	.96778	25
36	.18395	.98294	.20108	.97958	.21814	.97592	.23514	.97196	.25207	.96771	24
37	.18424	.98288	.20136	.97952	.21843	.97585	.23542	.97189	.25235	.96764	23
38	.18452	.98283	.20165	.97946	.21871	.97579	.23571	.97182	.25263	.96756	22
39	.18481	.98277	.20193	.97940	.21899	.97573	.23599	.97176	.25291	.96749	21
40	.18509	.98272	.20222	.97934	.21928	.97566	.23627	.97169	.25320	.96742	20
41	.18538	.98267	.20250	.97928	.21956	.97560	.23656	.97162	.25348	.96734	19
42	.18567	.98261	.20279	.97922	.21985	.97553	.23684	.97155	.25376	.96727	18
43	.18595	.98256	.20307	.97916	.22013	.97547	.23712	.97148	.25404	.96719	17
44	.18624	.98250	.20336	.97910	.22041	.97541	.23740	.97141	.25432	.96712	16
45	.18652	.98245	.20364	.97905	.22070	.97534	.23769	.97134	.25460	.96705	15
46	.18681	.98240	.20393	.97899	.22098	.97528	.23797	.97127	.25488	.96697	14
47	.18710	.98234	.20421	.97893	.22126	.97521	.23825	.97120	.25516	.96690	13
48	.18738	.98229	.20450	.97887	.22155	.97515	.23853	.97113	.25545	.96682	12
49	.18767	.98223	.20478	.97881	.22183	.97508	.23882	.97106	.25573	.96675	11
50	.18795	.98218	.20507	.97875	.22212	.97502	.23910	.97100	.25601	.96667	10
51	.18824	.98212	.20535	.97869	.22240	.97496	.23938	.97093	.25629	.96660	9
52	.18852	.98207	.20563	.97863	.22268	.97490	.23966	.97086	.25657	.96653	8
53	.18881	.98201	.20592	.97857	.22297	.97483	.23995	.97079	.25685	.96645	7
54	.18910	.98196	.20620	.97851	.22325	.97476	.24023	.97072	.25713	.96638	6
55	.18938	.98190	.20649	.97845	.22353	.97470	.24051	.97065	.25741	.96630	5
56	.18967	.98185	.20677	.97839	.22382	.97463	.24079	.97058	.25769	.96623	4
57	.18995	.98179	.20706	.97833	.22410	.97457	.24108	.97051	.25798	.96615	3
58	.19024	.98174	.20734	.97827	.22438	.97450	.24136	.97044	.25826	.96608	2
59	.19052	.98168	.20763	.97821	.22467	.97444	.24164	.97037	.25854	.96600	1
60	.19081	.98163	.20791	.97815	.22495	.97437	.24192	.97030	.25882	.96593	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	79°		78°		77°		76°		75°		

	15°		16°		17°		18°		19°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.25582	.96593	.27564	.96126	.29237	.95630	.30904	.95106	.32557	.94552	60
1	.25910	.96585	.27592	.96118	.29265	.95622	.30929	.95097	.32584	.94542	59
2	.25938	.96578	.27620	.96110	.29293	.95613	.30957	.95088	.32612	.94533	58
3	.25966	.96570	.27648	.96102	.29321	.95605	.30985	.95079	.32639	.94523	57
4	.25994	.96562	.27676	.96094	.29348	.95596	.31012	.95070	.32667	.94514	56
5	.26022	.96555	.27704	.96086	.29376	.95588	.31040	.95061	.32694	.94504	55
6	.26050	.96547	.27731	.96078	.29404	.95579	.31068	.95052	.32722	.94495	54
7	.26079	.96540	.27759	.96070	.29432	.95571	.31095	.95043	.32749	.94485	53
8	.26107	.96532	.27787	.96062	.29460	.95562	.31123	.95034	.32777	.94476	52
9	.26135	.96524	.27815	.96054	.29487	.95554	.31151	.95025	.32804	.94466	51
10	.26163	.96517	.27843	.96046	.29515	.95545	.31178	.95015	.32832	.94457	50
11	.26191	.96509	.27871	.96037	.29543	.95536	.31206	.95006	.32859	.94447	49
12	.26219	.96502	.27899	.96029	.29571	.95528	.31233	.94997	.32887	.94438	48
13	.26247	.96494	.27927	.96021	.29599	.95519	.31261	.94988	.32914	.94428	47
14	.26275	.96486	.27955	.96013	.29626	.95511	.31289	.94979	.32942	.94418	46
15	.26303	.96479	.27983	.96005	.29654	.95502	.31316	.94970	.32969	.94409	45
16	.26331	.96471	.28011	.95997	.29682	.95493	.31344	.94961	.32997	.94399	44
17	.26359	.96463	.28039	.95989	.29710	.95485	.31372	.94952	.33024	.94390	43
18	.26387	.96456	.28067	.95981	.29737	.95477	.31399	.94943	.33051	.94380	42
19	.26415	.96448	.28095	.95972	.29765	.95467	.31427	.94933	.33079	.94370	41
20	.26443	.96440	.28123	.95964	.29793	.95459	.31454	.94924	.33106	.94361	40
21	.26471	.96433	.28150	.95956	.29821	.95450	.31482	.94915	.33134	.94351	39
22	.26500	.96425	.28178	.95948	.29849	.95441	.31510	.94906	.33161	.94342	38
23	.26528	.96417	.28206	.95940	.29876	.95433	.31537	.94897	.33189	.94332	37
24	.26556	.96410	.28234	.95931	.29904	.95424	.31565	.94888	.33216	.94322	36
25	.26584	.96402	.28262	.95923	.29932	.95415	.31593	.94879	.33244	.94313	35
26	.26612	.96394	.28290	.95915	.29960	.95407	.31620	.94870	.33271	.94303	34
27	.26640	.96386	.28318	.95907	.29987	.95398	.31648	.94861	.33298	.94293	33
28	.26668	.96379	.28346	.95898	.30015	.95389	.31675	.94851	.33326	.94284	32
29	.26696	.96371	.28374	.95890	.30043	.95380	.31703	.94842	.33353	.94274	31
30	.26724	.96363	.28402	.95882	.30071	.95372	.31730	.94832	.33381	.94264	30
31	.26752	.96355	.28430	.95874	.30098	.95363	.31758	.94823	.33408	.94254	29
32	.26780	.96347	.28457	.95865	.30126	.95354	.31786	.94814	.33436	.94245	28
33	.26808	.96340	.28485	.95857	.30154	.95345	.31813	.94805	.33463	.94235	27
34	.26836	.96332	.28513	.95849	.30182	.95337	.31841	.94795	.33490	.94225	26
35	.26864	.96324	.28541	.95841	.30209	.95328	.31868	.94786	.33518	.94215	25
36	.26892	.96316	.28569	.95832	.30237	.95319	.31896	.94777	.33545	.94206	24
37	.26920	.96308	.28597	.95824	.30265	.95310	.31923	.94768	.33573	.94196	23
38	.26948	.96301	.28625	.95816	.30292	.95301	.31951	.94758	.33600	.94186	22
39	.26976	.96293	.28652	.95807	.30320	.95293	.31979	.94749	.33627	.94176	21
40	.27004	.96285	.28680	.95799	.30348	.95284	.32006	.94740	.33655	.94167	20
41	.27032	.96277	.28708	.95791	.30376	.95275	.32034	.94730	.33682	.94157	19
42	.27060	.96269	.28736	.95782	.30403	.95266	.32061	.94721	.33710	.94147	18
43	.27088	.96261	.28764	.95774	.30431	.95257	.32089	.94712	.33737	.94137	17
44	.27116	.96253	.28792	.95766	.30459	.95248	.32116	.94702	.33764	.94127	16
45	.27144	.96246	.28820	.95757	.30486	.95240	.32144	.94693	.33792	.94118	15
46	.27172	.96238	.28847	.95749	.30514	.95231	.32171	.94684	.33819	.94108	14
47	.27200	.96230	.28875	.95740	.30542	.95222	.32199	.94674	.33847	.94098	13
48	.27228	.96222	.28903	.95732	.30570	.95213	.32227	.94665	.33874	.94088	12
49	.27256	.96214	.28931	.95724	.30597	.95204	.32254	.94656	.33901	.94078	11
50	.27284	.96206	.28959	.95715	.30625	.95195	.32282	.94646	.33929	.94068	10
51	.27312	.96198	.28987	.95707	.30653	.95186	.32309	.94637	.33956	.94058	9
52	.27340	.96190	.29015	.95698	.30680	.95177	.32337	.94627	.33983	.94049	8
53	.27368	.96182	.29042	.95690	.30708	.95168	.32364	.94618	.34011	.94039	7
54	.27396	.96174	.29070	.95681	.30736	.95159	.32392	.94609	.34038	.94029	6
55	.27424	.96166	.29098	.95673	.30763	.95150	.32419	.94599	.34065	.94019	5
56	.27452	.96158	.29126	.95664	.30791	.95142	.32447	.94590	.34093	.94009	4
57	.27480	.96150	.29154	.95656	.30819	.95133	.32474	.94580	.34120	.93999	3
58	.27508	.96142	.29182	.95647	.30847	.95124	.32502	.94571	.34147	.93989	2
59	.27536	.96134	.29209	.95639	.30874	.95115	.32529	.94561	.34175	.93979	1
60	.27564	.96126	.29237	.95630	.30902	.95106	.32557	.94552	.34202	.93969	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	74°		73°		72°		71°		70°		

References

2

[illegible]

	25°		26°		27°		28°		29°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.42262	.90631	.43837	.89879	.45399	.89101	.46947	.88295	.48491	.87462	60
1	.42288	.90618	.43863	.89867	.45425	.89087	.46973	.88281	.48506	.87448	59
2	.42315	.90606	.43889	.89854	.45451	.89074	.46999	.88267	.48532	.87434	58
3	.42341	.90594	.43916	.89841	.45477	.89061	.47024	.88254	.48557	.87420	57
4	.42367	.90582	.43942	.89828	.45503	.89048	.47050	.88240	.48583	.87406	56
5	.42394	.90569	.43968	.89816	.45529	.89035	.47076	.88226	.48608	.87391	55
6	.42420	.90557	.43994	.89803	.45554	.89021	.47101	.88213	.48634	.87377	54
7	.42446	.90545	.44020	.89790	.45580	.89008	.47127	.88199	.48659	.87363	53
8	.42473	.90532	.44046	.89777	.45606	.88995	.47153	.88185	.48684	.87349	52
9	.42499	.90520	.44072	.89764	.45632	.88981	.47178	.88172	.48710	.87335	51
10	.42525	.90507	.44098	.89752	.45658	.88968	.47204	.88158	.48735	.87321	50
11	.42552	.90495	.44124	.89739	.45684	.88955	.47229	.88144	.48761	.87306	49
12	.42578	.90483	.44151	.89726	.45710	.88942	.47255	.88130	.48786	.87292	48
13	.42604	.90470	.44177	.89713	.45736	.88928	.47281	.88117	.48811	.87278	47
14	.42631	.90458	.44203	.89700	.45762	.88915	.47306	.88103	.48837	.87264	46
15	.42657	.90446	.44229	.89687	.45787	.88902	.47332	.88089	.48862	.87250	45
16	.42683	.90433	.44255	.89674	.45813	.88888	.47358	.88075	.48888	.87235	44
17	.42709	.90421	.44281	.89662	.45839	.88875	.47383	.88062	.48913	.87221	43
18	.42736	.90408	.44307	.89649	.45865	.88862	.47409	.88048	.48938	.87207	42
19	.42762	.90396	.44333	.89636	.45891	.88848	.47434	.88034	.48964	.87193	41
20	.42788	.90383	.44359	.89623	.45917	.88835	.47460	.88020	.48989	.87179	40
21	.42815	.90371	.44385	.89610	.45942	.88822	.47486	.88006	.49014	.87164	39
22	.42841	.90358	.44411	.89597	.45968	.88808	.47511	.87993	.49040	.87150	38
23	.42867	.90346	.44437	.89584	.45994	.88795	.47537	.87979	.49065	.87136	37
24	.42894	.90334	.44464	.89571	.46020	.88782	.47562	.87965	.49090	.87121	36
25	.42920	.90321	.44490	.89558	.46046	.88768	.47588	.87951	.49116	.87107	35
26	.42946	.90309	.44516	.89545	.46072	.88755	.47614	.87937	.49141	.87093	34
27	.42972	.90296	.44542	.89532	.46097	.88741	.47639	.87923	.49166	.87079	33
28	.42999	.90284	.44568	.89519	.46123	.88728	.47665	.87909	.49192	.87064	32
29	.43025	.90271	.44594	.89506	.46149	.88715	.47690	.87896	.49217	.87050	31
30	.43051	.90259	.44620	.89493	.46175	.88701	.47716	.87882	.49242	.87036	30
31	.43077	.90246	.44646	.89480	.46201	.88688	.47741	.87868	.49268	.87021	29
32	.43104	.90233	.44672	.89467	.46226	.88674	.47767	.87854	.49293	.87007	28
33	.43130	.90221	.44698	.89454	.46252	.88661	.47793	.87840	.49318	.86993	27
34	.43156	.90208	.44724	.89441	.46278	.88647	.47818	.87826	.49344	.86978	26
35	.43182	.90196	.44750	.89428	.46304	.88634	.47844	.87812	.49369	.86964	25
36	.43209	.90183	.44776	.89415	.46330	.88620	.47869	.87798	.49394	.86949	24
37	.43235	.90171	.44802	.89402	.46355	.88607	.47895	.87784	.49419	.86935	23
38	.43261	.90158	.44828	.89389	.46381	.88593	.47920	.87770	.49445	.86921	22
39	.43287	.90146	.44854	.89376	.46407	.88580	.47946	.87756	.49470	.86906	21
40	.43313	.90133	.44880	.89363	.46433	.88566	.47971	.87743	.49495	.86892	20
41	.43340	.90120	.44906	.89350	.46458	.88553	.47997	.87729	.49521	.86878	19
42	.43366	.90108	.44932	.89337	.46484	.88539	.48022	.87715	.49546	.86863	18
43	.43392	.90095	.44958	.89324	.46510	.88526	.48048	.87701	.49571	.86849	17
44	.43418	.90082	.44984	.89311	.46536	.88512	.48073	.87687	.49596	.86834	16
45	.43445	.90070	.45010	.89298	.46561	.88499	.48099	.87673	.49622	.86820	15
46	.43471	.90057	.45036	.89285	.46587	.88485	.48124	.87659	.49647	.86805	14
47	.43497	.90045	.45062	.89272	.46613	.88472	.48150	.87645	.49673	.86791	13
48	.43523	.90032	.45088	.89259	.46639	.88458	.48175	.87631	.49697	.86777	12
49	.43549	.90019	.45114	.89245	.46664	.88445	.48201	.87617	.49723	.86762	11
50	.43575	.90007	.45140	.89232	.46690	.88431	.48226	.87603	.49748	.86748	10
51	.43602	.89994	.45166	.89219	.46716	.88417	.48252	.87589	.49773	.86733	9
52	.43628	.89981	.45192	.89206	.46742	.88404	.48277	.87575	.49798	.86719	8
53	.43654	.89969	.45218	.89193	.46767	.88390	.48303	.87561	.49824	.86704	7
54	.43680	.89956	.45243	.89180	.46793	.88377	.48328	.87546	.49849	.86690	6
55	.43706	.89943	.45269	.89167	.46819	.88363	.48354	.87532	.49874	.86675	5
56	.43733	.89930	.45295	.89153	.46844	.88350	.48379	.87518	.49899	.86661	4
57	.43759	.89918	.45321	.89140	.46870	.88336	.48405	.87504	.49924	.86646	3
58	.43785	.89905	.45347	.89127	.46896	.88322	.48430	.87490	.49950	.86632	2
59	.43811	.89892	.45373	.89114	.46921	.88308	.48456	.87476	.49975	.86617	1
60	.43837	.89879	.45399	.89101	.46947	.88295	.48481	.87462	.49999	.86603	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	64°		63°		62°		61°		60°		

	30°		31°		32°		33°		34°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.50000	.86603	.51504	.85717	.52992	.84805	.54464	.83867	.55919	.82904	60
1	.50095	.86588	.51529	.85702	.53017	.84789	.54488	.83851	.55943	.82887	59
2	.50190	.86573	.51554	.85687	.53041	.84774	.54513	.83835	.55968	.82871	58
3	.50285	.86559	.51579	.85672	.53066	.84759	.54537	.83819	.55992	.82855	57
4	.50380	.86544	.51604	.85657	.53091	.84743	.54561	.83804	.56016	.82839	56
5	.50475	.86530	.51628	.85643	.53115	.84728	.54586	.83788	.56040	.82822	55
6	.50571	.86515	.51653	.85627	.53140	.84712	.54610	.83772	.56064	.82806	54
7	.50666	.86501	.51678	.85612	.53164	.84697	.54635	.83756	.56088	.82790	53
8	.50761	.86486	.51703	.85597	.53189	.84681	.54659	.83740	.56112	.82773	52
9	.50857	.86471	.51728	.85582	.53214	.84666	.54683	.83724	.56136	.82757	51
10	.50952	.86457	.51753	.85567	.53238	.84650	.54708	.83708	.56160	.82741	50
11	.51047	.86442	.51778	.85551	.53263	.84635	.54732	.83692	.56184	.82724	49
12	.51142	.86427	.51803	.85535	.53288	.84619	.54756	.83676	.56208	.82708	48
13	.51237	.86413	.51828	.85521	.53312	.84604	.54781	.83660	.56232	.82692	47
14	.51332	.86398	.51852	.85506	.53337	.84588	.54805	.83645	.56256	.82675	46
15	.51427	.86384	.51877	.85491	.53361	.84573	.54829	.83629	.56280	.82659	45
16	.51522	.86369	.51902	.85476	.53386	.84557	.54854	.83613	.56305	.82643	44
17	.51617	.86354	.51927	.85461	.53411	.84542	.54878	.83597	.56329	.82626	43
18	.51712	.86340	.51952	.85446	.53435	.84526	.54902	.83581	.56353	.82610	42
19	.51807	.86325	.51977	.85431	.53460	.84511	.54927	.83565	.56377	.82593	41
20	.51902	.86310	.52002	.85416	.53484	.84495	.54951	.83549	.56401	.82577	40
21	.51997	.86295	.52026	.85401	.53509	.84480	.54975	.83533	.56425	.82561	39
22	.52092	.86281	.52051	.85385	.53533	.84464	.54999	.83517	.56449	.82544	38
23	.52187	.86266	.52076	.85370	.53558	.84448	.55024	.83501	.56473	.82528	37
24	.52282	.86251	.52101	.85355	.53583	.84433	.55048	.83485	.56497	.82511	36
25	.52377	.86237	.52126	.85340	.53607	.84417	.55072	.83469	.56521	.82495	35
26	.52472	.86222	.52151	.85325	.53632	.84402	.55097	.83453	.56545	.82478	34
27	.52567	.86207	.52176	.85310	.53656	.84386	.55121	.83437	.56569	.82462	33
28	.52662	.86192	.52200	.85294	.53681	.84370	.55145	.83421	.56593	.82446	32
29	.52757	.86178	.52225	.85279	.53705	.84355	.55169	.83405	.56617	.82430	31
30	.52852	.86163	.52250	.85264	.53730	.84339	.55194	.83389	.56641	.82413	30
31	.52947	.86148	.52275	.85249	.53754	.84324	.55218	.83373	.56665	.82396	29
32	.53042	.86133	.52300	.85234	.53779	.84308	.55242	.83356	.56689	.82380	28
33	.53137	.86119	.52324	.85218	.53804	.84292	.55266	.83340	.56713	.82363	27
34	.53232	.86104	.52349	.85203	.53828	.84277	.55291	.83324	.56737	.82347	26
35	.53327	.86089	.52374	.85188	.53853	.84261	.55315	.83308	.56760	.82330	25
36	.53422	.86074	.52399	.85173	.53877	.84245	.55339	.83292	.56784	.82314	24
37	.53517	.86059	.52423	.85157	.53902	.84230	.55363	.83276	.56808	.82297	23
38	.53612	.86045	.52448	.85142	.53926	.84214	.55388	.83260	.56832	.82281	22
39	.53707	.86030	.52473	.85127	.53951	.84198	.55412	.83244	.56856	.82264	21
40	.53802	.86015	.52498	.85112	.53975	.84182	.55436	.83228	.56880	.82248	20
41	.53897	.86000	.52522	.85096	.54000	.84167	.55460	.83212	.56904	.82231	19
42	.53992	.85985	.52547	.85081	.54024	.84151	.55484	.83195	.56928	.82214	18
43	.54087	.85970	.52572	.85066	.54049	.84135	.55509	.83179	.56952	.82198	17
44	.54182	.85955	.52597	.85051	.54073	.84120	.55533	.83163	.56976	.82181	16
45	.54277	.85941	.52621	.85035	.54097	.84104	.55557	.83147	.57000	.82165	15
46	.54372	.85926	.52646	.85020	.54122	.84088	.55581	.83131	.57024	.82148	14
47	.54467	.85911	.52671	.85005	.54146	.84072	.55605	.83115	.57048	.82132	13
48	.54562	.85896	.52696	.84989	.54171	.84057	.55630	.83098	.57071	.82115	12
49	.54657	.85881	.52720	.84974	.54195	.84041	.55654	.83082	.57095	.82098	11
50	.54752	.85866	.52745	.84959	.54220	.84025	.55678	.83066	.57119	.82082	10
51	.54847	.85851	.52770	.84943	.54244	.84009	.55702	.83050	.57143	.82065	9
52	.54942	.85836	.52794	.84928	.54269	.83994	.55726	.83034	.57167	.82048	8
53	.55037	.85821	.52819	.84913	.54293	.83978	.55750	.83017	.57191	.82032	7
54	.55132	.85806	.52844	.84897	.54317	.83962	.55775	.83001	.57215	.82015	6
55	.55227	.85792	.52868	.84882	.54342	.83946	.55799	.82985	.57238	.81999	5
56	.55322	.85777	.52893	.84866	.54366	.83930	.55823	.82969	.57262	.81982	4
57	.55417	.85762	.52918	.84851	.54391	.83915	.55847	.82953	.57286	.81965	3
58	.55512	.85747	.52943	.84836	.54415	.83899	.55871	.82937	.57310	.81948	2
59	.55607	.85732	.52967	.84820	.54440	.83883	.55895	.82920	.57334	.81932	1
60	.55702	.85717	.52992	.84805	.54464	.83867	.55919	.82904	.57358	.81915	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	59°		58°		57°		56°		55°		

	35°		36°		37°		38°		39°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.57358	.81915	.58779	.80902	.60182	.79864	.61566	.78801	.62932	.77715	60
1	.57381	.81899	.58802	.80885	.60205	.79846	.61589	.78783	.62955	.77696	59
2	.57405	.81882	.58826	.80867	.60228	.79829	.61612	.78765	.62977	.77678	58
3	.57429	.81865	.58849	.80850	.60251	.79811	.61635	.78747	.63000	.77660	57
4	.57453	.81848	.58873	.80833	.60274	.79793	.61658	.78729	.63022	.77641	56
5	.57477	.81832	.58896	.80816	.60298	.79776	.61681	.78711	.63045	.77623	55
6	.57501	.81815	.58920	.80799	.60321	.79758	.61704	.78694	.63068	.77605	54
7	.57524	.81798	.58943	.80782	.60344	.79741	.61726	.78676	.63090	.77586	53
8	.57548	.81782	.58967	.80765	.60367	.79723	.61749	.78658	.63113	.77568	52
9	.57572	.81765	.58990	.80748	.60390	.79706	.61772	.78640	.63135	.77550	51
10	.57596	.81748	.59014	.80730	.60414	.79688	.61795	.78622	.63158	.77531	50
11	.57619	.81731	.59037	.80713	.60437	.79671	.61818	.78604	.63180	.77513	49
12	.57643	.81714	.59061	.80696	.60460	.79653	.61841	.78586	.63203	.77494	48
13	.57667	.81698	.59084	.80679	.60483	.79635	.61864	.78568	.63225	.77476	47
14	.57691	.81681	.59108	.80662	.60506	.79618	.61887	.78550	.63248	.77458	46
15	.57715	.81664	.59131	.80644	.60529	.79600	.61909	.78532	.63271	.77439	45
16	.57738	.81647	.59154	.80627	.60553	.79583	.61932	.78514	.63293	.77421	44
17	.57762	.81631	.59178	.80610	.60576	.79565	.61955	.78496	.63316	.77402	43
18	.57786	.81614	.59201	.80593	.60599	.79547	.61978	.78478	.63338	.77384	42
19	.57810	.81597	.59225	.80576	.60622	.79530	.62001	.78460	.63361	.77366	41
20	.57833	.81580	.59248	.80558	.60645	.79512	.62024	.78442	.63383	.77347	40
21	.57857	.81563	.59272	.80541	.60668	.79494	.62046	.78424	.63406	.77329	39
22	.57881	.81546	.59295	.80524	.60691	.79477	.62069	.78405	.63428	.77310	38
23	.57904	.81530	.59318	.80507	.60714	.79459	.62092	.78387	.63451	.77292	37
24	.57928	.81513	.59342	.80489	.60737	.79441	.62115	.78369	.63473	.77273	36
25	.57952	.81496	.59365	.80472	.60761	.79424	.62138	.78351	.63496	.77255	35
26	.57976	.81479	.59389	.80455	.60784	.79406	.62160	.78333	.63518	.77236	34
27	.57999	.81462	.59412	.80438	.60807	.79388	.62183	.78315	.63540	.77218	33
28	.58023	.81445	.59436	.80420	.60830	.79371	.62206	.78297	.63563	.77199	32
29	.58047	.81428	.59459	.80403	.60853	.79353	.62229	.78279	.63585	.77181	31
30	.58070	.81412	.59482	.80386	.60876	.79335	.62251	.78261	.63608	.77162	30
31	.58094	.81395	.59506	.80368	.60899	.79318	.62274	.78243	.63630	.77144	29
32	.58118	.81378	.59529	.80351	.60922	.79300	.62297	.78225	.63653	.77125	28
33	.58141	.81361	.59552	.80334	.60945	.79282	.62320	.78206	.63675	.77107	27
34	.58165	.81344	.59576	.80316	.60968	.79264	.62342	.78188	.63698	.77088	26
35	.58189	.81327	.59599	.80299	.60991	.79247	.62365	.78170	.63720	.77070	25
36	.58212	.81310	.59622	.80282	.61015	.79229	.62388	.78152	.63742	.77052	24
37	.58236	.81293	.59646	.80264	.61038	.79211	.62411	.78134	.63765	.77033	23
38	.58260	.81276	.59669	.80247	.61061	.79193	.62433	.78116	.63787	.77014	22
39	.58283	.81259	.59693	.80230	.61084	.79176	.62456	.78098	.63810	.76996	21
40	.58307	.81242	.59716	.80212	.61107	.79158	.62479	.78079	.63832	.76977	20
41	.58330	.81225	.59739	.80195	.61130	.79140	.62502	.78061	.63854	.76959	19
42	.58354	.81208	.59763	.80178	.61153	.79122	.62524	.78043	.63877	.76940	18
43	.58378	.81191	.59786	.80161	.61176	.79105	.62547	.78025	.63899	.76921	17
44	.58401	.81174	.59809	.80143	.61199	.79087	.62570	.78007	.63922	.76903	16
45	.58425	.81157	.59832	.80125	.61222	.79069	.62592	.77989	.63944	.76884	15
46	.58449	.81140	.59856	.80108	.61245	.79051	.62615	.77970	.63966	.76866	14
47	.58472	.81123	.59879	.80091	.61268	.79033	.62638	.77952	.63989	.76847	13
48	.58496	.81106	.59902	.80073	.61291	.79016	.62660	.77934	.64011	.76828	12
49	.58519	.81089	.59926	.80056	.61314	.78998	.62683	.77916	.64033	.76810	11
50	.58543	.81072	.59949	.80038	.61337	.78980	.62706	.77897	.64056	.76791	10
51	.58567	.81055	.59972	.80021	.61360	.78962	.62728	.77879	.64078	.76772	9
52	.58590	.81038	.59995	.80003	.61383	.78944	.62751	.77861	.64100	.76754	8
53	.58614	.81021	.60019	.79986	.61406	.78926	.62774	.77843	.64123	.76735	7
54	.58637	.81004	.60042	.79968	.61429	.78908	.62796	.77825	.64145	.76717	6
55	.58661	.80987	.60065	.79951	.61451	.78891	.62819	.77806	.64167	.76698	5
56	.58684	.80970	.60089	.79934	.61474	.78873	.62842	.77788	.64189	.76679	4
57	.58708	.80953	.60112	.79916	.61497	.78855	.62864	.77769	.64212	.76661	3
58	.58731	.80936	.60135	.79899	.61520	.78837	.62887	.77751	.64234	.76642	2
59	.58755	.80919	.60158	.79881	.61543	.78819	.62909	.77733	.64256	.76623	1
60	.58779	.80902	.60182	.79864	.61566	.78801	.62932	.77715	.64279	.76604	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	54°		53°		52°		51°		50°		

31

	40°		41°		42°		43°		44°		
	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	
0	.64279	.76604	.65606	.75471	.66913	.74314	.68200	.73135	.69466	.71934	60
1	.64301	.76586	.65628	.75452	.66935	.74295	.68221	.73116	.69487	.71914	59
2	.64323	.76567	.65650	.75433	.66956	.74276	.68242	.73096	.69508	.71894	58
3	.64346	.76548	.65672	.75414	.66978	.74256	.68264	.73076	.69529	.71875	57
4	.64368	.76529	.65694	.75395	.66999	.74237	.68285	.73056	.69549	.71855	56
5	.64391	.76511	.65716	.75375	.67021	.74217	.68306	.73036	.69570	.71835	55
6	.64412	.76492	.65738	.75356	.67043	.74198	.68327	.73016	.69591	.71815	54
7	.64435	.76473	.65759	.75337	.67064	.74178	.68349	.72996	.69612	.71795	53
8	.64457	.76455	.65781	.75317	.67086	.74159	.68370	.72976	.69633	.71775	52
9	.64479	.76436	.65803	.75298	.67107	.74139	.68391	.72957	.69654	.71755	51
10	.64501	.76417	.65825	.75280	.67129	.74120	.68412	.72937	.69675	.71735	50
11	.64524	.76398	.65847	.75261	.67151	.74100	.68434	.72917	.69696	.71715	49
12	.64546	.76380	.65869	.75241	.67172	.74080	.68455	.72897	.69717	.71695	48
13	.64568	.76361	.65891	.75222	.67194	.74061	.68476	.72877	.69737	.71675	47
14	.64590	.76342	.65913	.75203	.67215	.74041	.68497	.72857	.69758	.71655	46
15	.64612	.76323	.65935	.75184	.67237	.74022	.68518	.72837	.69779	.71635	45
16	.64635	.76304	.65956	.75165	.67258	.74002	.68539	.72817	.69800	.71615	44
17	.64657	.76286	.65978	.75146	.67280	.73983	.68561	.72797	.69821	.71595	43
18	.64679	.76267	.66000	.75126	.67301	.73963	.68582	.72777	.69842	.71575	42
19	.64701	.76248	.66022	.75107	.67323	.73944	.68603	.72757	.69863	.71555	41
20	.64723	.76229	.66044	.75088	.67344	.73924	.68624	.72737	.69883	.71535	40
21	.64746	.76210	.66066	.75069	.67366	.73904	.68645	.72717	.69904	.71515	39
22	.64768	.76192	.66088	.75050	.67387	.73885	.68666	.72697	.69925	.71495	38
23	.64790	.76173	.66109	.75030	.67409	.73865	.68688	.72677	.69946	.71475	37
24	.64812	.76154	.66131	.75011	.67430	.73846	.68709	.72657	.69966	.71455	36
25	.64834	.76135	.66153	.74992	.67452	.73826	.68730	.72637	.69987	.71435	35
26	.64856	.76116	.66175	.74973	.67473	.73806	.68751	.72617	.70008	.71415	34
27	.64878	.76097	.66197	.74953	.67495	.73787	.68772	.72597	.70029	.71395	33
28	.64901	.76078	.66218	.74934	.67516	.73767	.68793	.72577	.70049	.71375	32
29	.64923	.76059	.66240	.74915	.67538	.73747	.68814	.72557	.70070	.71355	31
30	.64945	.76041	.66262	.74896	.67559	.73728	.68835	.72537	.70091	.71335	30
31	.64967	.76022	.66284	.74876	.67580	.73708	.68857	.72517	.70112	.71315	29
32	.64989	.76003	.66306	.74857	.67602	.73688	.68878	.72497	.70132	.71295	28
33	.65011	.75984	.66327	.74838	.67623	.73669	.68899	.72477	.70153	.71275	27
34	.65033	.75965	.66349	.74818	.67645	.73649	.68921	.72457	.70174	.71255	26
35	.65055	.75946	.66370	.74799	.67666	.73629	.68942	.72437	.70195	.71235	25
36	.65077	.75927	.66392	.74780	.67688	.73610	.68963	.72417	.70215	.71215	24
37	.65100	.75907	.66414	.74760	.67709	.73590	.68983	.72397	.70236	.71195	23
38	.65122	.75889	.66435	.74741	.67730	.73570	.69004	.72377	.70257	.71175	22
39	.65144	.75870	.66458	.74722	.67752	.73551	.69025	.72357	.70277	.71155	21
40	.65166	.75851	.66480	.74703	.67773	.73531	.69046	.72337	.70298	.71135	20
41	.65188	.75832	.66501	.74683	.67795	.73511	.69067	.72317	.70319	.71115	19
42	.65210	.75813	.66523	.74664	.67816	.73491	.69088	.72297	.70339	.71095	18
43	.65232	.75794	.66545	.74644	.67837	.73472	.69109	.72277	.70360	.71075	17
44	.65254	.75775	.66566	.74625	.67859	.73452	.69130	.72257	.70381	.71055	16
45	.65276	.75756	.66588	.74606	.67880	.73432	.69151	.72237	.70401	.71035	15
46	.65298	.75737	.66610	.74586	.67901	.73413	.69172	.72217	.70422	.71015	14
47	.65320	.75719	.66632	.74567	.67923	.73393	.69193	.72197	.70442	.71005	13
48	.65342	.75700	.66653	.74547	.67944	.73373	.69214	.72176	.70461	.71057	12
49	.65364	.75680	.66675	.74528	.67965	.73353	.69235	.72156	.70482	.71037	11
50	.65386	.75661	.66697	.74509	.67987	.73333	.69256	.72136	.70503	.71016	10
51	.65408	.75642	.66718	.74489	.68008	.73314	.69277	.72116	.70523	.70996	9
52	.65430	.75623	.66740	.74470	.68029	.73294	.69298	.72095	.70544	.70975	8
53	.65452	.75604	.66762	.74451	.68051	.73274	.69319	.72075	.70565	.70955	7
54	.65474	.75585	.66783	.74431	.68072	.73254	.69340	.72055	.70586	.70935	6
55	.65496	.75566	.66805	.74412	.68093	.73234	.69361	.72035	.70607	.70915	5
56	.65518	.75547	.66827	.74392	.68115	.73215	.69382	.72015	.70628	.70905	4
57	.65540	.75528	.66848	.74373	.68136	.73195	.69403	.71995	.70649	.70905	3
58	.65562	.75509	.66870	.74353	.68157	.73175	.69424	.71974	.70670	.70925	2
59	.65584	.75490	.66891	.74334	.68179	.73155	.69445	.71954	.70690	.70925	1
60	.65606	.75471	.66913	.74314	.68200	.73135	.69466	.71934	.70711	.70916	0
	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	Cosine	Sine	
	49°		48°		47°		46°		45°		

	0°		1°		2°		3°		4°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.00000	Infin.	.01746	57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	60
1	.00023	3437.75	.01775	56.3506	.03591	28.3994	.05370	18.9755	.07022	14.2411	59
2	.00058	1718.87	.01804	55.4415	.03550	28.1664	.05499	18.8711	.07051	14.1821	58
3	.00087	1145.92	.01833	54.5513	.03579	27.9372	.05328	18.7678	.07080	14.1235	57
4	.00119	859.436	.01862	53.7086	.03609	27.7117	.05357	18.6656	.07110	14.0655	56
5	.00145	657.549	.01891	52.8821	.03638	27.4899	.05387	18.5645	.07139	14.0079	55
6	.00175	572.957	.01920	52.0807	.03667	27.2715	.05416	18.4645	.07168	13.9507	54
7	.00204	491.106	.01949	51.3032	.03696	27.0566	.05445	18.3655	.07197	13.8940	53
8	.00233	429.718	.01978	50.5485	.03725	26.8450	.05474	18.2677	.07226	13.8378	52
9	.00262	381.971	.02007	49.8157	.03754	26.6367	.05503	18.1708	.07255	13.7821	51
10	.00291	343.774	.02036	49.1039	.03783	26.4316	.05532	18.0750	.07285	13.7267	50
11	.00320	312.521	.02066	48.4121	.03812	26.2296	.05562	17.9802	.07314	13.6719	49
12	.00349	286.478	.02095	47.7395	.03841	26.0307	.05591	17.8863	.07344	13.6174	48
13	.00378	264.441	.02124	47.0853	.03871	25.8348	.05620	17.7934	.07373	13.5634	47
14	.00407	245.552	.02153	46.4489	.03900	25.6418	.05649	17.7015	.07402	13.5098	46
15	.00436	229.182	.02182	45.8294	.03929	25.4517	.05678	17.6106	.07431	13.4566	45
16	.00465	214.858	.02211	45.2261	.03958	25.2644	.05708	17.5205	.07461	13.4039	44
17	.00495	202.219	.02240	44.6386	.03987	25.0798	.05737	17.4314	.07490	13.3515	43
18	.00524	190.984	.02269	44.0661	.04016	24.8978	.05766	17.3432	.07519	13.2996	42
19	.00553	180.032	.02298	43.5081	.04046	24.7185	.05795	17.2558	.07548	13.2480	41
20	.00582	171.885	.02328	42.9641	.04075	24.5418	.05824	17.1693	.07578	13.1969	40
21	.00611	163.700	.02357	42.4335	.04104	24.3675	.05854	17.0837	.07607	13.1461	39
22	.00640	156.259	.02386	41.9158	.04133	24.1957	.05883	16.9990	.07636	13.0958	38
23	.00669	149.465	.02415	41.4106	.04162	24.0263	.05912	16.9150	.07665	13.0458	37
24	.00698	143.237	.02444	40.9174	.04191	23.8593	.05941	16.8319	.07695	12.9962	36
25	.00727	137.507	.02473	40.4358	.04220	23.6945	.05970	16.7496	.07724	12.9469	35
26	.00756	132.219	.02502	39.9655	.04250	23.5321	.05999	16.6681	.07753	12.8981	34
27	.00785	127.321	.02531	39.5059	.04279	23.3718	.06029	16.5874	.07782	12.8496	33
28	.00815	122.774	.02560	39.0568	.04308	23.2137	.06058	16.5075	.07812	12.8014	32
29	.00844	118.540	.02589	38.6177	.04337	23.0577	.06087	16.4283	.07841	12.7536	31
30	.00873	114.589	.02619	38.1885	.04366	22.9038	.06116	16.3499	.07870	12.7062	30
31	.00902	110.892	.02648	37.7686	.04395	22.7519	.06145	16.2722	.07899	12.6591	29
32	.00931	107.426	.02677	37.3579	.04424	22.6020	.06175	16.1952	.07929	12.6124	28
33	.00960	104.171	.02706	36.9560	.04454	22.4541	.06204	16.1190	.07958	12.5660	27
34	.00989	101.107	.02735	36.5627	.04483	22.3081	.06233	16.0435	.07987	12.5199	26
35	.01018	98.2179	.02764	36.1776	.04512	22.1640	.06262	15.9687	.08017	12.4742	25
36	.01047	95.4805	.02793	35.8006	.04541	22.0217	.06291	15.8945	.08046	12.4288	24
37	.01076	92.9085	.02822	35.4313	.04570	21.8813	.06321	15.8211	.08075	12.3838	23
38	.01105	90.4633	.02851	35.0695	.04599	21.7426	.06350	15.7483	.08104	12.3390	22
39	.01135	88.1436	.02881	34.7151	.04628	21.6056	.06379	15.6762	.08134	12.2946	21
40	.01164	85.9398	.02910	34.3678	.04658	21.4704	.06408	15.6048	.08163	12.2505	20
41	.01193	83.8435	.02939	34.0273	.04687	21.3369	.06437	15.5340	.08192	12.2067	19
42	.01222	81.8470	.02968	33.6935	.04716	21.2049	.06467	15.4638	.08221	12.1632	18
43	.01251	79.9434	.02997	33.3662	.04745	21.0747	.06496	15.3943	.08251	12.1201	17
44	.01280	78.1263	.03026	33.0452	.04774	20.9460	.06525	15.3254	.08280	12.0772	16
45	.01309	76.3900	.03055	32.7303	.04803	20.8188	.06554	15.2571	.08309	12.0346	15
46	.01338	74.7292	.03084	32.4213	.04833	20.6932	.06584	15.1893	.08339	11.9923	14
47	.01367	73.1390	.03114	32.1181	.04862	20.5691	.06613	15.1222	.08368	11.9504	13
48	.01396	71.6151	.03143	31.8205	.04891	20.4465	.06642	15.0557	.08397	11.9087	12
49	.01425	70.1533	.03172	31.5284	.04920	20.3253	.06671	14.9898	.08427	11.8673	11
50	.01455	68.7501	.03201	31.2416	.04949	20.2056	.06700	14.9244	.08456	11.8262	10
51	.01484	67.4019	.03230	30.9599	.04978	20.0872	.06730	14.8596	.08485	11.7853	9
52	.01513	66.1055	.03259	30.6833	.05007	19.9702	.06759	14.7954	.08514	11.7448	8
53	.01542	64.8580	.03288	30.4116	.05037	19.8546	.06788	14.7317	.08544	11.7045	7
54	.01571	63.6567	.03317	30.1446	.05066	19.7403	.06817	14.6685	.08573	11.6645	6
55	.01600	62.4992	.03346	29.8823	.05095	19.6273	.06847	14.6059	.08602	11.6248	5
56	.01629	61.3829	.03376	29.6245	.05124	19.5156	.06876	14.5438	.08632	11.5853	4
57	.01658	60.3058	.03405	29.3711	.05153	19.4051	.06905	14.4823	.08661	11.5461	3
58	.01687	59.2659	.03434	29.1220	.05182	19.2959	.06934	14.4212	.08690	11.5072	2
59	.01716	58.2612	.03463	28.8771	.05212	19.1879	.06963	14.3607	.08720	11.4685	1
60	.01746	57.2900	.03492	28.6363	.05241	19.0811	.06993	14.3007	.08749	11.4301	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	89°		88°		87°		86°		85°		

	5°		6°		7°		8°		9°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.08749	11.4301	.10510	9.51430	.12278	8.14435	.14054	7.11537	.15838	6.31375	60
1	.08778	11.3919	.10540	9.48781	.12308	8.12481	.14084	7.10038	.15868	6.30189	59
2	.08807	11.3540	.10569	9.46141	.12338	8.10536	.14113	7.08546	.15898	6.29007	58
3	.08837	11.3163	.10599	9.43515	.12367	8.08600	.14143	7.07059	.15928	6.27829	57
4	.08866	11.2789	.10628	9.40904	.12397	8.06674	.14173	7.05579	.15958	6.26655	56
5	.08895	11.2417	.10657	9.38307	.12426	8.04756	.14202	7.04105	.15988	6.25486	55
6	.08925	11.2043	.10687	9.35724	.12456	8.02843	.14232	7.02637	.16017	6.24321	54
7	.08954	11.1681	.10716	9.33155	.12485	8.00948	.14262	7.01174	.16047	6.23160	53
8	.08983	11.1316	.10746	9.30599	.12515	7.99058	.14291	6.99718	.16077	6.22003	52
9	.09013	11.0954	.10775	9.28050	.12544	7.97176	.14321	6.98263	.16107	6.20851	51
10	.09042	11.0594	.10805	9.25530	.12574	7.95302	.14351	6.96823	.16137	6.19703	50
11	.09071	11.0237	.10834	9.23016	.12603	7.93438	.14381	6.95385	.16167	6.18559	49
12	.09101	10.9882	.10863	9.20516	.12633	7.91582	.14410	6.93952	.16196	6.17410	48
13	.09130	10.9529	.10893	9.18028	.12662	7.89734	.14440	6.92525	.16226	6.16263	47
14	.09159	10.9178	.10922	9.15554	.12692	7.87895	.14470	6.91104	.16256	6.15151	46
15	.09189	10.8829	.10952	9.13093	.12722	7.86064	.14499	6.89688	.16286	6.14023	45
16	.09218	10.8483	.10981	9.10646	.12751	7.84242	.14529	6.88278	.16316	6.12899	44
17	.09247	10.8139	.11011	9.08211	.12781	7.82428	.14558	6.86874	.16346	6.11779	43
18	.09277	10.7797	.11040	9.05789	.12810	7.80622	.14588	6.85475	.16376	6.10664	42
19	.09306	10.7457	.11070	9.03379	.12840	7.78825	.14618	6.84082	.16405	6.09552	41
20	.09335	10.7119	.11099	9.00983	.12869	7.77035	.14648	6.82694	.16435	6.08444	40
21	.09365	10.6783	.11128	8.98598	.12899	7.75254	.14678	6.81312	.16465	6.07340	39
22	.09394	10.6450	.11158	8.96227	.12929	7.73480	.14707	6.79936	.16495	6.06240	38
23	.09423	10.6118	.11187	8.93867	.12958	7.71715	.14737	6.78564	.16525	6.05143	37
24	.09453	10.5789	.11217	8.91520	.12988	7.69957	.14767	6.77199	.16555	6.04051	36
25	.09482	10.5462	.11246	8.89185	.13017	7.68208	.14796	6.75838	.16585	6.02962	35
26	.09511	10.5136	.11276	8.86862	.13047	7.66466	.14826	6.74483	.16615	6.01878	34
27	.09541	10.4813	.11305	8.84551	.13076	7.64732	.14856	6.73133	.16645	6.00797	33
28	.09570	10.4491	.11335	8.82252	.13106	7.63005	.14886	6.71789	.16674	5.99720	32
29	.09600	10.4172	.11364	8.79964	.13136	7.61287	.14915	6.70450	.16704	5.98646	31
30	.09629	10.3854	.11394	8.77689	.13165	7.59575	.14945	6.69116	.16734	5.97576	30
31	.09658	10.3538	.11423	8.75425	.13195	7.57872	.14975	6.67787	.16764	5.96510	29
32	.09688	10.3224	.11452	8.73172	.13224	7.56176	.15005	6.66463	.16794	5.95448	28
33	.09717	10.2913	.11482	8.70931	.13254	7.54487	.15034	6.65144	.16824	5.94390	27
34	.09746	10.2602	.11511	8.68701	.13284	7.52806	.15064	6.63831	.16854	5.93335	26
35	.09776	10.2294	.11541	8.66482	.13313	7.51132	.15094	6.62523	.16884	5.92283	25
36	.09805	10.1988	.11570	8.64275	.13343	7.49465	.15124	6.61210	.16914	5.91236	24
37	.09834	10.1683	.11600	8.62078	.13372	7.47806	.15153	6.59921	.16944	5.90191	23
38	.09864	10.1381	.11629	8.59893	.13402	7.46154	.15183	6.58627	.16974	5.89151	22
39	.09893	10.1080	.11659	8.57718	.13432	7.44509	.15213	6.57339	.17004	5.88114	21
40	.09923	10.0780	.11688	8.55555	.13461	7.42871	.15243	6.56055	.17033	5.87080	20
41	.09952	10.0483	.11718	8.53402	.13491	7.41240	.15272	6.54777	.17063	5.86051	19
42	.09981	10.0187	.11747	8.51259	.13521	7.39616	.15302	6.53503	.17093	5.85026	18
43	.10011	9.98931	.11777	8.49128	.13550	7.37999	.15332	6.52234	.17123	5.84001	17
44	.10040	9.96007	.11806	8.47007	.13580	7.36389	.15362	6.50970	.17153	5.82982	16
45	.10069	9.93101	.11836	8.44896	.13609	7.34786	.15391	6.49710	.17183	5.81966	15
46	.10099	9.90211	.11865	8.42795	.13639	7.33190	.15421	6.48456	.17213	5.80953	14
47	.10128	9.87338	.11895	8.40705	.13668	7.31600	.15451	6.47206	.17243	5.79944	13
48	.10158	9.84482	.11924	8.38625	.13698	7.30018	.15481	6.45961	.17273	5.78938	12
49	.10187	9.81641	.11954	8.36555	.13728	7.28442	.15511	6.44720	.17303	5.77936	11
50	.10216	9.78817	.11983	8.34496	.13758	7.26873	.15540	6.43484	.17333	5.76937	10
51	.10246	9.76009	.12013	8.32446	.13787	7.25310	.15570	6.42253	.17363	5.75941	9
52	.10275	9.73217	.12042	8.30406	.13817	7.23754	.15600	6.41026	.17393	5.74949	8
53	.10305	9.70441	.12072	8.28376	.13846	7.22204	.15630	6.39804	.17423	5.73960	7
54	.10334	9.67680	.12101	8.26355	.13876	7.20661	.15660	6.38587	.17453	5.72976	6
55	.10363	9.64935	.12131	8.24345	.13906	7.19125	.15689	6.37374	.17483	5.71992	5
56	.10393	9.62205	.12160	8.22344	.13935	7.17594	.15719	6.36165	.17513	5.71013	4
57	.10422	9.59490	.12190	8.20352	.13965	7.16071	.15749	6.34961	.17543	5.70037	3
58	.10452	9.56791	.12219	8.18370	.13995	7.14553	.15779	6.33761	.17573	5.69064	2
59	.10481	9.54106	.12249	8.16398	.14024	7.13042	.15809	6.32566	.17603	5.68094	1
60	.10510	9.51436	.12278	8.14435	.14054	7.11537	.15838	6.31375	.17633	5.67128	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	84°		83°		82°		81°		80°		

	10°		11°		12°		13°		14°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.17633	5.67128	.19438	5.14455	.21256	4.70463	.23087	4.33148	.24933	4.01078	60
1	.17663	5.66165	.19468	5.13658	.21286	4.69791	.23117	4.32573	.24964	4.00582	59
2	.17693	5.65205	.19498	5.12862	.21316	4.69121	.23148	4.32001	.24995	4.00086	58
3	.17723	5.64244	.19529	5.12066	.21347	4.68452	.23179	4.31430	.25026	3.99592	57
4	.17753	5.63295	.19559	5.11270	.21377	4.67786	.23209	4.30860	.25056	3.99099	56
5	.17783	5.62344	.19589	5.10490	.21408	4.67121	.23240	4.30291	.25087	3.98607	55
6	.17813	5.61397	.19619	5.09704	.21438	4.66458	.23271	4.29724	.25118	3.98117	54
7	.17843	5.60452	.19649	5.08921	.21469	4.65797	.23301	4.29159	.25149	3.97627	53
8	.17873	5.59511	.19680	5.08139	.21499	4.65138	.23332	4.28595	.25180	3.97139	52
9	.17903	5.58573	.19710	5.07360	.21529	4.64480	.23363	4.28032	.25211	3.96651	51
10	.17933	5.57638	.19740	5.06584	.21560	4.63825	.23393	4.27471	.25242	3.96165	50
11	.17963	5.56706	.19770	5.05809	.21590	4.63171	.23424	4.26911	.25273	3.95680	49
12	.17993	5.55777	.19801	5.05037	.21621	4.62518	.23455	4.26352	.25304	3.95196	48
13	.18023	5.54851	.19831	5.04267	.21651	4.61868	.23485	4.25795	.25335	3.94713	47
14	.18053	5.53927	.19861	5.03499	.21682	4.61219	.23516	4.25239	.25366	3.94231	46
15	.18083	5.53007	.19891	5.02734	.21712	4.60572	.23547	4.24685	.25397	3.93751	45
16	.18113	5.52090	.19921	5.01971	.21743	4.59927	.23578	4.24132	.25428	3.93271	44
17	.18143	5.51176	.19952	5.01210	.21773	4.59283	.23608	4.23580	.25459	3.92793	43
18	.18173	5.50264	.19982	5.00451	.21804	4.58641	.23639	4.23030	.25490	3.92316	42
19	.18203	5.49356	.20012	4.99695	.21834	4.58001	.23670	4.22481	.25521	3.91839	41
20	.18233	5.48451	.20042	4.98940	.21864	4.57363	.23700	4.21933	.25552	3.91364	40
21	.18263	5.47548	.20073	4.98188	.21895	4.56726	.23731	4.21387	.25583	3.90890	39
22	.18293	5.46648	.20103	4.97438	.21925	4.56091	.23762	4.20842	.25614	3.90417	38
23	.18323	5.45751	.20133	4.96690	.21956	4.55458	.23793	4.20298	.25645	3.89945	37
24	.18353	5.44857	.20164	4.95945	.21986	4.54826	.23823	4.19756	.25676	3.89474	36
25	.18384	5.43966	.20194	4.95201	.22017	4.54196	.23854	4.19215	.25707	3.89004	35
26	.18414	5.43077	.20224	4.94460	.22047	4.53568	.23885	4.18675	.25738	3.88536	34
27	.18445	5.42192	.20254	4.93721	.22078	4.52941	.23916	4.18137	.25769	3.88068	33
28	.18474	5.41309	.20285	4.92984	.22108	4.52316	.23946	4.17600	.25800	3.87601	32
29	.18504	5.40429	.20315	4.92249	.22139	4.51693	.23977	4.17064	.25831	3.87136	31
30	.18534	5.39552	.20345	4.91516	.22169	4.51071	.24008	4.16530	.25862	3.86671	30
31	.18564	5.38677	.20376	4.90785	.22200	4.50451	.24039	4.15997	.25893	3.86208	29
32	.18594	5.37805	.20406	4.90056	.22231	4.49832	.24069	4.15465	.25924	3.85748	28
33	.18624	5.36930	.20436	4.89330	.22261	4.49215	.24100	4.14934	.25955	3.85284	27
34	.18654	5.36070	.20466	4.88605	.22292	4.48600	.24131	4.14405	.25986	3.84824	26
35	.18684	5.35206	.20497	4.87882	.22322	4.47986	.24162	4.13877	.26017	3.84364	25
36	.18714	5.34345	.20527	4.87162	.22353	4.47374	.24193	4.13350	.26048	3.83906	24
37	.18745	5.33487	.20557	4.86444	.22383	4.46764	.24223	4.12825	.26079	3.83449	23
38	.18775	5.32631	.20588	4.85727	.22414	4.46155	.24254	4.12301	.26110	3.82992	22
39	.18805	5.31778	.20618	4.85013	.22444	4.45548	.24285	4.11778	.26141	3.82537	21
40	.18835	5.30928	.20648	4.84302	.22475	4.44942	.24316	4.11256	.26172	3.82083	20
41	.18865	5.30080	.20679	4.83590	.22505	4.44338	.24347	4.10736	.26203	3.81630	19
42	.18895	5.29235	.20709	4.82882	.22536	4.43735	.24377	4.10216	.26235	3.81177	18
43	.18925	5.28393	.20739	4.82175	.22567	4.43134	.24408	4.09699	.26266	3.80726	17
44	.18955	5.27553	.20770	4.81471	.22597	4.42534	.24439	4.09182	.26297	3.80276	16
45	.18986	5.26715	.20800	4.80769	.22628	4.41936	.24470	4.08666	.26328	3.79827	15
46	.19016	5.25880	.20830	4.80068	.22658	4.41340	.24501	4.08152	.26359	3.79378	14
47	.19046	5.25048	.20861	4.79370	.22689	4.40745	.24532	4.07639	.26390	3.78931	13
48	.19076	5.24218	.20891	4.78673	.22719	4.40152	.24563	4.07127	.26421	3.78485	12
49	.19106	5.23391	.20921	4.77978	.22750	4.39560	.24593	4.06616	.26452	3.78040	11
50	.19136	5.22566	.20952	4.77286	.22781	4.38969	.24624	4.06107	.26483	3.77595	10
51	.19166	5.21744	.20982	4.76595	.22811	4.38381	.24655	4.05599	.26515	3.77152	9
52	.19197	5.20925	.21013	4.75906	.22842	4.37793	.24686	4.05092	.26546	3.76709	8
53	.19227	5.20107	.21043	4.75219	.22872	4.37207	.24717	4.04586	.26577	3.76268	7
54	.19257	5.19293	.21073	4.74534	.22903	4.36623	.24747	4.04081	.26608	3.75828	6
55	.19287	5.18480	.21104	4.73851	.22934	4.36040	.24778	4.03578	.26639	3.75388	5
56	.19317	5.17671	.21134	4.73170	.22964	4.35459	.24809	4.03076	.26670	3.74949	4
57	.19347	5.16863	.21164	4.72490	.22995	4.34879	.24840	4.02574	.26701	3.74512	3
58	.19378	5.16058	.21195	4.71813	.23026	4.34300	.24871	4.02074	.26733	3.74075	2
59	.19408	5.15256	.21225	4.71137	.23056	4.33723	.24902	4.01576	.26764	3.73640	1
60	.19438	5.14455	.21256	4.70463	.23087	4.33148	.24933	4.01078	.26795	3.73205	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	79°		78°		77°		76°		75°		

	15°		16°		17°		18°		19°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.26795	3.73205	.28765	3.48741	.30573	3.27085	.32492	3.07768	.34433	2.90421	60
1	.26820	3.72771	.28766	3.48359	.30605	3.26745	.32524	3.07464	.34465	2.90147	59
2	.26857	3.72338	.28768	3.47977	.30637	3.26406	.32556	3.07160	.34498	2.89873	58
3	.26888	3.71907	.28769	3.47596	.30669	3.26067	.32588	3.06857	.34530	2.89600	57
4	.26920	3.71476	.28800	3.47216	.30700	3.25729	.32621	3.06554	.34563	2.89327	56
5	.26951	3.71046	.28832	3.46837	.30732	3.25392	.32653	3.06252	.34596	2.89055	55
6	.26982	3.70616	.28864	3.46458	.30764	3.25055	.32685	3.05950	.34628	2.88783	54
7	.27013	3.70188	.28895	3.46080	.30796	3.24719	.32717	3.05649	.34661	2.88511	53
8	.27044	3.69761	.28927	3.45703	.30828	3.24383	.32749	3.05349	.34693	2.88240	52
9	.27076	3.69335	.28958	3.45327	.30860	3.24049	.32782	3.05049	.34726	2.87970	51
10	.27107	3.68909	.28990	3.44951	.30891	3.23714	.32814	3.04749	.34758	2.87700	50
11	.27138	3.68485	.29021	3.44576	.30923	3.23381	.32846	3.04450	.34791	2.87430	49
12	.27169	3.68061	.29053	3.44202	.30955	3.23048	.32878	3.04152	.34824	2.87161	48
13	.27201	3.67638	.29084	3.43827	.30987	3.22715	.32911	3.03854	.34856	2.86892	47
14	.27232	3.67217	.29116	3.43455	.31019	3.22384	.32943	3.03556	.34889	2.86624	46
15	.27263	3.66796	.29147	3.43084	.31051	3.22053	.32975	3.03260	.34922	2.86356	45
16	.27294	3.66376	.29179	3.42713	.31083	3.21722	.33007	3.02963	.34954	2.86089	44
17	.27326	3.65957	.29210	3.42343	.31115	3.21392	.33040	3.02667	.34987	2.85822	43
18	.27357	3.65538	.29242	3.41973	.31147	3.21063	.33072	3.02372	.35020	2.85555	42
19	.27388	3.65121	.29274	3.41604	.31178	3.20734	.33104	3.02077	.35052	2.85289	41
20	.27419	3.64705	.29305	3.41236	.31210	3.20406	.33136	3.01783	.35085	2.85023	40
21	.27451	3.64289	.29337	3.40869	.31242	3.20079	.33169	3.01489	.35118	2.84758	39
22	.27482	3.63874	.29368	3.40502	.31274	3.19752	.33201	3.01196	.35150	2.84494	38
23	.27513	3.63461	.29400	3.40136	.31306	3.19426	.33233	3.00903	.35183	2.84229	37
24	.27545	3.63048	.29432	3.39771	.31338	3.19100	.33266	3.00611	.35216	2.83965	36
25	.27576	3.62636	.29463	3.39406	.31370	3.18775	.33298	3.00319	.35248	2.83702	35
26	.27607	3.62224	.29495	3.39042	.31402	3.18451	.33330	3.00028	.35281	2.83439	34
27	.27638	3.61814	.29526	3.38679	.31434	3.18127	.33363	3.00738	.35314	2.83176	33
28	.27670	3.61405	.29558	3.38317	.31466	3.17804	.33395	3.00447	.35346	2.82914	32
29	.27701	3.60996	.29590	3.37955	.31498	3.17481	.33427	3.00158	.35379	2.82653	31
30	.27732	3.60588	.29621	3.37594	.31530	3.17159	.33460	3.00868	.35412	2.82391	30
31	.27764	3.60181	.29653	3.37234	.31562	3.16838	.33492	3.00580	.35445	2.82130	29
32	.27795	3.59775	.29685	3.36875	.31594	3.16517	.33524	3.00292	.35477	2.81870	28
33	.27826	3.59370	.29716	3.36516	.31626	3.16197	.33557	3.00004	.35510	2.81610	27
34	.27858	3.58966	.29748	3.36158	.31658	3.15877	.33589	3.00717	.35543	2.81350	26
35	.27889	3.58562	.29780	3.35800	.31690	3.15558	.33621	3.00430	.35576	2.81091	25
36	.27921	3.58160	.29811	3.35443	.31722	3.15240	.33654	3.00144	.35608	2.80833	24
37	.27952	3.57758	.29843	3.35087	.31754	3.14922	.33686	3.00858	.35641	2.80574	23
38	.27983	3.57357	.29875	3.34732	.31786	3.14605	.33718	3.00573	.35674	2.80316	22
39	.28015	3.56957	.29906	3.34377	.31818	3.14288	.33751	3.00288	.35707	2.80059	21
40	.28046	3.56557	.29938	3.34023	.31850	3.13972	.33783	3.00004	.35740	2.79802	20
41	.28077	3.56159	.29970	3.33670	.31882	3.13656	.33816	3.00721	.35772	2.79545	19
42	.28109	3.55761	.30001	3.33317	.31914	3.13341	.33848	3.00437	.35805	2.79289	18
43	.28140	3.55364	.30033	3.32965	.31946	3.13027	.33881	3.00155	.35838	2.79033	17
44	.28172	3.54968	.30065	3.32614	.31978	3.12713	.33913	3.00872	.35871	2.78778	16
45	.28203	3.54573	.30097	3.32264	.32010	3.12400	.33945	3.00589	.35904	2.78523	15
46	.28234	3.54179	.30128	3.31914	.32042	3.12087	.33978	3.00306	.35937	2.78269	14
47	.28266	3.53785	.30160	3.31565	.32074	3.11775	.34010	3.00028	.35969	2.78014	13
48	.28297	3.53393	.30192	3.31216	.32106	3.11464	.34043	3.00748	.36002	2.77761	12
49	.28329	3.53001	.30224	3.30868	.32139	3.11153	.34075	3.00468	.36035	2.77507	11
50	.28360	3.52609	.30255	3.30521	.32171	3.10842	.34108	3.00189	.36068	2.77254	10
51	.28391	3.52219	.30287	3.30174	.32203	3.10532	.34140	3.00910	.36101	2.77002	9
52	.28423	3.51829	.30319	3.29829	.32235	3.10223	.34173	3.00623	.36134	2.76750	8
53	.28454	3.51441	.30351	3.29483	.32267	3.09914	.34205	3.00335	.36167	2.76498	7
54	.28486	3.51051	.30382	3.29139	.32299	3.09606	.34238	3.00050	.36199	2.76247	6
55	.28517	3.50662	.30414	3.28795	.32331	3.09298	.34270	3.00769	.36232	2.75996	5
56	.28549	3.50270	.30446	3.28452	.32363	3.08991	.34303	3.00483	.36265	2.75746	4
57	.28580	3.49880	.30478	3.28109	.32396	3.08685	.34335	3.00202	.36298	2.75496	3
58	.28612	3.49509	.30509	3.27767	.32428	3.08379	.34368	3.00921	.36331	2.75246	2
59	.28643	3.49125	.30541	3.27426	.32460	3.08073	.34400	3.00640	.36364	2.74997	1
60	.28675	3.48741	.30573	3.27085	.32492	3.07768	.34433	3.00421	.36397	2.74748	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	74°		73°		72°		71°		70°		

	20°		21°		22°		23°		24°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.36397	2.74748	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	60
1	.36430	2.74499	.38420	2.60283	.40436	2.47302	.42482	2.35395	.44558	2.24428	59
2	.36463	2.74251	.38453	2.60057	.40470	2.47095	.42516	2.35205	.44593	2.24252	58
3	.36496	2.74004	.38487	2.59831	.40504	2.46888	.42551	2.35015	.44627	2.24077	57
4	.36529	2.73756	.38520	2.59606	.40538	2.46682	.42585	2.34825	.44662	2.23902	56
5	.36562	2.73509	.38553	2.59381	.40572	2.46476	.42619	2.34636	.44697	2.23727	55
6	.36595	2.73263	.38587	2.59156	.40606	2.46270	.42654	2.34447	.44732	2.23553	54
7	.36628	2.73017	.38620	2.58932	.40640	2.46065	.42688	2.34258	.44767	2.23378	53
8	.36661	2.72771	.38654	2.58708	.40674	2.45860	.42722	2.34069	.44802	2.23204	52
9	.36694	2.72526	.38687	2.58484	.40707	2.45655	.42757	2.33881	.44837	2.23030	51
10	.36727	2.72281	.38721	2.58261	.40741	2.45451	.42791	2.33693	.44872	2.22857	50
11	.36760	2.72035	.38754	2.58038	.40775	2.45246	.42826	2.33505	.44907	2.22683	49
12	.36793	2.71792	.38787	2.57815	.40809	2.45043	.42860	2.33317	.44942	2.22510	48
13	.36826	2.71548	.38821	2.57593	.40843	2.44839	.42894	2.33130	.44977	2.22337	47
14	.36859	2.71305	.38854	2.57371	.40877	2.44636	.42929	2.32943	.45012	2.22164	46
15	.36892	2.71062	.38888	2.57150	.40911	2.44433	.42963	2.32756	.45047	2.21990	45
16	.36925	2.70819	.38921	2.56928	.40945	2.44230	.42998	2.32570	.45082	2.21817	44
17	.36958	2.70577	.38955	2.56707	.40979	2.44027	.43032	2.32383	.45117	2.21644	43
18	.36991	2.70335	.38988	2.56487	.41013	2.43825	.43067	2.32197	.45152	2.21470	42
19	.37024	2.70094	.39022	2.56266	.41047	2.43622	.43101	2.32012	.45187	2.21297	41
20	.37057	2.69853	.39055	2.56046	.41081	2.43422	.43136	2.31826	.45222	2.21123	40
21	.37090	2.69612	.39089	2.55827	.41115	2.43220	.43170	2.31641	.45257	2.20951	39
22	.37123	2.69371	.39122	2.55608	.41149	2.43019	.43205	2.31456	.45292	2.20779	38
23	.37157	2.69131	.39156	2.55389	.41183	2.42818	.43239	2.31271	.45327	2.20610	37
24	.37190	2.68892	.39190	2.55170	.41217	2.42618	.43274	2.31086	.45362	2.20440	36
25	.37223	2.68653	.39223	2.54952	.41251	2.42418	.43308	2.30902	.45397	2.20278	35
26	.37256	2.68414	.39257	2.54734	.41285	2.42218	.43343	2.30718	.45432	2.20108	34
27	.37289	2.68175	.39290	2.54516	.41319	2.42019	.43378	2.30534	.45467	2.19938	33
28	.37322	2.67937	.39324	2.54299	.41353	2.41819	.43412	2.30351	.45502	2.19769	32
29	.37355	2.67700	.39357	2.54082	.41387	2.41620	.43447	2.30167	.45537	2.19599	31
30	.37388	2.67462	.39391	2.53865	.41421	2.41421	.43481	2.29984	.45573	2.19430	30
31	.37422	2.67225	.39425	2.53648	.41455	2.41223	.43516	2.29801	.45608	2.19261	29
32	.37455	2.66989	.39458	2.53432	.41489	2.41025	.43550	2.29619	.45643	2.19092	28
33	.37488	2.66752	.39492	2.53217	.41524	2.40827	.43585	2.29437	.45678	2.18923	27
34	.37521	2.66516	.39526	2.53001	.41558	2.40629	.43620	2.29254	.45713	2.18755	26
35	.37554	2.66281	.39559	2.52786	.41592	2.40432	.43654	2.29073	.45748	2.18587	25
36	.37588	2.66046	.39593	2.52571	.41626	2.40235	.43689	2.28891	.45784	2.18419	24
37	.37621	2.65811	.39626	2.52357	.41660	2.40038	.43724	2.28710	.45819	2.18251	23
38	.37654	2.65576	.39660	2.52142	.41694	2.39841	.43758	2.28528	.45854	2.18084	22
39	.37687	2.65342	.39694	2.51929	.41728	2.39645	.43793	2.28348	.45889	2.17916	21
40	.37720	2.65109	.39727	2.51715	.41763	2.39449	.43828	2.28167	.45924	2.17749	20
41	.37754	2.64875	.39761	2.51502	.41797	2.39253	.43862	2.27987	.45960	2.17582	19
42	.37787	2.64642	.39795	2.51289	.41831	2.39058	.43897	2.27806	.46000	2.17416	18
43	.37820	2.64410	.39829	2.51076	.41865	2.38863	.43932	2.27626	.46039	2.17249	17
44	.37853	2.64177	.39862	2.50864	.41899	2.38668	.43966	2.27447	.46080	2.17083	16
45	.37887	2.63945	.39896	2.50652	.41933	2.38473	.44001	2.27267	.46121	2.16917	15
46	.37920	2.63714	.39930	2.50440	.41968	2.38279	.44036	2.27088	.46163	2.16751	14
47	.37953	2.63483	.39963	2.50229	.42002	2.38084	.44071	2.26909	.46205	2.16585	13
48	.37986	2.63252	.39997	2.50018	.42036	2.37891	.44105	2.26730	.46247	2.16420	12
49	.38020	2.63022	.40031	2.49807	.42070	2.37697	.44140	2.26552	.46289	2.16255	11
50	.38053	2.62791	.40065	2.49597	.42105	2.37504	.44175	2.26374	.46331	2.16090	10
51	.38086	2.62561	.40098	2.49386	.42139	2.37311	.44210	2.26196	.46372	2.15925	9
52	.38120	2.62332	.40132	2.49177	.42173	2.37118	.44244	2.26018	.46413	2.15760	8
53	.38153	2.62103	.40166	2.48967	.42207	2.36925	.44279	2.25840	.46454	2.15595	7
54	.38186	2.61874	.40200	2.48758	.42242	2.36733	.44314	2.25663	.46495	2.15432	6
55	.38220	2.61646	.40234	2.48549	.42276	2.36541	.44349	2.25486	.46536	2.15268	5
56	.38253	2.61418	.40267	2.48340	.42310	2.36349	.44384	2.25309	.46578	2.15104	4
57	.38286	2.61190	.40301	2.48132	.42345	2.36158	.44418	2.25132	.46620	2.14940	3
58	.38320	2.60963	.40335	2.47924	.42379	2.35967	.44453	2.24956	.46662	2.14777	2
59	.38353	2.60736	.40369	2.47716	.42413	2.35776	.44488	2.24780	.46705	2.14614	1
60	.38386	2.60509	.40403	2.47509	.42447	2.35585	.44523	2.24604	.46747	2.14451	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	69°		68°		67°		66°		65°		

	25°		26°		27°		28°		29°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.46631	2.14451	.48773	2.05030	.50953	1.96261	.53171	1.88673	.55431	1.80405	60
1	.46666	2.14288	.48809	2.04879	.50989	1.96120	.53208	1.87941	.55469	1.80281	59
2	.46702	2.14125	.48845	2.04728	.51026	1.95979	.53246	1.87809	.55507	1.80158	58
3	.46737	2.13963	.48881	2.04577	.51063	1.95838	.53283	1.87677	.55545	1.80034	57
4	.46772	2.13801	.48917	2.04426	.51099	1.95698	.53320	1.87546	.55583	1.79911	56
5	.46808	2.13639	.48953	2.04276	.51136	1.95557	.53358	1.87415	.55621	1.79788	55
6	.46843	2.13477	.48989	2.04125	.51173	1.95417	.53395	1.87283	.55659	1.79665	54
7	.46879	2.13316	.49026	2.03975	.51209	1.95277	.53432	1.87152	.55697	1.79542	53
8	.46914	2.13154	.49062	2.03825	.51246	1.95137	.53470	1.87021	.55736	1.79419	52
9	.46950	2.12993	.49098	2.03675	.51283	1.94997	.53507	1.86891	.55774	1.79296	51
10	.46985	2.12832	.49134	2.03526	.51319	1.94858	.53545	1.86760	.55812	1.79174	50
11	.47021	2.12671	.49170	2.03376	.51356	1.94718	.53582	1.86630	.55850	1.79051	49
12	.47056	2.12511	.49206	2.03227	.51393	1.94579	.53620	1.86499	.55888	1.78929	48
13	.47092	2.12350	.49242	2.03078	.51430	1.94440	.53657	1.86369	.55926	1.78807	47
14	.47128	2.12189	.49278	2.02929	.51467	1.94301	.53694	1.86239	.55964	1.78685	46
15	.47163	2.12030	.49315	2.02780	.51503	1.94162	.53732	1.86109	.56003	1.78563	45
16	.47199	2.11871	.49351	2.02631	.51540	1.94023	.53769	1.85979	.56041	1.78441	44
17	.47234	2.11711	.49387	2.02483	.51577	1.93885	.53807	1.85850	.56079	1.78319	43
18	.47270	2.11552	.49423	2.02335	.51614	1.93746	.53844	1.85720	.56117	1.78197	42
19	.47305	2.11392	.49459	2.02187	.51651	1.93608	.53882	1.85591	.56156	1.78075	41
20	.47341	2.11233	.49495	2.02039	.51688	1.93470	.53920	1.85462	.56194	1.77953	40
21	.47377	2.11075	.49532	2.01891	.51724	1.93332	.53957	1.85333	.56232	1.77831	39
22	.47412	2.10916	.49568	2.01743	.51761	1.93195	.53995	1.85204	.56270	1.77713	38
23	.47448	2.10758	.49604	2.01596	.51798	1.93057	.54032	1.85075	.56309	1.77595	37
24	.47483	2.10600	.49640	2.01449	.51835	1.92920	.54070	1.84946	.56347	1.77477	36
25	.47519	2.10442	.49677	2.01302	.51872	1.92782	.54107	1.84818	.56385	1.77359	35
26	.47555	2.10284	.49713	2.01155	.51909	1.92645	.54145	1.84689	.56424	1.77239	34
27	.47590	2.10126	.49749	2.01008	.51946	1.92508	.54183	1.84561	.56462	1.77119	33
28	.47626	2.09969	.49786	2.00862	.51983	1.92371	.54220	1.84433	.56501	1.76999	32
29	.47662	2.09811	.49822	2.00715	.52020	1.92235	.54258	1.84305	.56539	1.76879	31
30	.47698	2.09654	.49858	2.00569	.52057	1.92098	.54296	1.84177	.56577	1.76749	30
31	.47733	2.09498	.49894	2.00423	.52094	1.91962	.54333	1.84049	.56616	1.76629	29
32	.47769	2.09341	.49931	2.00277	.52131	1.91826	.54371	1.83922	.56654	1.76510	28
33	.47805	2.09184	.49967	2.00131	.52168	1.91690	.54409	1.83794	.56693	1.76390	27
34	.47840	2.09028	.50004	1.99986	.52205	1.91554	.54446	1.83667	.56731	1.76271	26
35	.47876	2.08872	.50040	1.99841	.52242	1.91418	.54484	1.83540	.56769	1.76151	25
36	.47912	2.08716	.50076	1.99695	.52279	1.91282	.54522	1.83413	.56808	1.76032	24
37	.47948	2.08560	.50113	1.99550	.52316	1.91147	.54560	1.83286	.56846	1.75913	23
38	.47984	2.08405	.50149	1.99406	.52353	1.91012	.54597	1.83159	.56885	1.75794	22
39	.48019	2.08250	.50185	1.99261	.52390	1.90877	.54635	1.83033	.56923	1.75675	21
40	.48055	2.08094	.50222	1.99116	.52427	1.90741	.54673	1.82906	.56962	1.75556	20
41	.48091	2.07939	.50258	1.98972	.52464	1.90607	.54711	1.82780	.57000	1.75437	19
42	.48127	2.07785	.50295	1.98828	.52501	1.90472	.54748	1.82654	.57039	1.75319	18
43	.48163	2.07632	.50331	1.98684	.52538	1.90337	.54786	1.82528	.57078	1.75200	17
44	.48198	2.07476	.50368	1.98540	.52575	1.90203	.54824	1.82402	.57116	1.75082	16
45	.48234	2.07321	.50404	1.98396	.52613	1.90069	.54862	1.82276	.57155	1.74964	15
46	.48270	2.07167	.50441	1.98253	.52650	1.89935	.54900	1.82150	.57193	1.74846	14
47	.48306	2.07014	.50477	1.98110	.52687	1.89801	.54938	1.82025	.57232	1.74728	13
48	.48342	2.06860	.50514	1.97966	.52724	1.89667	.54975	1.81899	.57271	1.74610	12
49	.48378	2.06706	.50550	1.97823	.52761	1.89533	.55013	1.81774	.57309	1.74492	11
50	.48414	2.06553	.50587	1.97681	.52798	1.89400	.55051	1.81649	.57348	1.74375	10
51	.48450	2.06400	.50623	1.97538	.52836	1.89266	.55089	1.81524	.57386	1.74257	9
52	.48486	2.06247	.50660	1.97395	.52873	1.89133	.55127	1.81399	.57425	1.74140	8
53	.48521	2.06094	.50696	1.97252	.52910	1.89000	.55165	1.81274	.57464	1.74022	7
54	.48557	2.05942	.50733	1.97111	.52947	1.88867	.55203	1.81150	.57503	1.73905	6
55	.48593	2.05790	.50769	1.96969	.52985	1.88734	.55241	1.81025	.57541	1.73788	5
56	.48629	2.05637	.50806	1.96827	.53022	1.88602	.55279	1.80901	.57580	1.73671	4
57	.48665	2.05485	.50843	1.96685	.53059	1.88469	.55317	1.80777	.57619	1.73555	3
58	.48701	2.05333	.50879	1.96544	.53096	1.88337	.55355	1.80653	.57657	1.73438	2
59	.48737	2.05182	.50916	1.96402	.53134	1.88205	.55393	1.80529	.57696	1.73321	1
60	.48773	2.05030	.50953	1.96261	.53171	1.88073	.55431	1.80405	.57735	1.73205	0
	Cotang Tang		Cotang Tang		Cotang Tang		Cotang Tang		Cotang Tang		
	64°		63°		62°		61°		60°		

	30°		31°		32°		33°		34°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.57735	1.73205	.60086	1.66428	.62487	1.60033	.64941	1.53086	.67431	1.48236	60
1	.57774	1.73089	.60126	1.66318	.62527	1.59930	.64982	1.53888	.67493	1.48163	59
2	.57813	1.72973	.60165	1.66209	.62568	1.59826	.65024	1.53701	.67536	1.48070	58
3	.57851	1.72857	.60205	1.66099	.62608	1.59723	.65065	1.53603	.67578	1.47977	57
4	.57890	1.72741	.60245	1.65990	.62649	1.59620	.65106	1.53505	.67620	1.47885	56
5	.57929	1.72625	.60284	1.65881	.62689	1.59517	.65148	1.53407	.67663	1.47792	55
6	.57968	1.72509	.60324	1.65772	.62730	1.59414	.65189	1.53300	.67705	1.47699	54
7	.58007	1.72393	.60364	1.65663	.62770	1.59311	.65231	1.53202	.67748	1.47607	53
8	.58046	1.72278	.60403	1.65554	.62811	1.59208	.65272	1.53205	.67790	1.47514	52
9	.58085	1.72163	.60443	1.65445	.62852	1.59105	.65314	1.53107	.67832	1.47422	51
10	.58124	1.72047	.60483	1.65337	.62892	1.59002	.65355	1.53010	.67875	1.47330	50
11	.58162	1.71932	.60522	1.65228	.62933	1.58900	.65397	1.52913	.67917	1.47238	49
12	.58201	1.71817	.60562	1.65120	.62973	1.58797	.65438	1.52816	.67960	1.47146	48
13	.58240	1.71702	.60602	1.65011	.63014	1.58695	.65480	1.52719	.68002	1.47053	47
14	.58279	1.71588	.60642	1.64903	.63055	1.58593	.65521	1.52622	.68045	1.46962	46
15	.58318	1.71473	.60681	1.64795	.63095	1.58490	.65563	1.52525	.68088	1.46870	45
16	.58357	1.71358	.60721	1.64687	.63136	1.58388	.65604	1.52429	.68130	1.46778	44
17	.58396	1.71244	.60761	1.64579	.63177	1.58286	.65646	1.52332	.68173	1.46686	43
18	.58435	1.71129	.60801	1.64471	.63217	1.58184	.65688	1.52235	.68215	1.46595	42
19	.58474	1.71015	.60841	1.64363	.63258	1.58083	.65729	1.52139	.68258	1.46503	41
20	.58513	1.70901	.60881	1.64256	.63299	1.57981	.65771	1.52043	.68301	1.46411	40
21	.58552	1.70787	.60921	1.64148	.63340	1.57879	.65813	1.51946	.68343	1.46320	39
22	.58591	1.70673	.60960	1.64041	.63380	1.57777	.65854	1.51850	.68386	1.46228	38
23	.58631	1.70560	.61000	1.63934	.63421	1.57676	.65896	1.51754	.68429	1.46137	37
24	.58670	1.70446	.61040	1.63826	.63462	1.57575	.65938	1.51658	.68471	1.46046	36
25	.58709	1.70332	.61080	1.63719	.63503	1.57474	.65980	1.51562	.68514	1.45955	35
26	.58748	1.70219	.61120	1.63612	.63544	1.57372	.66021	1.51466	.68557	1.45864	34
27	.58787	1.70106	.61160	1.63505	.63584	1.57271	.66063	1.51370	.68600	1.45773	33
28	.58826	1.69992	.61200	1.63398	.63625	1.57170	.66105	1.51275	.68642	1.45682	32
29	.58865	1.69879	.61240	1.63292	.63666	1.57069	.66147	1.51179	.68685	1.45592	31
30	.58905	1.69766	.61280	1.63185	.63707	1.56969	.66189	1.51084	.68728	1.45501	30
31	.58944	1.69653	.61320	1.63079	.63748	1.56868	.66230	1.50988	.68771	1.45410	29
32	.58983	1.69541	.61360	1.62972	.63789	1.56767	.66272	1.50893	.68814	1.45320	28
33	.59022	1.69428	.61400	1.62866	.63830	1.56667	.66314	1.50797	.68857	1.45229	27
34	.59061	1.69316	.61440	1.62760	.63871	1.56566	.66356	1.50702	.68900	1.45137	26
35	.59101	1.69203	.61480	1.62654	.63912	1.56466	.66398	1.50607	.68942	1.45046	25
36	.59140	1.69091	.61520	1.62548	.63953	1.56366	.66440	1.50512	.68985	1.44955	24
37	.59179	1.68979	.61561	1.62442	.63994	1.56265	.66482	1.50417	.69028	1.44864	23
38	.59218	1.68866	.61601	1.62336	.64035	1.56165	.66524	1.50322	.69071	1.44773	22
39	.59258	1.68754	.61641	1.62230	.64076	1.56065	.66566	1.50228	.69114	1.44682	21
40	.59297	1.68643	.61681	1.62125	.64117	1.55966	.66608	1.50133	.69157	1.44592	20
41	.59336	1.68531	.61721	1.62019	.64158	1.55866	.66650	1.50038	.69200	1.44502	19
42	.59376	1.68419	.61761	1.61914	.64199	1.55766	.66692	1.49944	.69243	1.44412	18
43	.59415	1.68308	.61801	1.61808	.64240	1.55666	.66734	1.49849	.69286	1.44320	17
44	.59454	1.68196	.61842	1.61703	.64281	1.55567	.66776	1.49755	.69329	1.44230	16
45	.59494	1.68085	.61882	1.61598	.64322	1.55467	.66818	1.49661	.69372	1.44140	15
46	.59533	1.67974	.61922	1.61493	.64363	1.55368	.66860	1.49566	.69416	1.44050	14
47	.59573	1.67863	.61962	1.61388	.64404	1.55269	.66902	1.49472	.69459	1.43970	13
48	.59612	1.67752	.62003	1.61283	.64446	1.55170	.66944	1.49378	.69502	1.43881	12
49	.59651	1.67641	.62043	1.61179	.64487	1.55071	.66986	1.49284	.69545	1.43792	11
50	.59691	1.67530	.62083	1.61074	.64528	1.54972	.67028	1.49190	.69588	1.43703	10
51	.59730	1.67419	.62124	1.60970	.64569	1.54873	.67071	1.49097	.69631	1.43614	9
52	.59770	1.67309	.62164	1.60865	.64610	1.54774	.67113	1.49003	.69675	1.43525	8
53	.59809	1.67198	.62204	1.60761	.64652	1.54675	.67155	1.48909	.69718	1.43436	7
54	.59849	1.67088	.62245	1.60657	.64693	1.54576	.67197	1.48816	.69761	1.43347	6
55	.59888	1.66978	.62285	1.60553	.64734	1.54477	.67239	1.48722	.69804	1.43258	5
56	.59928	1.66867	.62325	1.60449	.64775	1.54379	.67282	1.48629	.69847	1.43169	4
57	.59967	1.66757	.62366	1.60345	.64817	1.54281	.67324	1.48536	.69890	1.43080	3
58	.60007	1.66647	.62406	1.60241	.64858	1.54183	.67366	1.48442	.69934	1.42992	2
59	.60046	1.66538	.62446	1.60137	.64899	1.54085	.67409	1.48349	.69977	1.42903	1
60	.60086	1.66428	.62487	1.60033	.64941	1.53986	.67451	1.48256	.70021	1.42815	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	59°		58°		57°		56°		55°		

°	35°		36°		37°		38°		39°		°
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.70021	.1.42815	.70054	.1.37638	.75355	.1.32704	.78129	.1.27994	.80978	.1.23490	60
1	.70064	.1.42726	.70099	.1.37554	.75401	.1.32624	.78175	.1.27917	.81027	.1.23416	59
2	.70107	.1.42638	.70143	.1.37470	.75447	.1.32544	.78222	.1.27841	.81075	.1.23343	58
3	.70151	.1.42550	.70188	.1.37386	.75492	.1.32464	.78269	.1.27766	.81123	.1.23270	57
4	.70194	.1.42462	.70232	.1.37302	.75538	.1.32384	.78316	.1.27691	.81171	.1.23196	56
5	.70238	.1.42374	.70277	.1.37218	.75584	.1.32304	.78363	.1.27616	.81219	.1.23123	55
6	.70281	.1.42286	.70321	.1.37134	.75630	.1.32224	.78410	.1.27541	.81267	.1.23050	54
7	.70325	.1.42198	.70366	.1.37050	.75675	.1.32144	.78457	.1.27466	.81316	.1.22977	53
8	.70368	.1.42110	.70410	.1.36967	.75721	.1.32064	.78504	.1.27391	.81364	.1.22904	52
9	.70412	.1.42022	.70455	.1.36883	.75767	.1.31984	.78551	.1.27316	.81413	.1.22831	51
10	.70455	.1.41934	.70500	.1.36800	.75812	.1.31904	.78598	.1.27239	.81461	.1.22758	50
11	.70499	.1.41847	.70544	.1.36716	.75858	.1.31825	.78645	.1.27163	.81510	.1.22685	49
12	.70542	.1.41759	.70589	.1.36633	.75904	.1.31745	.78692	.1.27087	.81558	.1.22612	48
13	.70586	.1.41672	.70634	.1.36549	.75950	.1.31666	.78739	.1.27011	.81606	.1.22539	47
14	.70629	.1.41584	.70682	.1.36466	.75996	.1.31586	.78786	.1.26935	.81655	.1.22467	46
15	.70673	.1.41497	.70732	.1.36383	.76042	.1.31507	.78834	.1.26859	.81703	.1.22394	45
16	.70717	.1.41409	.70786	.1.36300	.76088	.1.31427	.78881	.1.26784	.81752	.1.22321	44
17	.70760	.1.41322	.70837	.1.36217	.76134	.1.31348	.78928	.1.26708	.81800	.1.22249	43
18	.70804	.1.41235	.70889	.1.36134	.76180	.1.31269	.78975	.1.26632	.81849	.1.22176	42
19	.70848	.1.41148	.70934	.1.36051	.76226	.1.31190	.79022	.1.26556	.81898	.1.22104	41
20	.70891	.1.41061	.70981	.1.35967	.76272	.1.31110	.79070	.1.26481	.81946	.1.22031	40
21	.70935	.1.40974	.71029	.1.35885	.76318	.1.31031	.79117	.1.26405	.81995	.1.21959	39
22	.70979	.1.40887	.71077	.1.35802	.76364	.1.30952	.79164	.1.26329	.82044	.1.21886	38
23	.71023	.1.40800	.71126	.1.35719	.76410	.1.30873	.79212	.1.26254	.82092	.1.21814	37
24	.71066	.1.40714	.71176	.1.35637	.76456	.1.30795	.79259	.1.26179	.82141	.1.21742	36
25	.71110	.1.40627	.71227	.1.35554	.76502	.1.30716	.79306	.1.26103	.82190	.1.21670	35
26	.71154	.1.40540	.71279	.1.35472	.76548	.1.30637	.79354	.1.26028	.82238	.1.21598	34
27	.71198	.1.40454	.71332	.1.35389	.76594	.1.30558	.79401	.1.25953	.82287	.1.21526	33
28	.71242	.1.40367	.71387	.1.35307	.76640	.1.30480	.79449	.1.25877	.82336	.1.21454	32
29	.71285	.1.40281	.71442	.1.35224	.76686	.1.30401	.79496	.1.25802	.82385	.1.21383	31
30	.71329	.1.40195	.71497	.1.35142	.76732	.1.30323	.79544	.1.25717	.82434	.1.21310	30
31	.71373	.1.40109	.71548	.1.35060	.76779	.1.30244	.79591	.1.25642	.82483	.1.21238	29
32	.71417	.1.40022	.71606	.1.34978	.76825	.1.30166	.79639	.1.25567	.82531	.1.21166	28
33	.71461	.1.39936	.71657	.1.34896	.76871	.1.30087	.79686	.1.25492	.82580	.1.21094	27
34	.71505	.1.39850	.71710	.1.34814	.76918	.1.30009	.79734	.1.25417	.82629	.1.21023	26
35	.71549	.1.39764	.71762	.1.34732	.76964	.1.29931	.79781	.1.25343	.82678	.1.20951	25
36	.71593	.1.39679	.71817	.1.34650	.77010	.1.29853	.79829	.1.25268	.82727	.1.20879	24
37	.71637	.1.39593	.71871	.1.34568	.77057	.1.29775	.79877	.1.25193	.82776	.1.20808	23
38	.71681	.1.39507	.71927	.1.34485	.77103	.1.29696	.79924	.1.25118	.82825	.1.20736	22
39	.71725	.1.39421	.71982	.1.34405	.77149	.1.29618	.79972	.1.25044	.82874	.1.20665	21
40	.71769	.1.39336	.72044	.1.34323	.77196	.1.29541	.80020	.1.24969	.82923	.1.20593	20
41	.71813	.1.39250	.72102	.1.34242	.77242	.1.29463	.80067	.1.24895	.82972	.1.20522	19
42	.71857	.1.39165	.72158	.1.34160	.77289	.1.29385	.80115	.1.24820	.83022	.1.20451	18
43	.71901	.1.39079	.72217	.1.34079	.77335	.1.29307	.80163	.1.24746	.83071	.1.20379	17
44	.71946	.1.38994	.72276	.1.33998	.77382	.1.29229	.80211	.1.24672	.83120	.1.20308	16
45	.71990	.1.38909	.72336	.1.33916	.77428	.1.29152	.80258	.1.24597	.83169	.1.20237	15
46	.72034	.1.38824	.72397	.1.33835	.77475	.1.29074	.80306	.1.24523	.83218	.1.20166	14
47	.72078	.1.38738	.72458	.1.33754	.77521	.1.28997	.80354	.1.24449	.83268	.1.20095	13
48	.72122	.1.38653	.72519	.1.33673	.77568	.1.28919	.80402	.1.24375	.83317	.1.20024	12
49	.72167	.1.38568	.72580	.1.33592	.77615	.1.28842	.80450	.1.24301	.83366	.1.19953	11
50	.72211	.1.38484	.72640	.1.33511	.77661	.1.28764	.80498	.1.24227	.83415	.1.19882	10
51	.72255	.1.38399	.72704	.1.33430	.77708	.1.28687	.80546	.1.24153	.83465	.1.19811	9
52	.72299	.1.38314	.72767	.1.33349	.77754	.1.28610	.80594	.1.24079	.83514	.1.19740	8
53	.72344	.1.38229	.72831	.1.33268	.77801	.1.28533	.80642	.1.24005	.83564	.1.19669	7
54	.72388	.1.38145	.72895	.1.33187	.77848	.1.28456	.80690	.1.23931	.83613	.1.19599	6
55	.72432	.1.38060	.72959	.1.33107	.77895	.1.28379	.80738	.1.23858	.83662	.1.19528	5
56	.72477	.1.37976	.73024	.1.33026	.77941	.1.28302	.80786	.1.23784	.83712	.1.19457	4
57	.72521	.1.37891	.73089	.1.32946	.77988	.1.28225	.80834	.1.23710	.83761	.1.19387	3
58	.72565	.1.37807	.73154	.1.32865	.78035	.1.28148	.80882	.1.23637	.83811	.1.19316	2
59	.72610	.1.37722	.73219	.1.32785	.78082	.1.28071	.80930	.1.23563	.83860	.1.19246	1
60	.72654	.1.37638	.73285	.1.32704	.78129	.1.27994	.80978	.1.23490	.83910	.1.19175	0
Cotang		Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
54°		53°		52°		51°		50°			

	40°		41°		42°		43°		44°		
	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	
0	.83910	1.19175	.86920	1.15037	.90040	1.11061	.93252	1.07237	.96569	1.03553	60
1	.83960	1.19105	.86980	1.14969	.90093	1.10996	.93306	1.07174	.96625	1.03493	59
2	.84009	1.19035	.87031	1.14902	.90146	1.10931	.93360	1.07112	.96681	1.03433	58
3	.84059	1.18964	.87082	1.14834	.90199	1.10867	.93415	1.07049	.96738	1.03372	57
4	.84108	1.18894	.87133	1.14767	.90251	1.10802	.93469	1.06987	.96794	1.03312	56
5	.84158	1.18824	.87184	1.14700	.90304	1.10737	.93524	1.06925	.96850	1.03252	55
6	.84208	1.18754	.87236	1.14632	.90357	1.10672	.93578	1.06862	.96907	1.03192	54
7	.84258	1.18684	.87287	1.14565	.90410	1.10607	.93633	1.06800	.96963	1.03132	53
8	.84307	1.18614	.87338	1.14498	.90463	1.10543	.93688	1.06738	.97020	1.03072	52
9	.84357	1.18544	.87389	1.14430	.90516	1.10478	.93742	1.06676	.97076	1.03012	51
10	.84407	1.18474	.87441	1.14363	.90569	1.10414	.93797	1.06613	.97133	1.02952	50
11	.84457	1.18404	.87492	1.14296	.90621	1.10349	.93852	1.06551	.97189	1.02892	49
12	.84507	1.18334	.87543	1.14229	.90674	1.10285	.93906	1.06489	.97246	1.02832	48
13	.84556	1.18264	.87595	1.14162	.90727	1.10220	.93961	1.06427	.97302	1.02772	47
14	.84606	1.18194	.87646	1.14095	.90781	1.10155	.94016	1.06365	.97359	1.02713	46
15	.84656	1.18125	.87698	1.14028	.90834	1.10091	.94071	1.06303	.97416	1.02653	45
16	.84706	1.18055	.87749	1.13961	.90887	1.10027	.94125	1.06241	.97472	1.02593	44
17	.84756	1.17986	.87801	1.13894	.90940	1.09963	.94180	1.06179	.97529	1.02533	43
18	.84806	1.17916	.87852	1.13828	.90993	1.09899	.94235	1.06117	.97586	1.02474	42
19	.84856	1.17846	.87904	1.13761	.91046	1.09834	.94290	1.06056	.97643	1.02414	41
20	.84906	1.17777	.87955	1.13694	.91099	1.09770	.94345	1.05994	.97700	1.02355	40
21	.84956	1.17708	.88007	1.13627	.91153	1.09706	.94400	1.05932	.97756	1.02295	39
22	.85006	1.17638	.88059	1.13561	.91206	1.09642	.94455	1.05870	.97813	1.02236	38
23	.85057	1.17569	.88110	1.13494	.91259	1.09580	.94510	1.05808	.97870	1.02176	37
24	.85107	1.17500	.88162	1.13428	.91313	1.09514	.94565	1.05747	.97927	1.02117	36
25	.85157	1.17430	.88214	1.13361	.91366	1.09450	.94620	1.05685	.97984	1.02057	35
26	.85207	1.17361	.88265	1.13295	.91419	1.09386	.94676	1.05624	.98041	1.01998	34
27	.85257	1.17292	.88317	1.13228	.91473	1.09322	.94731	1.05562	.98098	1.01939	33
28	.85308	1.17223	.88369	1.13162	.91526	1.09258	.94786	1.05501	.98155	1.01879	32
29	.85358	1.17154	.88421	1.13096	.91580	1.09195	.94841	1.05439	.98213	1.01820	31
30	.85408	1.17085	.88473	1.13029	.91633	1.09131	.94896	1.05378	.98270	1.01761	30
31	.85458	1.17016	.88524	1.12963	.91687	1.09067	.94952	1.05317	.98327	1.01702	29
32	.85509	1.16947	.88576	1.12897	.91740	1.09003	.95007	1.05255	.98384	1.01642	28
33	.85559	1.16878	.88628	1.12831	.91794	1.08940	.95062	1.05194	.98441	1.01583	27
34	.85609	1.16809	.88680	1.12765	.91847	1.08876	.95118	1.05133	.98499	1.01524	26
35	.85660	1.16741	.88733	1.12699	.91901	1.08813	.95173	1.05072	.98556	1.01465	25
36	.85710	1.16672	.88784	1.12633	.91955	1.08749	.95228	1.05010	.98613	1.01406	24
37	.85761	1.16603	.88836	1.12567	.92008	1.08686	.95284	1.04949	.98671	1.01347	23
38	.85811	1.16535	.88888	1.12501	.92062	1.08622	.95340	1.04888	.98728	1.01288	22
39	.85862	1.16466	.88940	1.12435	.92116	1.08559	.95395	1.04827	.98786	1.01229	21
40	.85912	1.16398	.88992	1.12369	.92170	1.08496	.95451	1.04766	.98843	1.01170	20
41	.85963	1.16329	.89045	1.12303	.92224	1.08432	.95506	1.04705	.98901	1.01112	19
42	.86014	1.16261	.89097	1.12238	.92277	1.08369	.95562	1.04644	.98958	1.01053	18
43	.86064	1.16192	.89149	1.12172	.92331	1.08306	.95618	1.04583	.99016	1.00994	17
44	.86115	1.16124	.89201	1.12106	.92385	1.08243	.95673	1.04522	.99073	1.00935	16
45	.86166	1.16056	.89253	1.12041	.92439	1.08179	.95729	1.04461	.99131	1.00876	15
46	.86216	1.15987	.89306	1.11975	.92493	1.08116	.95785	1.04401	.99189	1.00818	14
47	.86267	1.15919	.89358	1.11909	.92547	1.08053	.95841	1.04340	.99247	1.00759	13
48	.86318	1.15851	.89410	1.11844	.92601	1.07990	.95897	1.04279	.99304	1.00701	12
49	.86368	1.15783	.89463	1.11778	.92655	1.07927	.95952	1.04218	.99362	1.00642	11
50	.86419	1.15715	.89515	1.11713	.92709	1.07864	.96008	1.04158	.99420	1.00583	10
51	.86470	1.15647	.89567	1.11648	.92763	1.07801	.96064	1.04097	.99478	1.00525	9
52	.86521	1.15579	.89620	1.11582	.92817	1.07738	.96120	1.04036	.99536	1.00467	8
53	.86572	1.15511	.89672	1.11517	.92872	1.07676	.96176	1.03976	.99594	1.00408	7
54	.86623	1.15443	.89725	1.11452	.92926	1.07613	.96232	1.03915	.99652	1.00350	6
55	.86674	1.15375	.89777	1.11387	.92980	1.07550	.96288	1.03855	.99710	1.00291	5
56	.86725	1.15308	.89830	1.11321	.93034	1.07487	.96344	1.03794	.99768	1.00233	4
57	.86776	1.15240	.89883	1.11256	.93088	1.07425	.96400	1.03734	.99826	1.00175	3
58	.86827	1.15172	.89935	1.11191	.93143	1.07362	.96457	1.03674	.99884	1.00116	2
59	.86878	1.15104	.89988	1.11126	.93197	1.07299	.96513	1.03613	.99942	1.00058	1
60	.86929	1.15037	.90040	1.11061	.93252	1.07237	.96569	1.03553	1.00000	1.00000	0
	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	Cotang	Tang	
	49°		48°		47°		46°		45°		

THE PROPERTIES OF SATURATED STEAM.

Pressure above Vacuum in Pounds per Square Inch.	Temperature, Fahrenheit Degrees.	Quantities of Heat in British Thermal Units.			Weight of a Cubic Foot of Steam in Pounds.	Volume.	
		Required to Raise Temperature of the Water from 32° to t°.	Total Latent Heat at Pressure P.	Total Heat above 32°.		Of a Pound of Steam in Cubic Feet.	Ratio of Vol. of Steam to Vol. of Eq. Weight of Dist. Water at Temp. of Maximum Density.
1	2	3	4	5	6	7	8
<i>p</i>	<i>t</i>	<i>q</i>	<i>L</i>	<i>H</i>	<i>W</i>	<i>V</i>	<i>R</i>
1	102.018	70.040	1043.015	1113.055	.003027	330.4	20623
2	126.302	94.368	1026.094	1120.462	.005818	171.9	10730
3	141.654	109.764	1015.380	1125.144	.008522	117.3	7325
4	153.122	121.271	1007.370	1128.641	.011172	89.51	5588
5	162.370	130.563	1000.899	1131.462	.013781	72.56	4530
6	170.173	138.401	995.441	1133.842	.016357	61.14	3816
7	176.945	145.213	990.695	1135.908	.018908	52.89	3302
8	182.952	151.255	986.485	1137.740	.021436	46.65	2912
9	188.357	156.699	982.690	1139.389	.023944	41.77	2607
10	193.284	161.660	979.232	1140.892	.026437	37.83	2361
11	197.814	166.225	976.050	1142.275	.028911	34.59	2159
12	202.012	170.457	973.098	1143.555	.031376	31.87	1990
13	205.929	174.402	970.346	1144.748	.033828	29.56	1845
14	209.604	178.112	967.757	1145.869	.036265	27.58	1721
14.69	212.000	180.531	966.069	1146.600	.037928	26.37	1646
15	213.067	181.608	965.318	1146.926	.038688	25.85	1614
16	216.347	184.919	963.007	1147.926	.041109	24.33	1519
17	219.452	188.056	960.818	1148.874	.043519	22.98	1434
18	222.424	191.058	958.721	1149.779	.045920	21.78	1359
19	225.255	193.918	956.725	1150.643	.048312	20.70	1292

1	2	3	4	5	6	7	8
p	t	q	L	H	W	V	R
20	227.964	196.655	954.814	1151.469	.050696	19.73	1231.0
22	233.069	201.817	951.209	1153.026	.055446	18.04	1126.0
24	237.803	206.610	947.861	1154.471	.060171	16.62	1038.0
26	242.225	211.089	944.730	1155.819	.064870	15.42	962.3
28	246.376	215.293	941.791	1157.084	.069545	14.38	897.6
30	250.293	219.261	939.019	1158.280	.074201	13.48	841.3
32	254.002	223.021	936.389	1159.410	.078839	12.68	791.8
34	257.523	226.594	933.891	1160.485	.083461	11.98	748.0
36	260.883	230.001	931.508	1161.509	.088067	11.36	708.8
38	264.093	233.261	929.227	1162.488	.092657	10.79	673.7
40	267.168	236.386	927.040	1163.426	.097231	10.28	642.0
42	270.122	239.389	924.940	1164.329	.101794	9.826	613.3
44	272.965	242.275	922.919	1165.194	.106345	9.403	587.0
46	275.704	245.061	920.968	1166.029	.110884	9.018	563.0
48	278.348	247.752	919.084	1166.836	.115411	8.665	540.9
50	280.904	250.355	917.260	1167.615	.119927	8.338	520.5
52	283.381	252.875	915.494	1168.369	.124433	8.037	501.7
54	285.781	255.321	913.781	1169.102	.128928	7.756	484.2
56	288.111	257.695	912.118	1169.813	.133414	7.496	467.9
58	290.374	260.002	910.501	1170.503	.137892	7.252	452.7
60	292.575	262.248	908.928	1171.176	.142362	7.024	438.5
62	294.717	264.433	907.396	1171.829	.146824	6.811	425.2
64	296.805	266.566	905.900	1172.466	.151277	6.610	412.6
66	298.842	268.644	904.443	1173.087	.155721	6.422	400.8
68	300.831	270.674	903.020	1173.694	.160157	6.244	389.8
70	302.774	272.657	901.629	1174.286	.164584	6.076	379.3
72	304.669	274.597	900.269	1174.866	.169003	5.917	369.4
74	306.526	276.493	898.938	1175.431	.173417	5.767	360.0
76	308.344	278.350	897.635	1175.985	.177825	5.624	351.1
78	310.123	280.170	896.359	1176.529	.182229	5.488	342.6
80	311.866	281.952	895.108	1177.060	.186627	5.358	334.5
82	313.576	283.701	893.879	1177.580	.191017	5.235	326.8
84	315.250	285.414	892.677	1178.091	.195401	5.118	319.5
86	316.893	287.096	891.496	1178.592	.199781	5.006	312.5
88	318.510	288.750	890.335	1179.085	.204155	4.898	305.8

TABLES AND FORMULAS.

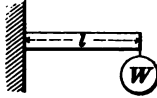
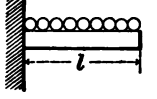
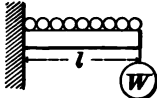
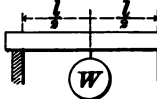
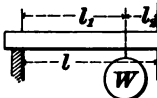
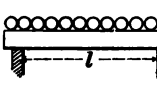
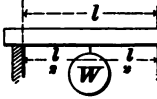
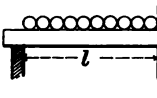
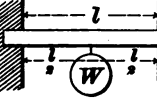
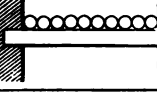
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1	2	3	4	5	6	7	8
p	t	q	L	H	W	V	R
90	320.094	290.373	889.196	1179.569	208525	4.796	299.4
92	321.653	291.970	888.075	1180.045	212892	4.697	293.2
94	323.183	293.539	886.972	1180.511	217253	4.603	287.3
96	324.688	295.083	885.887	1180.970	221604	4.513	281.7
98	326.169	296.601	884.821	1181.422	225950	4.426	276.3
100	327.625	298.093	883.773	1181.866	230293	4.342	271.1
105	331.169	301.731	881.214	1182.945	241139	4.147	258.9
110	334.582	305.242	878.744	1183.986	251947	3.969	247.8
115	337.874	308.621	876.371	1184.992	262732	3.806	237.6
120	341.058	311.885	874.076	1185.961	273500	3.656	228.3
125	344.136	315.051	871.848	1186.899	284243	3.518	219.6
130	347.121	318.121	869.688	1187.809	294961	3.390	211.6
135	350.015	321.105	867.590	1188.695	305659	3.272	204.2
140	352.827	324.003	865.552	1189.555	316338	3.161	197.3
145	355.562	326.823	863.567	1190.390	326998	3.058	190.9
150	358.223	329.566	861.634	1191.200	337643	2.962	184.9
160	363.346	334.850	857.912	1192.762	358886	2.786	173.9
170	368.226	339.892	854.359	1194.251	380071	2.631	164.3
180	372.886	344.708	850.963	1195.671	401201	2.493	155.6
190	377.352	349.329	847.703	1197.032	422280	2.368	147.8
200	381.636	353.766	844.573	1198.339	443310	2.256	140.8
210	385.759	358.041	841.556	1199.597	464295	2.154	134.5
220	389.736	362.168	838.642	1200.810	485237	2.061	128.7
230	393.575	366.152	835.828	1201.980	506139	1.976	123.3
240	397.285	370.008	833.103	1203.111	527003	1.898	118.5
250	400.883	373.750	830.459	1204.209	547831	1.825	114.0
260	404.370	377.377	827.896	1205.273	568626	1.759	109.8
270	407.755	380.905	825.401	1206.306	589390	1.697	105.9
280	411.048	384.337	822.973	1207.310	610124	1.639	102.3
290	414.250	387.677	820.609	1208.286	630829	1.585	99.0
300	417.371	390.933	818.305	1209.238	651506	1.535	95.8

MOMENTS OF INERTIA.

Form of Section.	Dotted Line Shows Position of Neutral Axis.	A	I	c
1. Rect-angle ...		$b d$	$\frac{1}{12} b d^3$	$\frac{1}{2} d$
2. Square ...		d^2	$\frac{1}{12} d^4$	$\frac{1}{2} d$
3. Axis through Diagonal		d^2	$\frac{1}{12} d^4$	$.707 d$
4. Hollow Square		$d^2 - d_1^2$	$\frac{1}{12} (d^4 - d_1^4)$	$\frac{1}{2} d$
5. Hollow Rect-angle, I or Channel Iron		$b d - b_1 d_1$	$\frac{1}{12} (b d^3 - b_1 d_1^3)$	$\frac{1}{2} d$
6. Triangle		$\frac{1}{2} b d$	$\frac{1}{30} b d^3$	$\frac{2}{3} d$
7. Cross....		$t d + t_1 b$	$\frac{1}{12} (t d^3 + b t_1^3)$	$\frac{1}{2} d$
8. Angle Iron....		$b d - b_1 d_1$	$\frac{(b d^3 - b_1 d_1^3) - 4 b d b_1 d_1 (d - d_1)^2}{12 (b d - b_1 d_1)}$	$\frac{d}{2} + \frac{b_1 d_1}{2} \left(\frac{d - d_1}{b d - b_1 d_1} \right)$
9. Circle....		$\frac{\pi}{4} d^2$	$\frac{\pi d^4}{64}$	$\frac{1}{2} d$
10. Hollow Circle...		$\frac{\pi}{4} (d^2 - d_1^2)$	$\frac{\pi (d^4 - d_1^4)}{64}$	$\frac{1}{2} d$
11. Ellipse...		$\frac{\pi}{4} b d$	$\frac{\pi b d^3}{64}$	$\frac{1}{2} d$
12. Hollow Ellipse..		$\frac{\pi}{4} (b d - b_1 d_1)$	$\frac{\pi (b d^3 - b_1 d_1^3)}{64}$	$\frac{1}{2} d$

BENDING MOMENTS AND DEFLECTIONS.

Manner of Supporting Beams.	Maximum Bending Moment, M .	Maximum Deflection, s .	Remarks.
1. 	Wl	$\frac{1}{8} \frac{W'l^3}{EI}$	Cantilever, load at free end.
2. 	$W_1l_1 + W_2l_2$		Cantilever, more than one load.
3. 	$\frac{wl^2}{2}$	$\frac{1}{8} \frac{W'l^3}{EI}$	Cantilever, uniform load w lb. per unit of length. $W' = w l$.
4. 	$\frac{wl^2}{2} + Wl$	$\frac{1}{3} \frac{W'l^3}{EI} + \frac{1}{8} \frac{W'l^3}{EI}$	Cantilever, load partly uniform, partly concentrated.
5. 	$\frac{Wl}{4}$	$\frac{1}{48} \frac{W'l^3}{EI}$	Simple beam, load at middle.
6. 	$W \frac{l_1l_2}{l}$		Simple beam, load at some other point than the middle.
7. 	$\frac{wl^2}{8}$	$\frac{5}{384} \frac{W'l^3}{EI}$	Simple beam, uniformly loaded.
8. 	$\frac{3}{16} Wl$	$.0182 \frac{W'l^3}{EI}$	One end fixed, other end supported, load in the middle.
9. 	$\frac{wl^2}{8}$	$.0054 \frac{W'l^3}{EI}$	One end fixed, other end supported, uniformly loaded.
10. 	$\frac{Wl}{8}$	$\frac{1}{192} \frac{W'l^3}{EI}$	Both ends fixed, load in the middle.
11. 	$\frac{wl^2}{12}$	$\frac{1}{384} \frac{W'l^3}{EI}$	Both ends fixed, uniformly loaded.

SPECIFIC GRAVITIES AND WEIGHTS PER CUBIC FOOT.

METALS.

Substance.	Specific Gravity.	Weight per Cubic Foot in Pounds.
Osmium	23.00	1,437.5
Platinum	21.50	1,343.8
Gold	19.50	1,218.8
Mercury	13.60	850.0
Lead (cast).....	11.35	709.4
Silver.....	10.50	656.3
Copper (cast).....	8.79	549.4
Brass	8.38	523.8
Wrought Iron	7.68	480.0
Cast Iron	7.21	450.0
Steel	7.84	490.0
Tin (cast).....	7.29	455.6
Zinc (cast)	6.86	428.8
Antimony.....	6.71	419.4
Aluminum	2.50	156.3

WOODS.

Substance.	Specific Gravity.	Weight per Cubic Foot in Pounds.
Ash	.845	52.80
Beech	.852	53.25
Cedar.....	.561	35.06
Cork	.240	15.00
Ebony (American).....	1.331	83.19
Lignum-vitæ	1.333	83.30
Maple	.750	46.88
Oak (old)	1.170	73.10
Spruce.....	.500	31.25
Pine (yellow).....	.660	41.20
Pine (white).....	.554	34.60
Walnut	.671	41.90

LIQUIDS.

Substance.	Specific Gravity.	Weight per Cubic Foot in Pounds.
Acetic Acid	1.062	66.4
Nitric Acid	1.217	76.1
Sulphuric Acid	1.841	115.1
Muriatic Acid	1.200	75.0
Alcohol	.800	50.0
Turpentine.....	.870	54.4
Sea Water (ordinary)	1.026	64.1
Milk	1.032	64.5

GASES.

At 32° F., and under a Pressure of One Atmosphere.

Substance.	Specific Gravity.	Weight per Cubic Foot in Pounds.
Atmospheric Air.....	1.0000	.08073
Carbonic Acid.....	1.5290	.12344
Carbonic Oxide.....	.9674	.07810
Chlorine	2.4400	.19700
Oxygen	1.1056	.08925
Nitrogen.....	.9736	.07860
Smoke (bituminous coal).....	.1020	.00815
Smoke (wood).....	.0900	.00727
*Steam at 212° F.....	.4700	.03790
Hydrogen.....	.0692	.00559

* The specific gravity of steam at any temperature and pressure compared with air at the same temperature and pressure is 0.622.

MISCELLANEOUS.

Substance.	Specific Gravity.	Weight per Cubic Foot in Pounds.
Emery	4.00	250
Glass (average).....	2.80	175
Chalk.	2.78	174
Granite	2.65	166
Marble	2.70	169
Stone (common).....	2.52	158
Salt (common).....	2.13	133
Soil (common)	1.98	124
Clay.....	1.93	121
Brick.....	1.90	118
Plaster Paris (average).....	2.00	125
Sand	1.80	113

MISCELLANEOUS TABLES.

SPECIFIC HEATS UNDER CONSTANT PRESSURE.

SOLIDS.

Copper.... 0.0951	Cast Iron.....0.1298
Gold 0.0324	Lead.....0.0314
Wrought Iron.....0.1138	Platinum 0.0324
Steel (soft) 0.1165	Silver.....0.0570
Steel (hard).....0.1175	Tin. 0.0562
Zinc.....0.0956	Ice.....0.5040
Brass.....0.0939	Sulphur 0.2026
Glass.....0.1937	Charcoal.....0.2410

LIQUIDS.

Water.....	1.0000	Lead (melted).....	0.0402
Alcohol.....	0.7000	Sulphur (melted).....	0.2340
Mercury.....	0.0333	Tin (melted).....	0.0637
Benzine	0.4500	Sulphuric Acid.....	0.3350
Glycerine.....	0.5550	Oil of Turpentine.....	0.4260

GASES.

	Constant Pressure.	Constant Volume.
Air.....	0.23751	0.16847
Oxygen.....	0.21751	0.15507
Nitrogen	0.24380	0.17273
Hydrogen	3.40900	2.41226
Superheated Steam...	0.48050	0.34600
Carbonic Oxide.....	0.24790	0.17580
Carbonic Acid.....	0.40400	0.15350

VOLUMES AND WEIGHTS OF GASES.

Gas.	Volume of one Pound at 32°F. and a Tension of 1 Atmosphere (14.7 Lb. per Sq. In.). Cu. Ft.	Weight of one Cu. Ft. at 32° F. and a Tension of 1 Atmosphere (14.7 Lb. per Sq. In.). Lb.	R.
Air.....	12.388	.08073	.37052
Oxygen.....	11.2056	.08925	.33552
Nitrogen.....	12.7226	.0786	.38143
Hydrogen.....	178.891	.00559	5.34946

TEMPERATURES OF FUSION AND VAPORIZATION.

Substance.	Tem- perature of Fusion.	Tem- perature of Vaporiza- tion.	Latent Heat of Fusion.	Latent Heat of Vaporiza- tion.
Water	32°	212°	142.65	966.6
Mercury	— 37.8°	662°	5.09	157
Sulphur	228.3°	824°	13.26	
Tin	446°		25.65	
Lead	626°		9.67	
Zinc	680°	1900°	50.63	493
Alcohol	Unknown	173°		372
Oil of Turpentine	14°	313°		124
Linseed Oil		600°		
Aluminum	1400°			
Copper	2100°			
Cast Iron	2192°	3300°		
Wrought Iron...	2912°	5000°		
Steel	2520°			
Platinum	3632°			
Iridium	4892°			

COEFFICIENTS OF EXPANSION.

Name of Substance.	Linear Expansion.	Surface Expansion.	Cubic Expansion.
Cast Iron	.00000617	.00001234	.00001850
Copper	.00000955	.00001910	.00002864
Brass	.00001037	.00002074	.00003112
Silver	.00000690	.00001390	.00002070
Bar Iron	.00000686	.00001372	.00002058
Steel (untempered)...	.00000599	.00001198	.00001798
Steel (tempered)	.00000702	.00001404	.00002106
Zinc	.00001634	.00003268	.00004903
Tin	.00001410	.00002820	.00004229
Mercury	.00003334	.00006668	.00010010
Alcohol	.00019259	.00038518	.00057778
Gases			.00203252

UNITED STATES STANDARD SCREW THREADS.

Diameter of Screw in Inches. d	Number of Threads per Inch. n	Diameter at Bot- tom of Threads in Inches. d_1	Area at Bottom of Threads in Square Inches. a
$\frac{1}{4}$	20	.185	.0269
$\frac{5}{16}$	18	.240	.0452
$\frac{3}{8}$	16	.294	.0679
$\frac{7}{16}$	14	.345	.0935
$\frac{1}{2}$	13	.400	.1257
$\frac{9}{16}$	12	.454	.1619
$\frac{5}{8}$	11	.507	.2019
$\frac{3}{4}$	10	.620	.3019
$\frac{7}{8}$	9	.731	.4197
1	8	.838	.5515
$1\frac{1}{8}$	7	.939	.6925
$1\frac{1}{4}$	7	1.064	.8892
$1\frac{3}{8}$	6	1.158	1.0532
$1\frac{1}{2}$	6	1.283	1.2928
$1\frac{5}{8}$	$5\frac{1}{2}$	1.389	1.5153
$1\frac{3}{4}$	5	1.490	1.7437
$1\frac{7}{8}$	5	1.615	2.0485
2	$4\frac{1}{2}$	1.711	2.2993
$2\frac{1}{4}$	$4\frac{1}{2}$	1.961	3.0203
$2\frac{1}{2}$	4	2.175	3.7154
$2\frac{3}{4}$	4	2.425	4.6186
3	$3\frac{1}{2}$	2.629	5.4284
$3\frac{1}{4}$	$3\frac{1}{2}$	2.879	6.5099
$3\frac{1}{2}$	$3\frac{1}{4}$	3.100	7.5477
$3\frac{3}{4}$	3	3.317	8.6414
4	3	3.567	9.9930
$4\frac{1}{4}$	$2\frac{7}{8}$	3.798	11.3292
$4\frac{1}{2}$	$2\frac{3}{4}$	4.027	12.7366
$4\frac{3}{4}$	$2\frac{5}{8}$	4.255	14.2197
5	$2\frac{1}{2}$	4.480	15.7633
$5\frac{1}{4}$	$2\frac{1}{2}$	4.730	17.5717
$5\frac{1}{2}$	$2\frac{3}{8}$	4.953	19.2676
$5\frac{3}{4}$	$2\frac{3}{8}$	5.203	21.2617
6	$2\frac{1}{4}$	5.423	23.0978

**STANDARD DIMENSIONS OF WROUGHT-IRON
STEAM, GAS, AND WATER PIPES.**

Nominal Diameter in Inches.	Thickness in Inches.	Actual Internal Diameter in Inches.	Actual External Diameter in Inches.	Threads per Inch. "	Pitch of Threads.
$\frac{1}{8}$	.068	.270	.405	27	.037
$\frac{1}{4}$	.088	.364	.540	18	.056
$\frac{3}{8}$	.091	.494	.675	18	.056
$\frac{1}{2}$	.109	.623	.840	14	.071
$\frac{3}{4}$	.113	.824	1.050	14	.071
1	.134	1.048	1.315	11 $\frac{1}{2}$	.087
1 $\frac{1}{4}$	.140	1.380	1.660	11 $\frac{1}{2}$	.087
1 $\frac{1}{2}$	.145	1.611	1.900	11 $\frac{1}{2}$	.087
2	.154	2.067	2.375	11 $\frac{1}{2}$	.087
2 $\frac{1}{2}$	.204	2.468	2.875	8	.125
3	.217	3.061	3.500	8	.125
3 $\frac{1}{2}$	.226	3.548	4.000	8	.125
4	.237	4.026	4.500	8	.125
4 $\frac{1}{2}$	.247	4.508	5.000	8	.125
5	.259	5.045	5.563	8	.125
6	.280	6.065	6.625	8	.125
7	.301	7.023	7.625	8	.125
8	.322	7.982	8.625	8	.125
9	.344	9.001	9.688	8	.125
10	.366	10.019	10.750	8	.125

STANDARD PIPE FLANGES.

Inside Diam. of Pipe.	Thick- ness of Pipe.	Diam. of Bolts.	Length of Bolts.	No. of Bolts.	Thick- ness of Flange.	Diam. of Bolt Circle.	Diam. of Flange.
2.0	.409	$\frac{5}{8}$	2.0	4	$\frac{5}{8}$	4.75	6.0
2.5	.429	$\frac{5}{8}$	2.25	4	$1\frac{1}{8}$	5.25	7.0
3.0	.448	$\frac{5}{8}$	2.5	4	$\frac{3}{4}$	6.0	7.5
3.5	.466	$\frac{5}{8}$	2.5	4	$1\frac{3}{8}$	6.5	8.5
4.0	.486	$\frac{3}{4}$	2.75	4	$1\frac{5}{8}$	7.25	9.0
4.5	.498	$\frac{3}{4}$	3.0	8	$1\frac{5}{8}$	7.75	9.25
5	.525	$\frac{3}{4}$	3.0	8	$1\frac{5}{8}$	8.5	10.0
6	.563	$\frac{3}{4}$	3.0	8	1	9.625	11.0
7	.600	$\frac{3}{4}$	3.25	8	$1\frac{1}{8}$	10.75	12.5
8	.639	$\frac{3}{4}$	3.5	8	$1\frac{1}{8}$	11.75	13.5
9	.678	$\frac{3}{4}$	3.5	12	$1\frac{1}{8}$	13.0	15.0
10	.713	$\frac{7}{8}$	3.625	12	$1\frac{3}{8}$	14.25	16.0
12	.790	$\frac{7}{8}$	3.75	12	$1\frac{1}{4}$	16.5	19.0
14	.864	1	4.25	12	$1\frac{3}{8}$	18.75	21.0
15	.904	1	4.25	16	$1\frac{3}{8}$	20.0	22.25
16	.946	1	4.25	16	$1\frac{7}{8}$	21.25	23.5
18	1.020	$1\frac{1}{8}$	4.75	16	$1\frac{9}{8}$	22.75	25.0
20	1.090	$1\frac{1}{8}$	5.0	20	$1\frac{1}{8}$	25.0	27.5
22	1.180	$1\frac{1}{4}$	5.5	20	$1\frac{3}{8}$	27.25	29.5
24	1.250	$1\frac{1}{4}$	5.5	20	$1\frac{7}{8}$	29.5	32.0
26	1.300	$1\frac{1}{4}$	5.75	24	2	31.75	34.25
28	1.380	$1\frac{1}{4}$	6.0	28	$2\frac{1}{8}$	34.0	36.5
30	1.480	$1\frac{3}{8}$	6.25	28	$2\frac{1}{8}$	36.0	38.75
36	1.710	$1\frac{3}{8}$	6.5	32	$2\frac{3}{8}$	42.75	45.75
42	1.870	$1\frac{1}{2}$	7.25	36	$2\frac{3}{8}$	49.5	52.75
48	2.170	$1\frac{1}{2}$	7.75	44	$2\frac{3}{4}$	56.0	59.5

LAP-WELDED AMERICAN CHARCOAL IRON BOILER TUBES.

STANDARD DIMENSIONS.

External Diameter.	Standard Thickness.	Wire Gauge.	Internal Diameter.	Internal Circumference.	External Circumference.	Length of Tube per sq. ft. Inside Surface.	Length of Tube per sq. ft. Out. Surface.	Internal Area.	External Area.	Weight per foot.
In.	In.		In.	In.	In.	Ft.	Ft.	Sq. In.	Sq. In.	Lb.
1	.072	15	.856	2.689	3.142	4.463	3.819	.575	.735	.708
1½	.083	14	1.334	4.191	4.712	2.863	2.547	1.396	1.767	1.250
2	.098	13	1.804	5.667	6.283	2.118	1.909	2.556	3.142	1.981
2½	.109	12	2.283	7.172	7.854	1.673	1.528	4.094	4.909	2.755
3	.109	12	2.783	8.743	9.425	1.373	1.273	6.083	7.069	3.333
3½	.119	11	3.262	10.248	10.996	1.171	1.091	8.357	9.621	4.272
4	.130	10	3.741	11.753	12.566	1.021	.955	10.992	12.566	5.320
4½	.130	10	4.241	13.323	14.137	.901	.849	14.126	15.904	6.010
5	.140	9.5	4.720	14.828	15.708	.809	.764	17.497	19.635	7.276
6	.151	9	5.699	17.904	18.850	.670	.637	25.509	28.274	9.346

PROPORTIONS OF RIVETED JOINTS.

Thick- ness of Plate. <i>t</i>	Diam- eter of Rivet.	Diam- eter of Hole. <i>d</i>	Pitch.		Efficiency of Joint.	
			Single.	Double.	Single.	Double.
$\frac{1}{4}$ "	$\frac{5}{8}$ "	$\frac{11}{16}$ "	2"	3"	.66	.77
$\frac{1}{8}$ "	$\frac{11}{16}$ "	$\frac{3}{4}$ "	$2\frac{1}{8}$ "	$3\frac{1}{8}$ "	.64	.76
$\frac{3}{8}$ "	$\frac{3}{4}$ "	$\frac{13}{16}$ "	$2\frac{1}{8}$ "	$3\frac{1}{8}$ "	.62	.75
$\frac{1}{2}$ "	$\frac{13}{16}$ "	$\frac{7}{8}$ "	$2\frac{3}{16}$ "	$3\frac{3}{8}$ "	.60	.74
$\frac{3}{4}$ "	$\frac{7}{8}$ "	$\frac{15}{16}$ "	$2\frac{1}{4}$ "	$3\frac{1}{2}$ "	.58	.73

PROPORTIONS OF GEAR TEETH.

C = Circular Pitch.

	Rough Cast Gears.	Cut Gears.
Addendum.....	$0.30 C$	$0.30 C$
Root	$0.40 C$	$0.35 C$
Whole Depth.....	$0.70 C$	$0.65 C$
Thickness of Tooth.....	$0.48 C$	$0.495 C$
Width of Space.....	$0.52 C$	$0.505 C$

**RELATION BETWEEN DIAMETRAL AND
CIRCULAR PITCH.**

Diametral Pitch.	Circular Pitch.	Circular Pitch.	Diametral Pitch.
2	1.571 inches.	2 inches	1.571
2 $\frac{1}{2}$	1.396 "	1 $\frac{7}{8}$ "	1.676
3	1.257 "	1 $\frac{3}{4}$ "	1.795
3 $\frac{1}{2}$	1.142 "	1 $\frac{5}{8}$ "	1.933
4	1.047 "	1 $\frac{1}{2}$ "	2.094
5	.898 "	1 $\frac{1}{8}$ "	2.185
6	.785 "	1 $\frac{3}{8}$ "	2.285
7	.628 "	1 $\frac{5}{8}$ "	2.394
8	.524 "	1 $\frac{1}{4}$ "	2.513
9	.449 "	1 $\frac{3}{8}$ "	2.646
10	.393 "	1 $\frac{1}{8}$ "	2.793
11	.349 "	1 $\frac{1}{8}$ "	2.957
12	.314 "	1 "	3.142
14	.286 "	1 $\frac{5}{8}$ "	3.351
16	.262 "	1 $\frac{7}{8}$ "	3.590
18	.224 "	1 $\frac{3}{4}$ "	3.867
20	.196 "	1 $\frac{3}{4}$ "	4.189
	.175 "	1 $\frac{1}{4}$ "	4.570
	.157 "	1 $\frac{1}{8}$ "	5.027

BREAKING STRENGTH OF AND POWER TRANSMITTED BY WIRE ROPES (42 WIRES).

Diameter of Ropes, Inches.	Diameter of Pulleys, Feet.	Revolutions per Minute.	Breaking Stress of Rope per Pound.	Horse-power Transmitted.	Velocity of Rope in Feet per Second.
$\frac{7}{16}$	5	100	4,260	8.6	26
$\frac{15}{32}$	6	100	5,660	13.4	31
$\frac{1}{2}$	7	100	8,200	21.1	36
$\frac{5}{8}$	8	100	11,600	27.5	42
$\frac{5}{8}$	8	120	11,600	33.0	50
$\frac{5}{8}$	9	100	11,600	51.9	47
$\frac{5}{8}$	9	120	11,600	62.2	56
$\frac{11}{16}$	10	100	15,200	73.0	52
$\frac{11}{16}$	10	120	15,200	87.6	62
$\frac{11}{16}$	10	140	15,200	102.2	73
$\frac{11}{16}$	12	100	15,200	116.7	63
$\frac{3}{4}$	12	120	17,600	148.9	75
$\frac{3}{4}$	12	140	17,600	173.7	87
$\frac{3}{4}$	14	100	17,600	185.0	73
$\frac{3}{4}$	14	120	17,600	222.0	87
$\frac{3}{4}$	15	120	17,600	300.0	94

SAFE PRESSURE ON BEARINGS AND SLIDES

Kind of Journal Bearing.	Pressure per Sq. In. of Projected Area, <i>p</i> .
Bearings on which the load is intermittent and the speed slow, such as crank-pins of shearing machines	3,000 lb.
Cross-head neck journals	1,200 lb.
Crank-pins of large, slow-speed engines	800 to 900 lb.
Crank-pins of marine engines, usually	400 to 500 lb.
Main crank-shaft bearings—marine engines (slow)	600 lb.

Main crank-shaft bearings—marine engines (fast)	400 lb.
Locomotive driving-axle journal.....180 to	350 lb
Railway journals.....	200 lb.
Fly-wheel shaft journals.....150 to	250 lb.
Small engine crank-pins.....150 to	200 lb.
Slipper slide blocks, marine engines.....	100 lb.
Stationary engine slide blocks.....25 to	125 lb.
Stationary engine slide blocks, usually.....30 to	60 lb.
Propeller thrust bearings.....50 to	70 lb.
Shaft in cast-iron steps or seats.....	15 lb.

RULES AND FORMULAS.

FORMULAS USED IN ALGEBRA.

Let a and b be any two quantities, then,

$$(a + b)^2 = a^2 + 2ab + b^2. \quad (1.) \text{ Art. 432.}$$

$$(a - b)^2 = a^2 - 2ab + b^2. \quad (2.) \text{ Art. 432.}$$

$$(a + b)(a - b) = a^2 - b^2. \quad (3.) \text{ Art. 432.}$$

$$a^2 + 2ab + b^2 = (a + b)(a + b) = (a + b)^2. \quad (4.) \text{ Art. 455.}$$

$$a^2 - 2ab + b^2 = (a - b)(a - b) = (a - b)^2. \quad (5.) \text{ Art. 455.}$$

$$a^2 - b^2 = (a + b)(a - b). \quad (6.) \text{ Art. 462.}$$

Let $ax^2 + bx = c$ be any quadratic equation (it must be borne in mind that b and c may be positive or negative); then,

$$x = -\frac{b}{2a} \pm \sqrt{\left(\frac{b}{2a}\right)^2 + \frac{c}{a}} = \frac{-b \pm \sqrt{b^2 + 4ac}}{2a}. \quad \text{Art. 597}$$

THE TRIGONOMETRIC FUNCTIONS.

Art. 754.

Rule 1.—*Sine* = $\frac{\text{side opposite}}{\text{hypotenuse}}$.

Rule 2.—*Side opposite* = *hypotenuse* $\times$ *sine*.

Rule 3.—*Cosine* = $\frac{\text{side adjacent}}{\text{hypotenuse}}$.

Rule 4.—*Side adjacent* = *hypotenuse* $\times$ *cosine*.

Rule 5.— $\text{Tangent} = \frac{\text{side opposite}}{\text{side adjacent}}$.

Rule 6.— $\text{Side opposite} = \text{side adjacent} \times \text{tangent}$.

Rule 7.— $\text{Cotangent} = \frac{\text{side adjacent}}{\text{side opposite}}$.

Rule 8.— $\text{Side adjacent} = \text{side opposite} \times \text{cotangent}$.

Rule 9.— $\text{Hypotenuse} = \frac{\text{side opposite}}{\text{sine}}$.

Rule 10.— $\text{Hypotenuse} = \frac{\text{side adjacent}}{\text{cosine}}$.

RULES FOR USING TABLE OF LOGARITHMS OF NUMBERS.

Arts. 625–636.

I. To find the Characteristic.—For a number greater than 1 the characteristic is one less than the number of integral places in the number. For a number wholly decimal the characteristic is negative, and is numerically one greater than the number of ciphers between the decimal point and the first digit of the decimal.

II. To find the Logarithm of a Number not having more than four figures.—Find the first three significant figures of the number whose logarithm is desired in the left-hand column; find the fourth figure in the column at the top (or bottom) of the page, and in the column under (or above) this figure, and opposite the first three figures previously found, will be the mantissa, or decimal part, of the logarithm. The characteristic being found as described above, write it at the left of the mantissa, and the resulting expression will be the logarithm of the required number.

III. To find the Logarithm of a Number consisting of five or more figures.

(a) If the number consists of more than five figures, and the sixth figure is 5 or greater, increase the fifth figure by 1, and write ciphers in place of the sixth and remaining figures.

(b) Find the mantissa corresponding to the logarithm of the first four figures, and subtract this mantissa from the next greater mantissa in the table; the remainder is the difference.

(c) Find in the secondary table headed *P. P.* a column headed by the same number as that just found for the difference, and in this column opposite the number corresponding to the fifth figure (or fifth figure increased by 1) of the given number (this figure is always situated at the left of the dividing line of the column) will be found the *P. P.* (proportional part) for that number. The *P. P.* thus found is to be added to the mantissa found in (b), and the result is the mantissa of the logarithm of the given number, as nearly as may be found with five-place tables.

IV. To find a Number whose Logarithm is given.—

(a) Consider the mantissa first. Glance along the different columns of the table which are headed *O* until the first two figures of the mantissa are found. Then glance down the same column until the third figure is found (or 1 less than the third figure). Having found the first three figures, glance to the right along the row in which they are situated until the last three figures of the mantissa are found. Then the number which heads the column in which the last three figures of the mantissa are found is the fourth figure of the required number, and the first three figures lie in the column headed *N*, and in the same row in which lie the last three figures of the mantissa.

(b) If the mantissa cannot be found in the table, find the mantissa which is nearest to, but less than, the given mantissa, and which call the **next less mantissa**. Subtract the next less mantissa from the next greater mantissa in the table to obtain the difference. Also subtract the next less mantissa from the mantissa of the given logarithm, and call the remainder the *P. P.* Looking in the secondary table headed *P. P.* for the column headed by the difference just found, find the number opposite the *P. P.* just found (or the *P. P.* corresponding most

nearly to that just found) ; this number is the fifth figure of the required number ; the fourth figure will be found at the top of the column containing the next less mantissa, and the first three figures in the column headed *N*, and in the same row which contains the next less mantissa.

(c) Having found the figures of the number as above directed, locate the decimal point by the rules for the characteristic, annexing ciphers to bring the number up to the required number of figures if the characteristic is greater than 4.

RULES FOR USING TRIGONOMETRIC TABLES.

Given, an angle, to find its sine, cosine, tangent, and cotangent.

Rule 11.—Find in the table the sine, cosine, tangent, or cotangent corresponding to the degrees and minutes of the angle.

For the seconds, find the difference of the values of the sine, cosine, tangent, or cotangent taken from the table, between which the seconds of the angle fall ; multiply this difference by a fraction whose numerator is the number of seconds in the given angle, and whose denominator is 60.

If sine or tangent, add this correction to the value first found; if cosine or cotangent, subtract the correction. **Art. 756.**

Given, the sine, cosine, tangent, or cotangent to find the angle corresponding.

To find the angle corresponding to a given sine, cosine, tangent, or cotangent whose exact value is not contained in the table:

Rule 12.—Find the difference of the two numbers in the table between which the given sine, cosine, tangent, or cotangent falls, and use the number of parts in this difference as the denominator of a fraction.

Find the difference between the number belonging to the **smaller angle**, and the given sine, cosine, tangent, or cotangent, and use the number of parts in the difference just found as the numerator of the fraction mentioned above. Multiply this fraction by 60, and the result will be the number of seconds to be added to the **smaller angle**. **Art. 758.**

RULES FOR MENSURATION.

THE TRIANGLE.

Rule.—*The area of any triangle equals one-half the product of the base and the altitude.* Art. 766.

THE QUADRILATERAL.

To find the area of a parallelogram:

Rule.—*The area of any parallelogram equals the product of the base and the altitude.* Art. 777.

To find the area of a trapezoid:

Rule.—*The area of a trapezoid equals one-half the sum of the parallel sides multiplied by the altitude.* Art. 778.

To find the area of an irregular figure bounded by straight lines:

Rule.—*Divide the figure into triangles, and find the area of each triangle separately. The sum of the areas of all the triangles will be the area of the figure.* Art. 779.

THE CIRCLE.

To find the circumference or diameter of a circle:

Rule.—*The circumference of a circle equals the diameter multiplied by 3.1416.* Art. 780.

Rule.—*The diameter of a circle equals the circumference divided by 3.1416.* Art. 780.

To find the length of an arc of a circle:

Rule.—*The length of an arc of a circle equals the circumference of the circle of which the arc is a part multiplied by the number of degrees in the arc, and divided by 360.* Art. 781.

To find the area of a circle:

Rule.—*Square the diameter, and multiply by .7854.* Art. 782.

Given, the area of a circle to find its diameter:

Rule.—*Divide the area by .7854, and extract the square root of the quotient.* Art. 783.

To find the area of a sector:

Rule.—*Divide the number of degrees in the arc of a sector by 360. Multiply the result by the area of the circle of which the sector is a part.* Art. 784.

To find the area of a segment of a circle:

Rule.—*Draw radii from the center of the circle to the extremities of the arc of the segment; find the area of the sector thus formed, subtract from this the area of the triangle formed by the radii and the chord of the arc of the segment, and the result is the area of the segment.* Art. 785.

THE ELLIPSE.

To find the perimeter of an ellipse:

Rule.—*Multiply the major axis by 1.82, and the minor axis by 1.315. The sum of the results will be the perimeter.* Art. 788.

To find the exact area of an ellipse:

Rule.—*The area of an ellipse is equal to the product of its two diameters multiplied by .7854.* Art. 789.

To find the area of any plane figure:

Rule.—*The area of any plane figure may be found by dividing it into triangles, quadrilaterals, circles or parts of circles, and ellipses, finding the area of each part separately, and adding them together.* Art. 790.

THE PRISM AND CYLINDER.

To find the area of the convex surface of any right prism or right cylinder:

Rule.—*Multiply the perimeter of the base by the altitude.* Art. 803.

To find the volume of a right prism or cylinder:

Rule.—*The volume of any right prism or cylinder equals the area of the base multiplied by the altitude.* Art. 804.

THE PYRAMID AND CONE.

To find the area of a right pyramid or right cone:

Rule.—*The convex area of a right pyramid or cone equals the perimeter of the base multiplied by one-half the slant height.* Art. 809.

To find the volume of a right pyramid or cone:

Rule.—*The volume of a right pyramid or cone equals the area of the base multiplied by one-third of the altitude.* Art. 810.

THE FRUSTUM OF A PYRAMID OR CONE.

To find the convex area of a frustum of a right pyramid or right cone:

Rule.—*The convex area of a frustum of a right pyramid or right cone equals one-half the sum of the perimeters of its bases multiplied by the slant height of the frustum.* Art. 814.

To find the volume of the frustum of a pyramid or cone:

Rule.—*Add the areas of the upper base, the lower base, and the square root of the product of the areas of the two bases; multiply this sum by one-third of the altitude.* Art. 815.

THE SPHERE.

To find the area of the surface of a sphere:

Rule.—*The area of the surface of a sphere equals the square of the diameter multiplied by 3.1416.* Art. 817.

To find the volume of a sphere:

Rule.—*The volume of a sphere equals the cube of the diameter multiplied by .5236.* Art. 818.

FORMULAS USED IN ELEMENTARY MECHANICS.**UNIFORM MOTION.**

Let S = the length of space passed over uniformly;

t = the time occupied in passing over the space S ;

V = the velocity.

$$V = \frac{S}{t}. \quad (7.) \text{ Art. 859.}$$

$$S = Vt. \quad (8.) \text{ Art. 859.}$$

$$t = \frac{S}{V}. \quad (9.) \text{ Art. 859.}$$

MASS, WEIGHT, AND GRAVITY.

If the mass of the body be represented by m , its weight by W , and the force of gravity at the place where the body was weighed by g , we have

$$\text{mass} = \frac{\text{weight of body}}{\text{force of gravity}}, \text{ or } m = \frac{W}{g}. \quad (10.) \text{ Art. 888.}$$

FORMULAS FOR GRAVITY PROBLEMS.

Let W = weight of body at the surface;

w = weight of a body at a given distance above or below the surface;

d = distance between the center of the earth and the center of the body;

R = radius of the earth = 4,000 miles.

Formula for weight when the body is below the surface:

$$w R = d W. \quad (11.) \text{ Art. 891.}$$

Formula for weight when the body is above the surface:

$$w d^2 = W R^2. \quad (12.) \text{ Art. 891.}$$

FALLING BODIES.

Let g = force of gravity = constant accelerating force due to the attraction of the earth;

t = number of seconds the body falls;

v = velocity at the end of the time t ;

h = distance that a body falls during the time t .

$$v = g t. \quad (13.) \text{ Art. 896.}$$

That is, the velocity acquired by a freely falling body at the end of t seconds equals 32.16 multiplied by the time in seconds.

$$t = \frac{v}{g}. \quad (14.) \text{ Art. 896.}$$

That is, the number of seconds during which a body must have fallen to acquire a given velocity equals the given velocity in feet per second divided by 32.16.

$$h = \frac{v^2}{2g}. \quad (15.) \text{ Art. 896.}$$

That is, the height from which a body must fall to acquire a given velocity equals the square of the given velocity divided by 2×32.16 .

$$v = \sqrt{2gh}. \quad (16.) \text{ Art. 896.}$$

That is, the velocity that a body will acquire in falling through a given height equals the square root of the product of twice 32.16 and the given height.

$$h = \frac{1}{2} g t^2. \quad (17.) \text{ Art. 896.}$$

That is, the distance a body will fall in a given time equals $32.16 \div 2$ multiplied by the square of the number of seconds.

$$t = \sqrt{\frac{2h}{g}}. \quad (18.) \text{ Art. 896.}$$

That is, the time it will take a body to fall through a given height equals the square root of twice the height divided by 32.16.

CENTRIFUGAL FORCE.

The value of the centrifugal force of any revolving body, expressed in pounds, is

$$F = .00034 W R N^2; \quad (19.) \text{ Art. 903.}$$

in which F = centrifugal force;

W = total weight of body in pounds;

R = radius, usually taken as the distance between the center of motion and the center of gravity of the revolving body, in feet;

N = number of revolutions per *minute*.

THE CENTER OF GRAVITY OF TWO BODIES.

Let l = the distance between the centers of the bodies;

l_1 = the short arm;

w = weight of small body;

W = weight of large body.

$$l_1 = \frac{wl}{W+w}. \quad (20.) \quad \text{Art. 911.}$$

THE EFFICIENCY OF A MACHINE.

Let F = the force applied to the machine;

V = the velocity ratio of the machine;

W = the weight actually lifted or equivalent resistance overcome;

E = the efficiency of the machine;

$$\text{Then, } E = \frac{W}{FV}. \quad (22.) \quad \text{Art. 950.}$$

WORK.

If the force necessary to overcome the resistance be represented by F , the space through which the resistance acts by S , and the work done by U , then $U = FS$.

If W = the weight of a body, and h = the height through which it is raised, $U = Wh$. Hence the work done

$$U = FS = Wh. \quad (23.) \quad \text{Art. 953.}$$

POWER.

The power of a machine may always be determined by *dividing the work done in foot-pounds by the time in minutes required to do the work; i. e.,*

$$\text{Power} = \frac{FS}{T}. \quad (24.) \quad \text{Art. 954.}$$

KINETIC ENERGY.

Let W = the weight of the body in pounds;

v = its velocity in feet per second;

h = the height in feet through which the body must fall to produce the velocity v ;

m = the mass of the body = $\frac{W}{g}$. (See formula 10.)

The work necessary to raise a body through a height h is Wh . The velocity produced in falling a height h is $v = \sqrt{2gh}$, and $h = \frac{v^2}{2g}$. (See formulas 15 and 16.)

Therefore, work $= Wh = W \frac{v^2}{2g} = \frac{1}{2} \times \frac{W}{g} \times v^2 = \frac{1}{2} m v^2$, or
 $Wh = \frac{1}{2} m v^2$. (25.) Art. 957.

DENSITY.

The density of a body is its mass divided by its volume in cubic feet.

Let D be the density; then the density of a body is

$$D = \frac{m}{V}. \text{ Since } m = \frac{W}{g}, D = \frac{W}{gV}. \quad (26.) \text{ Art. 962.}$$

RULES AND FORMULAS USED IN HYDRO-MECHANICS.

PASCAL'S LAW.

Rule I.—*The pressure per unit of area exerted anywhere upon a mass of liquid is transmitted undiminished in all directions, and acts with the same force upon all surfaces in a direction at right angles to those surfaces.*

THE GENERAL LAW FOR THE DOWNWARD PRESSURE UPON THE BOTTOM OF ANY VESSEL.

Rule II.—*The pressure upon the bottom of a vessel containing a fluid is independent of the shape of the vessel, and is equal to the weight of a prism of the fluid whose base has the same area as the bottom of the vessel, and whose altitude is the distance between the bottom and the upper surface of the fluid plus the pressure per unit of area upon the upper surface of the fluid multiplied by the area of the bottom of the vessel.*

GENERAL LAW FOR UPWARD PRESSURE.

Rule III.—*The upward pressure on any submerged horizontal surface equals the weight of a prism of the liquid*

whose base has an area equal to the area of the submerged surface, and whose altitude is the distance between the submerged surface and the upper surface of the liquid plus the pressure per unit of area on the upper surface of the fluid multiplied by the area of the submerged surface.

GENERAL LAW FOR LATERAL PRESSURE.

Rule IV.—*The pressure upon any vertical surface due to the weight of a liquid is equal to the weight of a prism of the liquid whose base has the same area as the vertical surface, and whose altitude is the depth of the center of gravity of the vertical surface below the level of the liquid.*

Any additional pressure is to be added as in the previous cases.

GENERAL LAW FOR PRESSURE.

Rule V.—*The pressure exerted by a fluid in any direction upon any surface is equal to the weight of a prism of the fluid whose base is the projection of the surface at right angles to the direction considered, and whose height is the depth of the center of gravity of the surface below the level of the liquid.*

SPECIFIC GRAVITY.

Let W be the weight of the solid in air and W' the weight in water; then, $W - W' =$ the weight of a volume of water equal to the volume of the solid, and

$$\text{Sp. Gr.} = \frac{W}{W - W'} \quad (27.) \quad \text{Art. 991.}$$

If the body be lighter than water, a piece of iron or other heavy substance must be attached to it sufficiently heavy to sink both. *Then weigh both bodies in air and both in water.*

Let W = weight of both bodies in air;
 W' = weight of both bodies in water;
 w = weight of light body in air;
 W_1 = weight of heavy body in air;
 W_2 = weight of heavy body in water.

Then, the specific gravity of the light body is given by

$$\text{Sp. Gr.} = \frac{w}{(W - W') - (W_1 - W_2)}. \quad (28.) \quad \text{Art. 992.}$$

To find the specific gravity of a liquid:

Weigh an empty flask; fill it with water, then weigh it, and find the difference between the two results; this will equal the weight of the water. Then weigh the flask filled with the liquid and subtract the weight of the flask; the result is the weight of a volume of the liquid equal to the volume of the water. The weight of the liquid divided by the weight of the water is the specific gravity of the liquid.

Let W = the weight of the flask and liquid;
 W' = the weight of the flask and water;
 w = the weight of the flask.

$$\text{Then,} \quad \text{Sp. Gr.} = \frac{W - w}{W' - w}. \quad (29.) \quad \text{Art. 993.}$$

FORMULAS FOR FLOW OF WATER.

MEAN VELOCITY.

Let Q = the quantity in cubic feet which passes any section in 1 second;

A = the area of the section in square feet;

v_m = the mean velocity in feet per second.

$$\text{Then,} \quad Q = A v_m, \quad (31.) \quad \text{Art. 1003.}$$

$$\text{and} \quad v_m = \frac{Q}{A}. \quad (32.) \quad \text{Art. 1003.}$$

VELOCITY OF EFFLUX FROM AN ORIFICE.

Let v = the velocity of efflux in feet per second;

h = the head in feet on the orifice considered;

h_1 = the head equivalent to a pressure p ;

W = the weight of the water in pounds flowing through the aperture per second.

$$\text{The kinetic energy of the issuing water} = \frac{Wv^2}{2g}.$$

The work the issuing water can do = Wh .

$$Wh = \frac{Wv^2}{2g}, \text{ or } v = \sqrt{2gh}.$$

$$h = \frac{p}{.434}, \text{ where } h_1 \text{ is in feet, and } p \text{ in pounds per square inch.}$$

$$h_1 = \frac{p}{62.5}, \text{ where } h_1 \text{ is in feet, and } p \text{ in pounds per square foot.}$$

$h + h_1$ = the *total head*.

$$v = \sqrt{2g(h_1 + h)}. \quad (33.) \text{ Art. 1007.}$$

If a is the area of a large orifice in the bottom of a small vessel whose area is A , the velocity is

$$v \sqrt{\frac{2gh}{1 - \frac{a^2}{A^2}}}. \quad (35.) \text{ Art. 1010.}$$

Actual velocity of efflux from a small square-edged orifice:

$$v = .98 \sqrt{2gh}. \quad (36.) \text{ Art. 1013.}$$

Actual quantity discharged from a small square-edged orifice:

$$Q = .615 A v. \quad (37.) \text{ Art. 1015.}$$

THEORETICAL AND ACTUAL DISCHARGE.

Let Q = theoretical number of cubic feet discharged per second;

v_m = theoretical mean velocity through orifice in feet per second = $Q \div A$;

A = area of orifice in square feet;

h = theoretical head necessary to give a mean velocity v_m .

Q_a = actual quantity discharged in cubic feet per second.

Then, for an orifice in a thin plate, or a square-edged orifice (the hole itself may be of any shape, triangular,

square, circular, etc., but the edges must not be rounded), the actual quantity discharged is:

$$Q_a = .615 Q = .615 A v_m = .615 A \sqrt{2gh}. \quad (38.)$$

Art. 1017.

For a discharge through a short tube,

$$Q_a = .815 Q = .815 A v_m = .815 A \sqrt{2gh}. \quad (39.) \text{ Art. 1017.}$$

For a discharge through a mouthpiece,

$$Q_a = .97 Q = .97 A v_m = .97 A \sqrt{2gh}. \quad (40.) \text{ Art. 1017.}$$

For a discharge through the compound mouthpiece, the area of the orifice being taken as the area of the smallest section,

$$Q_a = 1.5526 Q = 1.5526 A v_m = 1.5526 A \sqrt{2gh}. \quad (41.)$$

Art. 1017.

In these four formulas it is taken for granted that there is a constant head.

FLOW OF WATER THROUGH WEIRS.

If d = the depth of the opening in feet, and b its breadth in feet, the area of the opening is $A = d \times b$, and the theoretical discharge is $Q = d \times b \times v_m = db \times \frac{2}{3} \sqrt{2gh} = \frac{2}{3} bd \sqrt{2gd}$, the head for this case being taken as d .

The actual discharge is

$$Q_a = .615 Q = .615 \times \frac{2}{3} bd \sqrt{2gd} = .41 b \sqrt{2gd^3}. \quad (42.)$$

Art. 1020.

That is, *the actual discharge through a weir in cubic feet per second, whose top is on a level with the upper surface of the water, is equal to .41 multiplied by the breadth of the weir, multiplied by the square root of 2 g times the cube of the depth of the weir. All dimensions are to be taken in feet.*

To obtain the mean velocity v_m , divide the actual discharge by the area of the weir, or

$$v_m = \frac{Q_a}{A} = \frac{Q_a}{bd}. \quad (43.) \text{ Art. 1020.}$$

For a weir whose upper edge is below the level of the upper surface of the water, let h_1 be the depth in feet of the top of the weir below the surface of the water, and h the depth in feet of the bottom of the weir below the surface of the water. The actual discharge Q_a in cubic feet per second is

$$Q_a = .41 b \sqrt{2g} (\sqrt{h^3} - \sqrt{h_1^3}). \quad (44.) \text{ Art. 1022.}$$

FLOW OF WATER IN PIPES.

THE MEAN VELOCITY OF DISCHARGE.

For straight cylindrical pipes of uniform diameter:

Let v_m = mean velocity of discharge in feet per second;
 h = total head in feet = the vertical distance between the level of the water in the reservoir and the point of discharge;
 l = length of pipe in feet;
 d = diameter of pipe in inches;
 f = coefficient of friction.

$$\text{Then, } v_m = 2.315 \sqrt{\frac{hd}{fl + \frac{1}{8}d}}. \quad (45.) \text{ Art. 1024.}$$

When the pipe is very long, compared with the diameter, the following formula may be used:

$$v_m = 2.315 \sqrt{\frac{hd}{fl}}. \quad (46.) \text{ Art. 1027.}$$

THE ACTUAL HEAD.

The actual head necessary to produce a certain velocity v_m may be calculated by the formula

$$h = \frac{flv_m^2}{5.36d} + .0233 v_m^2. \quad (47.) \text{ Art. 1029.}$$

THE QUANTITY DISCHARGED FROM PIPES.

Let d = the diameter of the pipe in inches, then the discharge Q in gallons per second is

$$Q = .0408 d^2 v_m. \quad (48.) \text{ Art. 1030.}$$

If the diameter of the pipe and the discharge are known, the mean velocity v_m is

$$v_m = \frac{24.51 Q}{d^2}. \quad (49.) \text{ Art. 1031.}$$

If the head, the length of the pipe, and the diameter of the pipe are given, to find the discharge use the formula

$$Q = .09445 d^2 \sqrt{\frac{h d}{f l + \frac{1}{8} d}}. \quad (50.) \text{ Art. 1032.}$$

To find the value of f , calculate v_m by formula 46, assuming that $f = .025$, and get the final value of f from the following table. Art. 1033.

$v_m =$	0.1	0.2	0.3	0.4	0.5	0.6
$f =$	.0686	.0527	.0457	.0415	.0387	.0365

$v_m =$	0.7	0.8	0.9	1	1½	1½
$f =$	.0349	.0336	.0325	.0315	.0297	.0284

$v_m =$	2	3	4	6	8	12
$f =$	.0265	.0243	.0230	.0214	.0205	.0193

NOTE.—The values given in the above table are calculated by the formula $f = .014892 + \frac{.017156}{\sqrt{v_m}}$.

TO CALCULATE THE DIAMETER OF A PIPE.

Neglecting the fraction $\frac{1}{8} d$ in formula 50, and solving for d ,

$$d = 2.57 \sqrt[5]{\frac{f l Q^2}{h}}.$$

Assuming that $f = .025$, for a trial value, the above equation then becomes

$$d = 1.229 \sqrt[5]{\frac{l Q^2}{h}}. \quad (51.) \text{ Art. 1035.}$$

Formula 50 may also be written

$$d = 2.57 \sqrt[5]{\frac{(fl + \frac{1}{8}d) Q^2}{h}}. \quad (52.) \text{ Art. 1035.}$$

By aid of formulas 51 and 52, the diameter of a pipe may be approximated as follows:

Rule.—Find the value of d by formula 51; substitute this value in formula 49, and find the value of v_m . Then find from the table the value of f corresponding to this value of v_m . Substitute the values of d and f just found in the right-hand member of formula 52, and solve for d ; the result will be the diameter of the pipe, nearly enough for all practical purposes.

FORMULAS USED IN PNEUMATICS.

PRESSURE, VOLUME, DENSITY, AND WEIGHT OF AIR WHEN THE TEMPERATURE IS CONSTANT:

Mariotte's Law.—The temperature remaining the same, the volume of a given quantity of gas varies inversely as the pressure.

Let p = pressure for one position of the piston;
 p_1 = pressure for any other position of the piston;
 v = volume corresponding to the pressure p ;
 v_1 = volume corresponding to the pressure p_1 .

Then, $p v = p_1 v_1$. (53.) Art. 1049.

Let D be the density corresponding to the pressure p and volume v , and D_1 be the density corresponding to the pressure p_1 and volume v_1 ; then,

$$p : D = p_1 : D_1, \text{ or } p D_1 = p_1 D, \quad (54.) \text{ Art. 1052.}$$

$$\text{and } v : D_1 = v_1 : D, \text{ or } v D = v_1 D_1. \quad (55.) \text{ Art. 1052.}$$

Thus, let W be the weight of a cubic foot of air or other gas, whose volume is v , and pressure is p ; let W_1 be the weight of a cubic foot when the volume is v_1 , and pressure is p_1 ; then,

$$p W_1 = p_1 W. \quad (56.) \text{ Art. 1052.}$$

$$v W = v_1 W_1. \quad (57.) \text{ Art. 1052.}$$

PRESSURE AND VOLUME OF A GAS WITH VARIABLE TEMPERATURE:

Gay-Lussac's Law.—*If the pressure remains constant, every increase of temperature of 1° F. produces in a given quantity of gas an expansion of $\frac{1}{460}$ of its volume at 32° F.*

If the pressure remains constant it will also be found that every decrease of temperature of 1° F. will cause a decrease of $\frac{1}{460}$ of the volume at 32° F.

Let v = original volume of gas;
 v_1 = final volume of gas;
 t = temperature corresponding to volume v ;
 t_1 = temperature corresponding to volume v_1 .

Then,
$$v_1 = v \left(\frac{460 + t_1}{460 + t} \right). \quad (58.) \text{ Art. 1054.}$$

That is, *the volume of gas after heating (or cooling) equals the original volume multiplied by 460 plus the final temperature divided by 460 plus the original temperature.*

Let p = the original tension;
 t = the corresponding temperature;
 p_1 = final tension;
 t_1 = final temperature.

Then,
$$p_1 = p \left(\frac{460 + t_1}{460 + t} \right). \quad (59.) \text{ Art. 1055.}$$

Let p = pressure in pounds per square inch;
 V = volume of air in cubic feet;
 T = absolute temperature;
 W = weight in pounds.

Then,
$$p V = .37052 T. \quad (60.) \text{ Art. 1056.}$$

If the weight of the air be greater or less than 1 pound, the following formula must be used:

$$p V = .37052 W T. \quad (61.) \text{ Art. 1057.}$$

Let p , V , and T represent the pressure, volume, and temperature of the same weight of air in another state; then,

$$\frac{p V}{T} = \frac{p_1 V_1}{T_1}. \quad (62.) \text{ Art. 1058.}$$

MIXTURE OF TWO GASES HAVING UNEQUAL VOLUMES AND PRESSURES.

Let v and p be the volume and pressure, respectively, of one of the gases.

Let v_1 and p_1 be the volume and pressure, respectively, of the other gas.

Let V and P be the volume and pressure, respectively, of the mixture. Then, if the temperature remains the same,

$$VP = v p + v_1 p_1. \quad (63.) \quad \text{Art. 1062.}$$

MIXTURE OF TWO VOLUMES OF AIR HAVING UNEQUAL PRESSURES, VOLUMES, AND TEMPERATURES.

If a body of air having a temperature t_1 , a pressure p_1 , and a volume v_1 , be mixed with another volume of air having a temperature t_2 , a pressure p_2 , and a volume v_2 , to form a volume V having a pressure P , and a temperature t , then, either the new temperature t , the new volume V , or the new pressure P may be found, if the other two quantities are known, by the following formula, in which T_1 , T_2 , and T are the absolute temperatures corresponding to t_1 , t_2 , and t :

$$PV = \left[\frac{p_1 v_1}{T_1} + \frac{p_2 v_2}{T_2} \right] T. \quad (64.) \quad \text{Art. 1063.}$$

FORMULAS USED IN HEAT.**TO CHANGE FAHRENHEIT TEMPERATURES TO CENTIGRADE, AND CENTIGRADE TO FAHRENHEIT.**

Let t_c = temperature Centigrade, and t_f = temperature Fahrenheit. Then,

$$t_f = \frac{9}{5} t_c + 32^\circ, \quad (65.) \quad \text{Art. 1104.}$$

$$\text{and } t_c = (t_f - 32^\circ) \frac{5}{9}. \quad (66.) \quad \text{Art. 1104.}$$

EXPANSION OR CONTRACTION OF BODIES FROM CHANGES OF TEMPERATURE.

Let L = length of any body;

l = amount of expansion or contraction due to heating or cooling the body;

A = area of any section of the body;

a = increase or decrease of area of the same section after heating or cooling the body;

V = volume of the body;

$\dot{v}$ = increase or decrease in volume due to heating or cooling the body;

C_1 = coefficient of expansion taken from column 1, Table 1;

C_2 = coefficient taken from column 2, Table 1;

C_3 = coefficient taken from column 3, Table 1;

t = difference in degrees of temperature between the original temperature and the temperature of the body after it has been heated or cooled.

Then, $l = L C_1 t$; (67.) Art. 1113.

$a = A C_2 t$; (68.) Art. 1113.

$v = V C_3 t$. (69.) Art. 1113.

RESULTING TEMPERATURES AND SPECIFIC HEATS OF THE MIXTURE OF SEVERAL BODIES HAVING UNEQUAL TEMPERATURES.

$$t = \frac{W_1 s_1 t_1 + W_2 s_2 t_2 + W_3 s_3 t_3 + \text{etc.}}{W_1 s_1 + W_2 s_2 + W_3 s_3 + \text{etc.}}, \quad \left\{ \begin{array}{l} (73.) \\ \text{Art. 1136.} \end{array} \right.$$

$$\text{or } s_4 = \frac{W_1 s_1 (t_1 - t) + W_2 s_2 (t_2 - t) + \text{etc.}}{W_4 (t - t_4)}, \quad \left\{ \begin{array}{l} (74.) \\ \text{Art. 1137.} \end{array} \right.$$

in which t is the final temperature of the mixture; W_1, s_1 , and t_1 , the weight, specific heat, and temperature, respectively, of one body; W_2, s_2 , and t_2 , the same for second body; and W_3, s_3 , and t_3 , the same for a third body, etc.

WORK DONE BY THE ISOTHERMAL EXPANSION OF A GAS.

L = the work in foot-pounds;

P = the total initial pressure in pounds per square foot;

P_1 = the total final pressure in pounds per square foot;

V = the initial volume in cubic feet;

V_1 = the final volume in cubic feet.

$$L = 2.3026 P V \log \frac{V_1}{V}. \quad (75.) \quad \text{Art. 1160.}$$

C. Vol. V.—6.

Since $PV = P_1 V_1$, $\frac{P}{P_1} = \frac{V_1}{V}$, and formula 75 might be written

$$L = 2.3026 PV \log \frac{P}{P_1}. \quad (76.) \quad \text{Art. 1160.}$$

Whichever formula is used it must be kept in mind that the fraction $\frac{V_1}{V}$ or $\frac{P}{P_1}$ must *always be greater than 1; that is, the numerator must always be greater than the denominator.*

WORK REQUIRED TO COMPRESS A GAS ISOTHERMALLY.

$$L = 2.3026 PV \log \frac{V}{V_1}, \quad (77.) \quad \text{and}$$

$$L = 2.3026 PV \log \frac{P_1}{P}, \quad (78.) \quad \text{Art. 1162.}$$

in which the letters have the same meaning as before, and *the larger volume or pressure is always in the numerator.*

Formulas 75, 76, 77, and 78 will be easier to use if the pressure be taken in pounds per square inch, and $144 \times 2.3026 = 331.5744$ be substituted for 2.3026. As before, the volume must always be taken in cubic feet. Formulas 75 and 76 then become

$$L = 331.5744 p V \log \frac{V}{V_1}, \quad (79.)$$

$$L = 331.5744 p V \log \frac{p}{p_1}, \quad (80.) \quad \text{Art. 1163.}$$

in which p = pressure in pounds per square inch.

RELATION BETWEEN PRESSURES AND VOLUMES OF AIR DURING ADIABATIC EXPANSION OR COMPRESSION.

Let p and v = the volume and pressure during one stage;

p_1 and v_1 = the volume and pressure during the next stage;

p_2 and v_2 = the volume and pressure during the third stage, etc.;

then $p v^{1.41} = p_1 v_1^{1.41} = p_2 v_2^{1.41} = \text{etc.} \quad (81.) \quad \text{Art. 1164.}$

WORK DONE BY THE ADIABATIC EXPANSION OF AIR.

Let L = work in foot-pounds;

P = initial pressure in pounds per square foot;

P_1 = final pressure in pounds per square foot;

V = initial volume in cubic feet;

V_1 = final volume in cubic feet.

$$L = 2.44 PV \left[1 - \left(\frac{V}{V_1} \right)^{.41} \right], \quad (82.) \text{ Art. 1165.}$$

$$L = 2.44 PV \left[1 - \left(\frac{P_1}{P} \right)^{.29078} \right]. \quad (83.) \text{ Art. 1166.}$$

Let p and p_1 be the initial and final pressures, respectively, in pounds per square inch, then,

$$L = 351.36 p V \left[1 - \left(\frac{V}{V_1} \right)^{.41} \right], \quad (84.)$$

$$L = 351.36 p V \left[1 - \left(\frac{p_1}{p} \right)^{.29078} \right]. \quad (85.) \text{ Art. 1167.}$$

The relation between the pressures and temperatures, and the volumes and temperatures, during the adiabatic expansion of air, are given by the following formulas:

$$\left(\frac{P}{P_1} \right)^{.29078} = \frac{T}{T_1}. \quad (86.) \text{ Art. 1170.}$$

$$\left(\frac{V_1}{V} \right)^{.41} = \frac{T}{T_1}. \quad (87.) \text{ Art. 1170.}$$

To obtain the area of the diagram representing the adiabatic compression of air, the following formula may be used which gives it directly when p and p_1 are the greater and lesser pressures, respectively, and V and V_1 their corresponding volumes:

$$\frac{pV - p_1V_1}{.41} = \text{area.} \quad (88.) \text{ Art. 1172.}$$

EFFICIENCY OF A PERFECT HEAT ENGINE.

Let $c = \frac{P_1 V_1}{T_1}$, and $r = \frac{V_2}{V_1}$, then, the efficiency of a perfect

$$\text{heat engine} = \frac{2.3026 c \log r_1 (T_1 - T_2)}{2.3026 c T_1 \log r_1} = E = \frac{T_1 - T_2}{T_1}. \quad (89.)$$

Art. 1182.

That is, *for a perfect heat engine, operating through a reversible cycle process, the efficiency of the machine is the ratio of the difference of the absolute temperatures of the sources of heat and of cold to the absolute temperature of the source of heat.*

FORMULAS USED IN STEAM AND STEAM ENGINES.

RELATION BETWEEN THE PRESSURE AND TEMPERATURE OF SATURATED STEAM.

Let t = temperature, Fahrenheit;

T = absolute temperature = $t + 460^\circ$;

p = absolute pressure (pressure above vacuum) in pounds per sq. in.

$$\text{Log } p = 6.1007 - \frac{2,719.78}{T} - \frac{400,215}{T^2}. \quad \left. \begin{array}{l} (90.) \\ \text{Art. 1197.} \end{array} \right\}$$

TOTAL HEAT OF VAPORIZATION.

Let H = total heat of vaporization;

t = temperature;

$$H = 1,081.94 + .305 t. \quad (91.) \quad \text{Art. 1200.}$$

SPECIFIC VOLUME OF SATURATED STEAM.

$$p V^{\frac{1}{3}} = 475, \quad (92.) \quad \text{Art. 1203.}$$

in which p is the pressure in pounds per square inch, and V the volume in cubic feet of a pound of steam at the given pressure.

WORK DONE IN THE CYLINDER OF A STEAM ENGINE.

Let P = the pressure on the piston in pounds per sq. ft.;

p = pressure on piston in pounds per sq. in.;

V = volume swept through by the piston;

W = work in foot-pounds.

$$\text{Then,} \quad W = P V = 144 p V. \quad (93.) \quad \text{Art. 1212.}$$

RELATION BETWEEN CLEARANCE, CUT-OFF, AND NUMBER OF EXPANSIONS, OR RATIO OF EXPANSION.

Let e = the number of expansions;

i = the clearance, expressed as a per cent. of the stroke;

k = the real cut-off;

k_1 = the apparent cut-off;

r = the apparent number of expansions = $\frac{1}{k_1}$.

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at the beginning of the stroke, are known, the M. E. P. may be found approximately by the following formula:

$$\text{M. E. P.} = \frac{.9 P(1 + 2.3 \log e)}{e} - .9 p, \quad (99.)$$

Art. 1269.

in which P = absolute steam pressure = gauge pressure + 14.7 pounds;

e = ratio of expansion;

p = absolute back pressure.

p is usually taken as about 3 pounds for condensing engines, and 17 pounds for non-condensing engines.

RELATION BETWEEN LENGTH OF STROKE, NUMBER OF REVOLUTIONS, AND PISTON SPEED.

Let L = length of stroke in inches;

R = number of revolutions per minute;

S = piston speed in feet per minute.

$$\left. \begin{aligned} S &= \frac{LR}{6}. \\ L &= \frac{6S}{R}. \\ R &= \frac{6S}{L}. \end{aligned} \right\} \quad (100.) \text{ Art. 1270.}$$

RATIO OF EXPANSION IN A COMPOUND OR TRIPLE-EXPANSION ENGINE.

Let e = ratio of expansion in high-pressure cylinder;

E = total ratio of expansion;

v = volume of cylinder receiving steam from the boiler;

V = volume of cylinder exhausting into atmosphere or condenser.

Then, $E = \frac{eV}{v}. \quad (102.) \text{ Art. 1298.}$

RATIO BETWEEN THE CYLINDERS OF A COMPOUND ENGINE.

Letting the letters have the same meaning as in the last formula, then either of the following formulas may be used:

$$E = 2.72 \frac{V}{v}, \text{ or } \frac{V}{v} = \frac{E}{2.72}. \quad (103.) \text{ Art. 1306.}$$

$$\frac{V}{v} = \sqrt{E}. \quad (104.) \text{ Art. 1306.}$$

AMOUNT OF WATER AND THE COOLING SURFACE FOR CONDENSERS.

Water Required by a Condenser.

Let t_1 = the temperature of departing condensing water;
 t_2 = the temperature of entering condensing water;
 t_3 = the temperature of the condensed steam upon leaving the condenser;

H = total heat of one pound of steam at the pressure of the exhaust;

W = the weight of water required per pound of steam condensed.

$$W = \frac{H - t_3 + 32}{t_1 - t_2}. \quad (105.) \text{ Art. 1323.}$$

Cooling Surface.

Let S = the required surface in square feet;

W = total weight of steam used per hour.

Then, $S = .0944 W$. (106.) Art. 1325.

TO FIND THE WEIGHT OF A FLY-WHEEL.

Let V_1 = the greatest velocity of the crank-pin in ft. per sec. ;
 V_2 = the least velocity of the crank-pin in ft. per sec. ;
 V_0 = average velocity of crank-pin in ft. per sec. ;

W = required weight of fly-wheel in pounds;

H = the number of foot-pounds per sq. in. of piston represented by the excess of crank effect over the resistance;

A = area of piston in square inches;

n = ratio between radius of fly-wheel and length of crank;

$E = \frac{V_1 - V_2}{V_0}$ = coefficient of unsteadiness.

$$W = \frac{A H g}{n^2 E V_0^2}. \quad (107.) \text{ Art. 1328.}$$

FORMULAS USED IN STRENGTH OF MATERIALS.**UNIT STRESS, UNIT STRAIN, AND COEFFICIENT OF ELASTICITY.**

Let P = the total stress in pounds;

A = area of cross-section in square inches;

S = unit stress in pounds per square inch;

l = length of body in inches;

e = elongation in inches;

s = unit strain;

E = coefficient of elasticity.

$$S = \frac{P}{A}, \text{ or } P = A S. \quad (108.) \text{ Art. 1345.}$$

$$s = \frac{e}{l}, \text{ or } e = l s. \quad (109.) \text{ Art. 1346.}$$

$$E = \frac{S}{s} = \frac{P}{A} \div \frac{e}{l} = \frac{Pl}{Ae}. \quad (110.) \text{ Art. 1352.}$$

STRENGTH OF PIPES AND CYLINDERS.

Let d = inside diameter of pipe in inches;

l = length of pipe in inches;

p = pressure in pounds per square inch;

P = total pressure; then $P = p l d$;

t = thickness of pipe;

S = working strength of the material.

For longitudinal rupture

$$p l d = 2 t l S, \text{ or}$$

$$p d = 2 t S. \quad (111.) \text{ Art. 1365.}$$

For transverse rupture

$$p d = 4 t S. \quad (112.) \text{ Art. 1366.}$$

Since, for longitudinal rupture, $p d = 2 t S$, it is seen that a cylinder is twice as strong against transverse rupture as against longitudinal rupture.

For pipes and cylinders whose thickness is greater than $\frac{1}{10}$ of the radius, use the following formula, in which r = the inner radius, and the other letters have the same meaning as before.

$$p = \frac{St}{r+t}. \quad (113.) \text{ Art. 1367.}$$

The following formula gives the collapsing pressure in lb. per sq. in. for wrought-iron pipe:

$$p = 9,600,000 \frac{t^{2.18}}{ld}. \quad (114.) \text{ Art. 1368.}$$

MOMENT OF INERTIA, RESISTING MOMENT, AND BENDING MOMENT OF BEAMS.

Let I = moment of inertia;

A = area of cross-section;

r = radius of gyration;

c = distance from neutral axis to outermost fiber;

S_s = ultimate strength of flexure;

f = factor of safety;

M = bending moment.

$$I = A r^2. \quad (115.) \text{ Art. 1396.}$$

The resisting moment is given by the expression

$$\frac{S}{c} A r^2 = \frac{S}{c} I, \text{ or } S \frac{I}{c}.$$

For the bending moment

$$M = S_s \frac{I}{c}, \quad (116.) \text{ Art. 1398.}$$

and, when a factor of safety is used,

$$M = \frac{S_s I}{f c}. \quad (117.) \text{ Art. 1401.}$$

DEFLECTION OF A BEAM.

Let a = a constant depending on the manner of loading the beam and the condition of the ends;

s = the deflection;

E = the coefficient of elasticity;

l = the length of the beam in inches;

W = the total weight supported in pounds;

I = moment of inertia about the neutral axis.

$$s = a \frac{W l^3}{E I}. \quad (118.) \text{ Art. 1404.}$$

STRENGTH OF COLUMNS.

Let W = load on a column;

S_c = ultimate strength for compression;

A = area of section of column;

f = factor of safety;

l = length of column in inches;

g = a constant to be taken from table;

I = least moment of inertia of cross-section;

b = length of longer side of a rectangular column;

d = length of shorter side of a rectangular column,
or the diameter of a circular column;

c = length of one side of a square column.

$$W = \frac{S_c A}{f \left(1 + \frac{A l^2}{g I} \right)}. \quad (119.) \text{ Art. 1411.}$$

$$c = \sqrt{\frac{W f}{2 S_c}} + \sqrt{\frac{W f}{S_c} \left(\frac{W f}{4 S_c} + \frac{12 l^2}{g} \right)}. \quad \left\{ \begin{array}{l} (120.) \\ \text{Art. 1413.} \end{array} \right.$$

For a circular column,

$$d = 1.4142 \sqrt{\frac{.3183 W f}{S_c}} + \sqrt{\frac{.3183 W f}{S_c} \left(\frac{.3183 W f}{S_c} + \frac{16 l^2}{g} \right)}. \quad (121.) \text{ Art. 1413.}$$

For a rectangular column, assume d , then,

$$b = \frac{W f \left(1 + \frac{12 l^2}{d^2 g} \right)}{d S_c}. \quad (122.) \text{ Art. 1413.}$$

STRENGTH OF SHAFTS.

Let d = diameter of a round shaft, or side of a square shaft, in inches;

c = a constant taken from Table 31;

c_1 = a constant taken from Table 31;

P = a force applied at the end of a lever arm in pounds;

r = length of lever arm in inches;

H = horsepower transmitted by shaft;
 N = number of revolutions per minute;
 k = a constant taken from Table 32;
 k_1 = a constant taken from Table 32;
 q = a constant taken from Table 32;
 q_1 = a constant taken from Table 32.

For all solid shafts below 11 inches in diameter use the formula

$$d = c \sqrt[4]{Pr} = c_1 \sqrt[4]{\frac{H}{N}}. \quad (123.) \text{ Art. 1415.}$$

If the diameter of a wrought-iron shaft is greater than 12.4", of a cast-iron shaft greater than 10.3", or of a steel shaft greater than 13.6", the following formula should be used:

$$d = k \sqrt[4]{Pr} = k_1 \sqrt[4]{\frac{H}{N}}. \quad (124.) \text{ Art. 1416.}$$

If the shaft is hollow (round) either of the two following formulas may be used:

$$P = q \left(\frac{d_1^4 - d_2^4}{d_1 r} \right), \quad (125.) \text{ Art. 1416.}$$

$$\text{or } H = q_1 N \left(\frac{d_1^4 - d_2^4}{d_1} \right). \quad (126.) \text{ Art. 1416.}$$

**SHAFTS SUBJECTED TO COMBINED BENDING AND
TWISTING.**

Let B = bending moment;

T = twisting moment;

T_1 = the twisting moment which would have the same effect as B and T acting together.

$$\text{Then, } T_1 = B + \sqrt{B^2 + T^2}. \quad (255.) \text{ Art. 1991.}$$

The twisting moment T_1 is called the **ideal twisting moment**, and should be used in place of Pr in formulas **123** and **124** to determine the diameter of a shaft subjected to combined bending and twisting.

VALUES OF c AND c_1 TO BE USED IN FORMULA 123.

Material.	c		c_1	
	Round.	Square.	Round.	Square.
Wrought Iron	.31	.272	4.92	4.31
Cast Iron	.353	.309	5.59	4.89
Steel	.297	.26	4.7	4.11

VALUES OF k , k_1 , q , AND q_1 TO BE USED IN FORMULAS 124, 125, AND 126.

Material.	k	k_1	q	q_1
Wrought Iron	.0909	3.62	1,335	.0212
Cast Iron	.1145	4.56	669	.0106
Steel	.0828	3.3	1,767	.028

STRENGTH OF ROPES AND CHAINS.

Let P = working or safe load in pounds;

C = circumference of rope in inches;

d = diameter of the link of a chain in inches.

For manila ropes, hemp ropes, or tarred hemp ropes,

$$P = 100 C. \quad (127.) \text{ Art. 1417.}$$

For iron wire rope of 7 strands, 19 wires to the strand,

$$P = 600 C. \quad (128.) \text{ Art. 1418.}$$

For the best steel wire rope, 7 strands, 19 wires to the strand,

$$P = 1,000 C. \quad (129.) \text{ Art. 1418.}$$

For open-link chains made from a good quality of wrought iron,

$$P = 12,000 d^2, \quad (130.) \text{ Art. 1421.}$$

and for stud-link chains,

$$P = 18,000 d^2. \quad (131.) \text{ Art. 1421.}$$

FORMULAS USED IN APPLIED MECHANICS.**RELATION BETWEEN THE DIAMETERS AND NUMBER OF REVOLUTIONS OF PULLEYS.**

Let D_1 = diameter of driving pulley;
 N_1 = number of revolutions of driving pulley;
 F_1 = diameter of driven pulley;
 n_1 = number of revolutions of driven pulley.

$$\frac{N_1}{n_1} = \frac{F_1}{D_1}. \quad (136.) \text{ Art. 1477.}$$

$$D_1 N_1 = F_1 n_1.$$

HORSEPOWER OF BELTS.

Let H = horsepower to be transmitted;
 W = width of belt in inches;
 S = belt speed in feet per minute.

FOR SINGLE BELTS.

$$H = \frac{WS}{900}. \quad (138.) \text{ Art. 1488.}$$

$$W = \frac{900 H}{S}. \quad (139.) \text{ Art. 1488.}$$

$$S = \frac{900 H}{W}. \quad (140.) \text{ Art. 1488.}$$

FOR DOUBLE BELTS.

$$H = \frac{WS}{630}. \quad (141.) \text{ Art. 1489.}$$

$$W = \frac{630 H}{S}. \quad (142.) \text{ Art. 1489.}$$

$$S = \frac{630 H}{W}. \quad (143.) \text{ Art. 1489.}$$

TEETH OF GEAR-WHEELS.

Let P = diametral pitch;
 D = diameter of pitch circle of large gear;
 d = diameter of pitch circle of small gear;
 $O D$ = outside diameter;

C = circular pitch;

N = number of teeth;

A = distance between centers of wheels;

V = velocity; i. e., revolutions per minute of large gear.

v = velocity; i. e., revolutions per minute of small gear.

$$P = \frac{3.1416}{C}, \text{ and} \quad (149.)$$

$$C = \frac{3.1416}{P}. \quad (150.) \text{ Art. 1556.}$$

$$N = DP. \quad (151.) \text{ Art. 1557.}$$

$$OD = \frac{N}{P} + 2 \times \frac{1}{P} = \frac{N+2}{P}. \quad (152.) \text{ Art. 1557.}$$

$$D = \frac{C \times N}{3.1416}. \quad (153.) \text{ Art. 1557.}$$

Given the distance between the centers of two gears and their velocities, the formulas for their diameters are

$$d = \frac{2 A V}{V+v}; \quad (154.)$$

$$\text{and } D = \frac{2 A v}{v+V}. \quad (155.) \text{ Art. 1557.}$$

THE PRONY BRAKE.

Let $H. P.$ = number of horsepower absorbed;

R = length of lever arm in feet;

W = weight in scale pan;

N = number of revolutions per minute;

r = length of lever arm in inches.

$$H. P. = \frac{2 \times 3.1416 \times R \times W \times N}{33,000}, \text{ or}$$

$$H. P. = .0001904 R W N. \quad (156.) \text{ Art. 1593.}$$

$$H. P. = .00001586 r W N. \quad (157.) \text{ Art. 1595.}$$

FORMULAS USED IN STEAM BOILERS.**STRENGTH OF BOILER SHELLS AND TUBES.**

Let p = the pressure of steam in pounds per square inch;
 t = thickness of plate in shell or tube;
 d = diameter of shell or tube;
 S_1 = ultimate tensile strength of material;
 f = factor of safety;
 y = efficiency of joint;
 l = length of a tube subjected to external pressure.

For tubes without riveted joints,

$$t = \frac{fpd}{2S_1}. \quad (164.) \text{ Art. 1730.}$$

$$p = \frac{2tS_1}{fd}. \quad (166.) \text{ Art. 1731.}$$

For tubes or shells with riveted joints,

$$t = \frac{fpd}{2S_1y}, \quad (165.)$$

$$p = \frac{2tS_1y}{fd}. \quad (167.) \text{ Art. 1731.}$$

For tubes subjected to external pressure,

$$p = 1,600,000 \frac{t^3}{ld}. \quad (168.) \text{ Art. 1732.}$$

RIVETED JOINTS.

Let d = diameter of rivet hole in inches;

h = pitch of rivets in inches;

t = thickness of plate in inches.

$$h = \left(1 + \frac{7d}{8t}\right)d. \quad (169.) \text{ Art. 1742.}$$

For double-riveted lap joints or single butt joints, formula 169 becomes

$$h = \left(1 + \frac{7d}{4t}\right)d. \quad (170.) \text{ Art. 1742.}$$

For double-riveted double butt joints, formula 170 becomes

$$h = \left(1 + \frac{7d}{2t}\right)d. \quad (171.) \text{ Art. 1742.}$$

The d in the above formulas refers to the diameter of the rivet hole, or of the rivet after being headed.

The diameter of the cold rivet is $\frac{1}{8}$ " less.

For single and double-riveted lap joints and butt joints, with one cover plate, the diameter of the rivet is

$$d = t + \frac{3}{8} \quad (172.) \text{ Art. 1742.}$$

for values of t between $\frac{1}{4}$ " and $\frac{3}{4}$ ". For butt joints with double cover plates, the diameter of rivet may be taken about $1\frac{1}{2}$ times the thickness of the plate.

FLAT SURFACES.

The strength of a circular plate supported at the edges, as, for example, the head of a boiler shell, is given by the following formula:

$$S = \frac{2r^2p}{3t^3}, \quad (174.) \text{ Art. 1751.}$$

$$t = r\sqrt{\frac{2p}{3S}}, \quad (175.) \text{ Art. 1751.}$$

where S represents the safe tensile strength of the material, r the radius of the plate in inches, t the thickness of the plate in inches, and p the pressure in lb. per sq. in.

The following formula gives the strength of a square unstayed flat plate fixed along the edge (the length of side is a):

$$\left. \begin{aligned} S &= \frac{a^2p}{4t^3}, \\ \text{or } t &= \frac{a}{2}\sqrt{\frac{p}{S}}. \end{aligned} \right\} \quad (176.) \text{ Art. 1752.}$$

BOILER STAYS.

Let A = area in sq. in. of plate supported by one stay;

d = smallest diameter of stay in inches;

p = pressure of steam in pounds per sq. in.;

T = safe stress per sq. in. allowed on stay;
 a = pitch for stays arranged at equal distances apart,
 both horizontally and vertically.

$$\left. \begin{aligned} \frac{1}{4} \pi d^2 T &= A p, \\ \text{or } d &= 1.13 \sqrt{\frac{A p}{T}}. \end{aligned} \right\} \quad (177.) \text{ Art. 1756.}$$

$$d = 1.13 a \sqrt{\frac{p}{T}}, \quad (178.) \text{ Art. 1756.}$$

$$\text{and } a = .885 d \sqrt{\frac{T}{p}}. \quad (179.) \text{ Art. 1756.}$$

The values of T used in formulas 177, 178, and 179 may be taken as follows:

For copper screw staybolts..... $T = 4,000$

Iron Stays.—For screw stays, and for other stays not exceeding $1\frac{1}{4}$ inches in diameter, and for all stays which are welded..... $T = 6,000$

For unwelded stays above $1\frac{1}{4}$ inches effective diameter..... $T = 7,500$

Steel Stays.—For screw stays, and for other stays not exceeding $1\frac{1}{4}$ inches effective diameter..... $T = 8,000$

For stays above $1\frac{1}{4}$ inches effective diameter..... $T = 9,000$

No steel stays are to be welded.

The size of a diagonal stay may be calculated from formula 178 by substituting $\frac{p}{\cos B}$ for p , B being the angle between the stay and the shell. Formula 178 thus becomes

$$d = 1.13 \sqrt{\frac{A p}{T \cos B}}. \quad (180.) \text{ Art. 1758.}$$

For the strength of a girder stay:

Let l = length of girder in inches;

h = distance between adjacent girders in inches;

p = steam pressure in lb. per sq. in.;

b = breadth of girder in inches = $\frac{1}{4} d$;

d = depth of girder in inches.

$$d = \sqrt[3]{\frac{p h l^3}{6,000}}. \quad (181.) \text{ Art. 1761.}$$

$$p = \frac{6,000 d^3}{h l^3}. \quad (182.) \text{ Art. 1761.}$$

- For the safe pressure allowable on a flat surface, strengthened by screw staybolts:

Let p = pressure in lb. per sq. in.;

h = pitch of staybolts;

t = thickness of plate;

k = a constant.

$$\text{Then, } p = k \frac{t^2}{h^2}, \quad (183.)$$

$$\text{and } t = h \sqrt{\frac{p}{k}}. \quad (184.) \text{ Art. 1763.}$$

The constant k has the following values:

For iron plates and iron bolts $k = 24,000$

For low steel plates and iron bolts $k = 25,000$

For low steel plates and low steel bolts $k = 28,000$

For iron plates and iron bolts with nuts $k = 40,000$

For copper plates and iron bolts $k = 14,500$

SAFETY VALVES.

For a dead-weight safety valve:

Let A = area of opening in valve seat in sq. in.;

p = pressure at which the valve is to blow off (in lb. per sq. in.);

W = dead weight in pounds (including weight of valve).

$$W = A p. \quad \text{Art. 1774.}$$

For a weighted-lever safety valve:

Let $d = FB$ = distance from fulcrum to weight in inches;

$c = FG$ = distance from fulcrum to center of gravity of lever in inches;

$a = FV$ = distance from fulcrum to center of valve in inches;

A = area of orifice beneath bottom of valve in inches;

W = weight of weight P in pounds;

W_1 = weight of valve and stem in pounds;

W_2 = weight of lever in pounds;

P = blow-off pressure in pounds per sq. in.;

$W_3 = W_1 + W_2$ = combined weight of valve and lever;

b = distance from fulcrum of center of gravity of W_3 .

$$W = \frac{a(pA - W_1) - W_3c}{d}, \quad (185.) \text{ Art. 1776.}$$

$$\text{and } d = \frac{a(pA - W_1) - W_3c}{W}. \quad (186.) \text{ Art. 1776.}$$

$$\text{Also } d = \frac{pAa - W_3b}{W}. \quad (187.) \text{ Art. 1778.}$$

To find the area of a safety valve:

Let a = area of the valve opening in square inches;

w = maximum weight of steam generated in pounds per hour;

p = gauge pressure in pounds per square inch.

$$a = \frac{.5w}{p + 10}. \quad (188.) \text{ Art. 1781.}$$

DIMENSIONS OF CHIMNEYS.

Let H = height of chimney in feet;

$H. P.$ = horsepower of boiler or boilers;

A = actual area of chimney in square feet;

E = effective area of chimney in square feet;

S = side of square chimney in inches;

d = diameter of round chimney in inches;

p = pressure of draft in inches of water;

T_a = absolute temperature of outside air;

T_c = absolute temperature of gas in chimney.

$$p = H \left(\frac{7.6}{T_a} - \frac{7.9}{T_c} \right). \quad (192.) \text{ Art. 1825.}$$

$$H = \frac{p}{\left(\frac{7.6}{T_a} - \frac{7.9}{T_c} \right)}. \quad (193.) \text{ Art. 1826.}$$

$$E = \frac{.3 H. P.}{\sqrt{H}} = A - .6 \sqrt{A}. \quad (194.) \text{ Art. 1827.}$$

$$H. P. = 3.33 E \sqrt{H}. \quad (195.) \text{ Art. 1827.}$$

$$S = 12 \sqrt{E} + 4. \quad (196.) \text{ Art. 1827.}$$

$$d = 13.54 \sqrt{E} + 4. \quad (197.) \text{ Art. 1827.}$$

The *maximum* rates of combustion attainable under natural draft are given by the following formulas:

Let F = weight in pounds of coal per hour per square foot of grate area;

H = height in feet of chimney or stack.

Then, for anthracite coal burned under the most favorable conditions,

$$F = 2 \sqrt{H} - 1, \quad (198.) \text{ Art. 1829.}$$

and under ordinary conditions,

$$F = 1.5 \sqrt{H} - 1. \quad (199.) \text{ Art. 1829.}$$

For best semianthracite and bituminous coals,

$$F = 2.25 \sqrt{H}, \quad (200.) \text{ Art. 1829.}$$

and for less valuable soft coals,

$$F = 3 \sqrt{H}. \quad (201.) \text{ Art. 1829.}$$

GRATE AREA.

Let G = area of grate in sq. ft.;

F = rate of combustion in lb. per sq. ft. of grate surface per hour;

W = weight of steam generated per hour by boiler or boilers;

e = evaporation in pounds of water per pound of coal per hour.

$$\text{Then,} \quad G = \frac{W}{Fe}. \quad (202.) \text{ Art. 1830.}$$

In using this formula care must be taken that W and e are taken at the same pressure and temperature.

TO REDUCE THE ACTUAL EVAPORATION TO AN EQUIVALENT EVAPORATION.

Let W = the actual evaporation;

H = total heat of steam above 32° at pressure of actual evaporation;

t = observed temperature of feed-water;

W' = equivalent evaporation from and at 212° .

Then, $W(H - t + 32) = 966.1 W'$,

$$\text{or } W' = \frac{W(H - t + 32)}{966.1}. \quad (203.) \text{ Art. 1838.}$$

The quantity $\left(\frac{H - t + 32}{966.1}\right)$ which changes actual evaporation to equivalent evaporation from and at 212° is called the **factor of evaporation**.

TO FIND THE QUALITY OF STEAM BY MEANS OF THE BARREL CALORIMETER.

Let W = original weight of water in barrel;

w = weight of steam and water condensed in the cold water;

l = latent heat of steam at observed pressure;

t = temperature of steam at observed pressure;

t_1 = initial temperature of water;

t_2 = final temperature of water;

x = the portion of w which is dry steam;

Q = quality of steam; that is, the percentage of the mixture evaporated, which is pure dry steam.

$$Q = \frac{x}{w} = \frac{1}{l} \left[\frac{W}{w} (t_2 - t_1) - (t - t_1) \right]. \quad (204.) \text{ Art. 1853.}$$

TO FIND THE QUALITY OF STEAM BY MEANS OF THE SEPARATOR CALORIMETER.

Let W = weight of dry steam discharged from the instrument;

w = weight of water drawn from separator;

R = water condensed by radiation;

Q = quality of steam.

$$Q = \frac{W + R}{W + R + w}. \quad (205.) \text{ Art. 1855.}$$

FORMULAS USED IN MACHINE DESIGN.**PROPORTIONS OF BOLT HEADS, NUTS, AND WASHERS.** d = diameter of bolt.

Diameter of nut or head across flats:

$$\left. \begin{aligned} D &= 1\frac{1}{2}d + \frac{1}{8}" \text{ for rough work.} \\ D &= 1\frac{1}{2}d + \frac{1}{16}" \text{ for finished work.} \end{aligned} \right\} \quad (220.) \text{ Art. 1937.}$$

Height of nut:

$$\left. \begin{aligned} h &= d \text{ for rough work.} \\ h &= d - \frac{1}{16}" \text{ for finished work.} \end{aligned} \right\} \quad (221.) \text{ Art. 1937.}$$

$$\text{Thickness of washer, } t = .15 d. \quad (222.) \text{ Art. 1937.}$$

$$\text{Diameter of washer, } D_1 = 1\frac{1}{8} D. \quad (223.) \text{ Art. 1937.}$$

The above proportions for diameters D hold for both hexagonal and square nuts. The diameter across corners D_1 is as follows:

For hexagonal nuts:

$$D_1 = \left\{ \begin{aligned} &1.73 d + .14" \text{ for rough nuts.} \\ &1.73 d + .07" \text{ for finished nuts.} \end{aligned} \right. \quad (224.) \text{ Art. 1937.}$$

For square nuts:

$$D_1 = \left\{ \begin{aligned} &2.12 d + .18" \text{ for rough nuts.} \\ &2.12 d + .09" \text{ for finished nuts.} \end{aligned} \right. \quad (225.) \text{ Art. 1937.}$$

Height of head:

$$\left. \begin{aligned} h' &= \frac{3}{4}d + \frac{1}{16}" \text{ for rough bolts.} \\ h' &= d - \frac{1}{16}" \text{ for finished bolts.} \end{aligned} \right\} \quad (226.) \text{ Art. 1937.}$$

PROPORTIONS OF KEYS.Let b = width of key in inches; t = thickness of key in inches; l = length of key in inches; N = number of revolutions per minute; H = horsepower transmitted by a pulley.

$$\left. \begin{aligned} b &= \frac{d}{7} + \frac{1}{4}" \\ t &= \frac{d}{12} + \frac{3}{16}" \end{aligned} \right\} \text{ For driven pulleys. } \quad (234.) \text{ Art. 1965.}$$

$$\left. \begin{aligned} b &= .2d + .16". \\ t &= .1d + .16". \end{aligned} \right\} \text{For driving pulleys.} \quad (235.) \text{ Art. 1965.}$$

$$\left. \begin{aligned} b &= \frac{d}{3}. \\ t &= \frac{d}{5}. \end{aligned} \right\} \text{When } d \text{ is less than } 1\frac{3}{4} \text{ in.,} \quad (236.) \text{ Art. 1965.}$$

When the pulley transmits but a small part of the power of a shaft, use the formula $d = 5\sqrt[3]{\frac{H}{N}}$ from which to obtain the value of d to use in formula 236.

For sliding feather keys,

$$\left. \begin{aligned} b &= \frac{d}{8} + \frac{1}{16} ". \\ t &= \frac{3d}{16} + \frac{1}{16} ". \end{aligned} \right\} \quad (237.) \text{ Art. 1965.}$$

PROPORTIONS AND STRENGTH OF GEAR-WHEELS.

Let p = pressure acting at pitch line;

b = breadth of tooth;

n = number of revolutions per minute;

H = horsepower transmitted;

D = diameter of gear in inches;

C = the circular pitch;

P = diametral pitch;

S = allowable working stress in tooth;

v = velocity of a point in the pitch circle in feet per minute;

c = thickness of rim.

$$bC = 16.8 \frac{p}{S}. \quad (266.) \text{ Art. 2024.}$$

If v is greater than 100 feet per minute make

$$S = \frac{9,600,000}{v + 2,160}. \quad (267.) \text{ Art. 2024.}$$

To insure durability make

$$\frac{pn}{b} = 28,000, \text{ or } b = 4\frac{1}{2} \frac{H}{D}. \quad (268.) \text{ Art. 2025.}$$

To calculate the dimensions of the arms·

Let z = number of arms in wheel;

a = width of arm, measured at center of wheel;

x = thickness of arm;

S_1 = allowable safe stress in arm;

R = radius of wheel in inches;

p = pressure between gears at pitch line.

For cross-shaped, T, or I sections:

$$\left. \begin{aligned} a &= \sqrt{\frac{Rb}{z}}. \\ x &= \frac{1}{2} C. \end{aligned} \right\} \quad (270.) \text{ Art. 2030.}$$

For oval or elliptical sections:

$$\left. \begin{aligned} a &= 1.2 \sqrt[3]{\frac{bCR}{z}}. \\ a &= 1.75 \sqrt[3]{\frac{bR}{Pz}}. \\ x &= \frac{a}{2}. \end{aligned} \right\} \quad (271.) \text{ Art. 2030.}$$

For thickness of rim:

$c = \frac{1}{2} C$ for large gears and coarse pitch.

$c = .4 C \times \frac{1}{8}''$ for gears with small pitch.

PROPORTIONS OF BEVEL GEARS.

Denote the mean circular pitch by C_m .

Then, $b C_m = 16.8 \frac{p}{S}$. (266a.) Art. 2033.

$$c = .4 C_m + \frac{1}{8}'' = \frac{5}{4P} + \frac{1}{8}'' \quad (269a.) \text{ Art. 2033.}$$

$$\left. \begin{aligned} a &= \sqrt{\frac{Rb}{z}}. \\ x &= \frac{1}{2} C_m. \end{aligned} \right\} \quad (270a.) \text{ Art. 2033.}$$

$$\left. \begin{aligned} a &= 1.2 \sqrt[3]{\frac{b C_m R}{z}}. \\ a &= 1.75 \sqrt[3]{\frac{b R}{P_m z}}. \end{aligned} \right\} \quad (271a.) \text{ Art. 2033.}$$

RULES AND FORMULAS USED IN DYNAMOS AND MOTORS.

DIRECTION OF LINES OF FORCE AROUND A CONDUCTOR.

Rule.—*If the current is flowing in the conductor away from the observer, then the direction of the lines of force will be around the conductor in the direction of the hands of a watch.* Art. 2157.

TO DETERMINE THE POLARITY OF A SOLENOID.

Rule.—*In looking at the end of the helix, if it is so wound that the current circulates around the helix in the direction of the hands of a watch, that end will be a south pole; if in the other direction it will be a north pole.* Art. 2160.

RESISTANCE OF CONDUCTORS.

Let r_1 = the original resistance of a conductor;

r_2 = the changed resistance;

l_1 = the original length;

l_2 = the changed length;

a_1 = the original sectional area;

a_2 = the changed sectional area;

D = the original diameter;

d = the changed diameter;

k = temperature coefficient;

t = rise or fall in temperature, degrees Fahrenheit.

For a change in the length of a conductor:

$$r_2 = \frac{r_1 l_2}{l_1}. \quad (306.) \quad \text{Art. 2171.}$$

For a change in the sectional area of a conductor:

$$r_2 = \frac{r_1 a_1}{a_2}. \quad (307.) \quad \text{Art. 2172.}$$

For a change in the diameter of a conductor:

$$r_2 = \frac{r_1 D^2}{d^2}. \quad (308.) \quad \text{Art. 2173.}$$

For a rise in the temperature of a conductor:

$$r_2 = r_1(1 + t k). \quad (309.) \text{ Art. 2177.}$$

For a fall in the temperature of a conductor:

$$r_2 = \frac{r_1}{1 + t k}. \quad (310.) \text{ Art. 2178.}$$

**RESISTANCES AND TEMPERATURE COEFFICIENTS OF
DIFFERENT METALS.**

Name of Metal.	Resistance, Microhms per Cu. In.	Relative Resistance.	Temperature Coefficient.
Silver, annealed.....	.5921	1.	.002094
Copper, annealed....	.6292	1.063	.002155
Silver, hard-drawn...	.6433	1.086	.002094
Copper, hard-drawn..	.6433	1.086	.002155
Gold, annealed.....	.8102	1.369	.002028
Gold, hard-drawn....	.8247	1.393	.002028
Aluminum, annealed	1.1470	1.935	
Zinc, pressed.....	2.215	3.741	.002028
Platinum, annealed.	3.565	6.022	
Iron, annealed.....	3.825	6.460	
Nickel, annealed....	4.907	8.285	
Tin, pressed.....	5.202	8.784	.002028
Lead, pressed.....	7.728	13.05	.002150
German silver.....	8.240	13.92	.000244
Antimony, pressed...	13.98	23.60	.002161
Mercury	37.15	62.73	.000400
Bismuth, pressed....	51.65	87.23	.001967

**CURRENT STRENGTH, ELECTROMOTIVE FORCE, AND
RESISTANCE.**

Let C = strength of current flowing in a closed circuit;

E = electromotive force;

R = resistance.

$$C = \frac{E}{R}. \quad (311.) \text{ Art. 2192.}$$

$$R = \frac{E}{C}. \quad (312.) \text{ Art. 2193.}$$

$$E = C R. \quad (313.) \text{ Art. 2194.}$$

**TO FIND THE AVAILABLE ELECTROMOTIVE FORCE
IN A CELL.**

Let E = the total generated E. M. F.;

E' = *available* E. M. F. when the circuit is closed;

C = the current flowing when the circuit is closed;

r_i = the internal resistance of the cell.

$$E' = E - C r_i. \quad (314.) \text{ Art. 2198.}$$

**THE CURRENT AND RESISTANCE IN BRANCHES OF
DIVIDED CONDUCTORS.**

Let r_1 = resistance of first branch;

r_2 = resistance of second branch;

r_3 = resistance of third branch;

c_1 = current in first branch;

c_2 = current in second branch;

C = sum of the currents in the two branches;

R'' = joint resistance of two branches in parallel;

R''' = joint resistance of three branches in parallel.

$$c_1 = \frac{C r_2}{r_1 + r_2}. \quad (315.) \text{ Art. 2200.}$$

$$c_2 = \frac{C r_1}{r_1 + r_2}. \quad (316.) \text{ Art. 2200.}$$

$$R'' = \frac{r_1 r_2}{r_1 + r_2}. \quad (317.) \text{ Art. 2202.}$$

$$R''' = \frac{r_1 r_2 r_3}{r_1 r_2 + r_1 r_3 + r_2 r_3}. \quad (318.) \text{ Art. 2203.}$$

ELECTRICAL QUANTITY.

Let Q = quantity of electricity in coulombs;

C = current strength in amperes;

t = time in seconds;

$$Q = C t. \quad (319.) \text{ Art. 2207.}$$

ELECTRICAL WORK AND POWER. J = electrical work in joules; $F.P$ = work in foot-pounds; Q = quantity of electricity in coulombs; C = current in amperes; t = time in seconds during which the current flows; E = potential, or E. M. F., of circuit; R = resistance of circuit; W = power in watts; $H. P.$ = horsepower.

$$J = C E t. \quad (320.) \text{ Art. 2209.}$$

$$J = C^2 R t. \quad (321.) \text{ Art. 2209.}$$

$$J = \frac{E^2 t}{R}. \quad (322.) \text{ Art. 2209.}$$

$$F.P = .7373 J. \quad (323.) \text{ Art. 2210.}$$

$$W = C E. \quad (324.) \text{ Art. 2211.}$$

$$W = C^2 R. \quad (325.) \text{ Art. 2211.}$$

$$W = \frac{E^2}{R}. \quad (326.) \text{ Art. 2211.}$$

$$H. P. = \frac{W}{746}. \quad (327.) \text{ Art. 2212.}$$

$$W = H. P. \times 746. \quad (328.) \text{ Art. 2213.}$$

TO DETERMINE THE DIRECTION OF THE CURRENT GENERATED IN A CONDUCTOR.

Rule.—Place thumb, forefinger, and middle finger of the right hand so that each will be perpendicular to the other two; if the forefinger points in the direction of the lines of force, and the thumb points in the direction towards which the conductor is moving, then the middle finger will point in the direction towards which the current generated in the conductor tends to flow. Art. 2221.

DETERMINATION OF ELECTROMOTIVE FORCE.

Let E = maximum electromotive force obtained at the brushes;

N = total number of lines of force passing from north pole through the core to the south pole;

S = number of outside wires on the periphery through which the current flows *in series*;

n = number of complete revolutions per second of core.

$$E = \frac{2 N S n}{10^8}. \quad (329.) \quad \text{Art. 2236.}$$

TO DETERMINE THE DIRECTION OF MOTION IMPARTED TO A CONDUCTOR.

Rule.—Place thumb, forefinger, and middle finger of the left hand each at right angles to the other two; if the forefinger points in the direction of the lines of force, and the middle finger points in the direction towards which the current flows, then the thumb will point in the direction of movement imparted to the conductor. Art. 2239.

EFFICIENCY OF A DYNAMO.

Let I = input of a dynamo;

O = output;

E = efficiency, per cent.

$$E = \frac{100 \times O}{I}. \quad (330.) \quad \text{Art. 2273.}$$

PER CENT. LOSS IN A DYNAMO.

Let L = per cent. loss;

I = input;

O = output.

$$L = \frac{100 (I - O)}{I}. \quad (331.) \quad \text{Art. 2274.}$$

When the output and efficiency are given:

$$I = \frac{100 \times O}{E}. \quad (332.) \quad \text{Art. 2275.}$$

When the input and efficiency are given:

$$O = \frac{I E}{100} \quad (333.) \quad \text{Art. 2276.}$$

**HORSEPOWER, TORQUE, AND NUMBER OF REVOLUTIONS
OF MOTORS.**

Let $H. P.$ = horsepower.

T = torque;

S = number of revolutions per minute.

$$H. P. = .0001904 T S. \quad (334.) \quad \text{Art. 2346.}$$

$$S = \frac{H. P.}{.0001904 T} \quad (335.) \quad \text{Art. 2346.}$$

$$T = \frac{H. P.}{.0001904 S} \quad (336.) \quad \text{Art. 2346.}$$

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